



โครงการพัฒนาพื้นที่ส่วนขยาย
ศูนย์ราชการเฉลิมพระเกียรติ ๘๐ พรรษา ๕ ธันวาคม ๒๕๕๐ พื้นที่โซน C
บริษัท ธนารักษ์พัฒนาสินทรัพย์ จำกัด

แบบรายละเอียดฉบับสมบูรณ์ (Final Detailed Design)
สัญญาก่อสร้างอาคารทิศตะวันตก
(ส่วนงานโครงสร้าง งานสถาปัตยกรรม และงานระบบหลัก)

รายงานการออกแบบ Design Note รายการคำนวณ
งานโครงสร้าง

(REVISION 0)

จัดทำโดย



1 เมษายน 2564



สารบัญ

หมวด

1.	เกณฑ์กำหนดในการออกแบบ (Design Criteria)	1
2.	รายการคำนวณเสา, กำแพง	2
3.	รายการคำนวณพื้นคอนกรีตอัดแรงภายหลัง	3
4.	รายการคำนวณพื้นค.สล.	4
5.	รายการคำนวณคาน	5
6.	รายการคำนวณบันไดและเบ็ดเตล็ด.....	6
7.	รายการคำนวณโครงสร้างเหล็ก.....	7





รายงานการออกแบบ Design Note รายการคำนวณงานโครงสร้าง

(สัญญาก่อสร้างอาคารทิศตะวันตก Final Detailed Design)

(ส่วนงานโครงสร้าง งานสถาปัตยกรรม และงานระบบหลัก)

โครงการพัฒนาพื้นที่ส่วนขยายศูนย์ราชการเฉลิมพระเกียรติ ๘๐ พรรษา ๕ ธันวาคม ๒๕๕๐ พื้นที่โซน C

1. เกณฑ์กำหนดในการออกแบบ (Design Criteria)



หมวดที่ 1

ข้อกำหนดที่ใช้ในการออกแบบ (Design Criteria)

1. มาตรฐาน พระราชบัญญัติ และข้อบัญญัติที่ใช้อ้างอิง (Standards and Codes)

ในการออกแบบโครงสร้างคอนกรีตเสริมเหล็กใช้ทฤษฎีกำลังประลัย (Ultimate Strength Design) สำหรับโครงสร้างเหล็กใช้วิธีหน่วยแรงที่ยอมให้ (Allowable Strength Design) โดยจะยึดถือตามกฎหมายที่เกี่ยวข้อง และมาตรฐานของสมาคมวิชาชีพ ดังนี้

- พระราชบัญญัติควบคุมอาคาร พ.ศ. 2522 และกฎกระทรวงที่ออกตามความในพระราชบัญญัติฉบับนี้
- ข้อบัญญัติกรุงเทพมหานคร เรื่องควบคุมอาคาร พ.ศ. 2544
- มาตรฐานสำหรับอาคารคอนกรีตเสริมเหล็กโดยวิธีกำลังของวิศวกรรมสถานแห่งประเทศไทยในพระบรมราชูปถัมภ์
- มาตรฐานสำหรับอาคารเหล็กgrupพรรณ ของวิศวกรรมสถานแห่งประเทศไทยในพระบรมราชูปถัมภ์
- มาตรฐานประกอบการออกแบบอาคารเพื่อดำเนินงานการสันเสีของแผ่นดินไหว มยผ. 1302-52 กรมโยธาธิการและผังเมือง, กระทรวงมหาดไทย
- มาตรฐานประกอบการออกแบบอาคารเพื่อดำเนินงานการสันเสีของแผ่นดินไหว ปรับปรุงครั้งที่ 1 มยผ.1301-54 กรมโยธาธิการและผังเมือง, กระทรวงมหาดไทย
- มาตรฐานการออกแบบอาคารเพื่อดำเนินงานการสันเสีของแผ่นดินไหว มยผ.1301/1302-61
- มาตรฐานการคำนวณแรงลมและการตอบสนองของอาคาร, มยผ.1311-50 กรมโยธาธิการและผังเมือง, กระทรวงมหาดไทย
- American Society of Civil Engineer, Minimum Design Loads for Buildings and Other Structures (ASCE/SEI 7)
- American Society for Testing and Material (ASTM)
- Precast-Prestressed Concrete Institute (PCI)
- ACI Committee 318, "Building Code Requirement for Reinforced Concrete" (ACI 318)
- American Institute of Steel Construction, "Steel Construction Manual" (AISC)
- Uniform Building Code (UBC)
- ACI Committee 350, "Code Requirements for Environmental Engineering Concrete Structures"
- International Building Code (IBC)

2. กำลังวัสดุที่ใช้ในการออกแบบ

กำลังวัสดุที่ใช้ในการคำนวณหรือควบคุมคุณภาพวัสดุ จะใช้ค่าต่าง ๆ ดังต่อไปนี้

- (1) คอนกรีต ค่ากำลังต้านทานแรงอัด (Compressive Strength: f_c') ของคอนกรีตรูปทรงกระบอกมาตรฐานเส้นผ่าศูนย์กลาง 0.15 ม. สูง 0.30 ม. ที่อายุครบ 28 วัน มีค่าดังนี้
 - คอนกรีตอัดแรง f_c' ไม่น้อยกว่า 350 กก./ตร.ซม.
 - คอนกรีตเสริมเหล็กทั่วไป f_c' ไม่น้อยกว่า 350 กก./ตร.ซม.
- (2) เหล็กเสริมและเหล็กรูปพรรณ ค่าแรงดึงที่จุดคราก (Yield Strength: f_y) ของเหล็กมีค่าดังนี้
 - เหล็กข้ออ้อย ตามมาตรฐานผลิตภัณฑ์อุตสาหกรรม (มอก.) 24-2559 ของกระทรวงอุตสาหกรรม ชั้นคุณภาพ SD-40 มีค่า f_y ไม่น้อยกว่า 4,000 กก./ตร.ซม. สำหรับเหล็กเสริม ขนาดเส้นผ่าศูนย์กลาง 12 มม. ถึง 28 มม.
 - เหล็กข้ออ้อย ตามมาตรฐานผลิตภัณฑ์อุตสาหกรรม (มอก.) 24-2559 ของกระทรวงอุตสาหกรรม ชั้นคุณภาพ SD-50 มีค่า f_y ไม่น้อยกว่า 5,000 กก./ตร.ซม. สำหรับเหล็กเสริม ขนาดเส้นผ่าศูนย์กลาง 32 มม.
 - เหล็กเส้นกลม ตามมาตรฐานผลิตภัณฑ์อุตสาหกรรม (มอก.) 20-2559 ชั้นคุณภาพ SR-24 มีค่า f_y ไม่น้อยกว่า 2,400 กก./ตร.ซม.
 - เหล็กที่เกลียวกำลังสูงชนิด 7 เส้น (PC Strand) ตามมาตรฐานผลิตภัณฑ์อุตสาหกรรม (มอก.) 420-2540
 - เหล็กรูปพรรณชนิด Hot-rolled of Cold rolled Mild Steel ชั้นคุณภาพ SS-400 ตามมาตรฐานอุตสาหกรรมไทย มอก.1227-2558 โดยมีค่าแรงดึงที่จุดคราก (Yield Strength: F_y) มีค่าไม่น้อยกว่า 2,350 กก./ ตร.ซม.
 - เหล็กรูปพรรณชนิด Hot-rolled of Cold rolled Mild Steel ชั้นคุณภาพ HS-41 ตามมาตรฐานอุตสาหกรรมไทย มอก.107-2533 โดยมีค่าแรงดึงที่จุดคราก (Yield Strength: F_y) มีค่าไม่น้อยกว่า 2,350 กก./ ตร.ซม.

3. น้ำหนักบรรทุกใช้งานในการออกแบบ (Design Load)

- (1) น้ำหนักบรรทุกคงที่ (Dead Load: DL)

- น้ำหนักคอนกรีต	=	2400	กก./ตร.ม.
- น้ำหนักเหล็กรูปพรรณ	=	7850	กก./ลบ.ม.
- น้ำหนักผนังก่ออิฐมวลเบา	=	100	กก./ตร.ม.
- น้ำหนักผนังก่ออิฐบล็อก	=	180	กก./ตร.ม.
- น้ำหนักผนังกระจก	=	100	กก./ตร.ม.
- น้ำหนักผนังก่ออิฐมอญเต็มแผ่น	=	360	กก./ตร.ม.
- น้ำหนักผนังก่ออิฐมอญครึ่งแผ่น	=	180	กก./ตร.ม.
- กระเบื้องยางปูพื้น	=	5	กก./ตร.ม.
- กระเบื้องเซรามิกปูพื้น	=	15-20	กก./ตร.ม.



- ฝ้าเพดานยิปซัมบอร์ดโครงเคร่าโลหะ = 30 กก./ตร.ม
- น้ำหนักเครื่องจักรฯ วัสดุอื่น ๆ ให้คำนวณจากข้อมูลจริง
- (2) น้ำหนักบรรทุกคงที่เพิ่มเติม (Superimposed Dead Load: SDL)
 - พื้นที่ลานอเนกประสงค์ = 120 กก./ตร.ม
 - พื้นที่สำนักงาน = 120 กก./ตร.ม
 - ห้องประชุม, ห้องอเนกประสงค์, ภัตตาคาร = 120 กก./ตร.ม
 - สวนบนหลังคา = 1,200 กก./ตร.ม
- (3) น้ำหนักบรรทุกจร (Live Load: LL)
 - หลังคาเบา = 50 กก./ตร.ม
 - กันสาดหรือหลังคาคอนกรีตเสริมเหล็ก = 200 กก./ตร.ม
 - พื้นที่สำนักงาน = 300 กก./ตร.ม
 - ห้องประชุม, ห้องอเนกประสงค์, ภัตตาคาร = 400 กก./ตร.ม
 - บันได ช่องทางเดินห้องประชุม, ภัตตาคาร = 500 กก./ตร.ม
 - ห้องเก็บของ (ไม่น้อยกว่า) = 500 กก./ตร.ม
 - สวนบนหลังคา = 400 กก./ตร.ม
 - ที่จอดรถยนต์ = 400 กก./ตร.ม
 - พื้นที่อาคารศูนย์ประชุม = 500 กก./ตร.ม
 - ห้องเก็บสำนวนคดี = 1,000 กก./ตร.ม
 - ห้องไฟฟ้า = 300* กก./ตร.ม
 - ห้อง AHU = 500* กก./ตร.ม
 - ห้องเครื่อง Pump = 800* กก./ตร.ม
 - ห้องหม้อแปลง, เครื่องกำเนิดไฟฟ้า, Chiller, Cooling Tower = 2,000* กก./ตร.ม
 - ห้องเครื่องลิฟต์ = 2,000* กก./ตร.ม

หมายเหตุ น้ำหนักบรรทุกจร * ที่เสนอจะต้องตรวจสอบอีกครั้งเมื่อมีข้อมูลน้ำหนักที่แท้จริงของอุปกรณ์แล้ว

(4) แรงลม (Wind Load, WL)

- 4.1 ตามข้อบัญญัติกรุงเทพมหานคร เรื่องควบคุมอาคาร พ.ศ. 2544 กำหนดให้ค่าหน่วยแรงลมออกแบบมีความสัมพันธ์กับความสูงของอาคารและมีค่าไม่น้อยกว่าค่าที่ระบุในตารางต่อไปนี้

ความสูงของอาคารหรือส่วนของอาคาร	หน่วยแรงลมอย่างน้อย กิโลกรัมต่อตารางเมตร
ส่วนของอาคารที่สูงไม่เกิน 10 เมตร	50
ส่วนของอาคารที่สูงกว่า 10 เมตร แต่ไม่เกิน 20 เมตร	80
ส่วนของอาคารที่สูงกว่า 20 เมตร แต่ไม่เกิน 40 เมตร	120
ส่วนของอาคารที่สูงเกิน 40 เมตร แต่ไม่เกิน 80 เมตร	160
ส่วนของอาคารที่สูงเกินกว่า 80 เมตร	200

4.2 ตามมาตรฐานการคำนวณแรงลมและการตอบสนองของอาคาร (มยผ. 1311-50)

(5) การลดน้ำหนักบรรทุกของอาคาร

ในการคำนวณน้ำหนักที่ถ่ายลงเสาและฐานราก ให้ใช้น้ำหนักของอาคารเต็มอัตราจริงส่วนน้ำหนักบรรทุก (Live Load) ให้ลดส่วนลงได้ตามชั้นของอาคารดังต่อไปนี้

ตารางที่ 1 อัตราการลดน้ำหนักบรรทุกบนพื้นแต่ละชั้นของอาคาร

การรับน้ำหนักของพื้น	อัตราการลดน้ำหนักบรรทุก บนพื้นแต่ละชั้นเป็นร้อยละ
หลังคาหรือดาดฟ้า	0
ชั้นที่หนึ่งถัดจากหลังคาหรือดาดฟ้า	0
ชั้นที่สองถัดจากหลังคาหรือดาดฟ้า	0
ชั้นที่สามถัดจากหลังคาหรือดาดฟ้า	10
ชั้นที่สี่ถัดจากหลังคาหรือดาดฟ้า	20
ชั้นที่ห้าถัดจากหลังคาหรือดาดฟ้า	30
ชั้นที่หกถัดจากหลังคาหรือดาดฟ้า	40
ชั้นที่เจ็ดถัดจากหลังคาหรือดาดฟ้า และชั้นต่อไป	50



สำหรับห้องประชุม, ห้องเอนกประสงค์, ห้องเก็บของ, ที่จอดรถยนต์ให้คิदनน้ำหนักบรรทุกเต็มอัตราทุกชั้น

(6) แรงแผ่นดินไหว (Earthquake Load, E)

ตามกฎหมายกระทรวง พ.ศ. 2550 ได้กำหนดการรับน้ำหนัก ความต้านทาน ความคงทนของอาคาร และพื้นดินที่รองรับอาคารในการต้านแรงสั่นสะเทือนของแผ่นดินไหว ตามความในพระราชบัญญัติควบคุมอาคาร พ.ศ. 2522 และมีผลบังคับใช้ตั้งแต่วันที่ 30 พฤศจิกายน 2550 ซึ่งกฎหมายดังกล่าวได้แก้ไขเพิ่มเติมและยกเลิกกฎหมายฉบับที่ 49 (พ.ศ. 2540) ตามความในพระราชบัญญัติควบคุมอาคาร พ.ศ. 2522 ว่าด้วยการออกแบบโครงสร้าง จะต้องออกแบบรับแรงแผ่นดินไหว เนื่องจากโครงการอยู่ในเขตที่อาคารออกแบบอาคารรับ

แรงเนื่องจากแผ่นดินไหว ซึ่งตามกฎกระทรวงที่กำหนดให้พื้นที่หรือบริเวณเฝ้าระวัง บริเวณที่ 1 และบริเวณที่ 2 สำหรับอาคารที่จำเป็นต่อความเป็นอยู่ของสาธารณชนจะต้องออกแบบโครงสร้างต้านทานแรงแผ่นดินไหว

“บริเวณเฝ้าระวัง” หมายถึง พื้นที่หรือบริเวณที่อาจได้รับผลกระทบจากแผ่นดินไหว ได้แก่ จังหวัดกระบี่ จังหวัดชุมพร จังหวัดพังงา จังหวัดภูเก็ต จังหวัดระนอง จังหวัดสงขลา และ จังหวัดสุราษฎร์ธานี

“บริเวณที่ 1” หมายถึง พื้นที่หรือบริเวณที่เป็นดินอ่อนมากที่อาจได้รับผลกระทบจากแผ่นดินไหวระยะไกล ได้แก่ กรุงเทพมหานคร จังหวัดนนทบุรี จังหวัดปทุมธานี จังหวัดสมุทรปราการ และจังหวัดสมุทรสาคร

“บริเวณที่ 2” หมายถึง พื้นที่หรือบริเวณที่อยู่ใกล้รอยเลื่อนที่อาจได้รับผลกระทบจากแผ่นดินไหว ได้แก่ จังหวัดกาญจนบุรี จังหวัดเชียงราย จังหวัดเชียงใหม่ จังหวัดตาก จังหวัดน่าน จังหวัดพะเยา จังหวัดแพร่ จังหวัดแม่ฮ่องสอน จังหวัดลำปาง และจังหวัดลำพูน

ซึ่งโครงการก่อสร้างนี้ตั้งอยู่ในจังหวัดกรุงเทพมหานคร เป็นเขตเสี่ยงต่อแผ่นดินไหวอยู่ในบริเวณที่ 1 จำเป็นต้องออกแบบระบบโครงสร้างที่คำนึงถึง แรงเนื่องจากแผ่นดินไหวด้วย โดยการออกแบบอาคารให้อ้างอิงตามมาตรฐานประกอบการออกแบบอาคารเพื่อต้านทานสั่นสะเทือนของแผ่นดินไหว ปี พ.ศ. 2552 (มยผ. 1302-52) , ปี พ.ศ. 2554 (มยผ. 1301-54) และ ปี พ.ศ. 2561 (มยผ. 1301/1302-61)

(7) แรงเนื่องจากการทรุดตัวที่แตกต่างกัน (Differential Settlement, S)

เป็นแรงกระทำต่อโครงสร้างเนื่องจากการทรุดตัวที่แตกต่างกันของฐานรากอาคาร ซึ่งในการออกแบบโครงสร้างอาคารนี้จะพิจารณาถึงผลอันเนื่องมาจากการทรุดตัวที่แตกต่างกันของฐานรากที่ไม่ก่อให้เกิดการแตกร้าวของโครงสร้างอาคาร

(8) แรงดันดิน (H)

เป็นแรงกระทำต่อโครงสร้างทางด้านข้างในการออกแบบโครงสร้างอาคารจะพิจารณาถึงผลกระทบที่เกิดจากแรงดันดินดังกล่าว ดังนี้

For Sand or Sandy Clay

$K_a = \tan^2 (45 - \phi/2)$ Coefficient to active earth pressure.

$K_o = \tan^2 (45 + \phi/2)$ Coefficient of passive earth pressure.

$K_p = 1 - \sin \phi$ Coefficient of earth pressure at rest.

ϕ = Angle of internal friction



For clay, $\phi = 0$

Active soil pressure, $P_a = \gamma h - 2C$

Passive soil pressure, $P_p = \gamma h + 2C$

γ = Density of Soil

C = Co-efficient of Cohesion

Unless otherwise noted, the lateral soil pressure coefficients are:

Active soil pressure coefficient, $K_a = 0.33$

At-rest soil pressure coefficient, $K_o = 0.50$

Passive soil pressure coefficient, $K_p = 3.00$

- (9) แรงเนื่องจากการเปลี่ยนแปลงของอุณหภูมิ (Temperature Change, T)
เป็นแรงกระทำที่ทำให้เกิดการยึดหดตัวของโครงสร้าง โดยการเปลี่ยนแปลงของอุณหภูมิจะอยู่ที่ ± 15 องศาเซลเซียส ในการออกแบบโครงสร้างอาคารซึ่งเป็นอาคารช่วงยาว จะพิจารณาถึงผลที่เกิดจากการเปลี่ยนแปลงของอุณหภูมิที่ไม่ก่อให้เกิดการแตกร้าวของโครงสร้างอาคาร

4. การรวมน้ำหนักบรรทุกต่าง ๆ

- (1) การออกแบบอาคารคอนกรีตเสริมเหล็กโดยวิธีกำลัง (Ultimate Strength Design) ตามกฎกระทรวงและมาตรฐาน (ACI 318)

สัญลักษณ์ (Symbols)

DL	=	ผลที่เกิดจากน้ำหนักบรรทุกคงที่ (Dead Load)
LL	=	ผลที่เกิดจากน้ำหนักบรรทุกจร (Live Load)
WL	=	ผลที่เกิดจากแรงลม (Wind Load)
E	=	ผลที่เกิดจากแรงแผ่นดินไหว (Seismic Load Effects)

กำลังที่ต้องการ

U	=	1.7DL + 2.0 LL	(กฎกระทรวงฉบับที่ 6 พ.ศ.2527)
U	=	0.75(1.7DL + 2.0LL + 2.0WL)	(กฎกระทรวงฉบับที่ 6 พ.ศ.2527)
U	=	0.90DL + 1.30WL	(กฎกระทรวงฉบับที่ 6 พ.ศ.2527)
U	=	0.75(1.7DL + 2.0LL + 2.0EQ)	(กฎกระทรวง พ.ศ.2550)
U	=	0.90DL + 1.3EQ	(กฎกระทรวง พ.ศ.2550)
U	=	1.2DL + 1.0LL + 1.0EQ	(มยพ.1302-52 และ มยพ. 1302-54)
U	=	0.75(1.4DL + 1.7LL) + 1.0EQ	(มยพ.1301/1302-61)
U	=	0.90DL + 1.0EQ	(มยพ.1302-52, มยพ. 1302-54 และ มยพ. 1301/1302-61)



$$\begin{aligned} U &= 1.4DL + 1.7 LL & (EIT 1008-38) \\ U &= 0.75(1.4DL + 1.7LL + 1.7WL) & (EIT 1008-38) \\ U &= 0.75(1.4DL + 1.7LL + 1.87EQ) & (EIT 1008-38) \\ U &= 0.90DL + 1.43EQ & (EIT 1008-38) \end{aligned}$$

ตัวคูณลดกำลัง (Strength Reduction Factor)

- สำหรับแรงดัด	0.90
- สำหรับแรงเฉือนและแรงบิด	0.85
- สำหรับแรงอัดตามแนวแกน, เหล็กปลอกเดี่ยว	0.70
- สำหรับแรงอัดตามแนวแกน, เหล็กปลอกเกลียว	0.75

Flexural Strength Design

$$\rho_b = 0.85 \times \beta_1 \times \frac{f_c'}{f_y} \times \frac{6120}{(6120 + f_y)}$$

$$\beta_1 = 0.85 - 0.05 \times \frac{(f_c' - 280)}{70}; \beta_1 < 0.85$$

$$\rho_{max} = 0.75\rho_b$$

$$\rho_{min} = \frac{14}{f_y} \quad ; \text{ for beam and footing}$$

$$= 0.0018 \quad ; \text{ for slab where Grade SD40 deformed bars are used}$$

$$= 0.0025 \quad ; \text{ for slab where Grade SR24 round bars are used}$$

$$R = 0.75\rho_b f_y \left(1 - 0.44\rho_b \frac{f_y}{f_c'} \right)$$

$$\phi M_n = \phi R b d^2$$

For single reinforcement: ($M_u < \phi M_n$)

$$\rho = 0.85 \frac{f_c'}{f_y} \times \left(1 - \sqrt{1 - \frac{236M_u}{\phi b d^2 f_c'}} \right)$$



Shear Strength Design

For beam shear strength

$$V_c = 0.53\sqrt{f_c'} \cdot b \cdot d$$

For punching shear strength

$$V_c = 1.06\sqrt{f_c'} \cdot b_o \cdot d$$

Compressive Strength Design

$$\phi V_n = 0.80\phi(0.85f_c'(A_g - A_s) + A_s f_y)$$

Where

- ϕ = Strength reduction factor
- = 0.90 for flexure
- = 0.85 for shear
- = 0.70 for axial compression

Where

- A_g = Gross area of member (cm^2)
- A_s = Area of reinforcing steel (cm^2)
- M_u = Ultimate moment (kg-m)
- M_n = Nominal flexural strength (kg-m)
- P_n = Nominal Compressive strength (kg)
- R = Flexural resistance factor (kg/cm^2)
- V_u = Ultimate shear force (kg)
- V_c = Concrete shear strength (kg)
- B = member width (cm)
- b_o = Critical perimeter (cm)
- d = Effective depth of member (cm)
- f_c' = Compressive strength of concrete (kg/cm^2)
- f_y = Yield strength of reinforcing steel (kg/cm^2)
- h = Depth of member (cm)
- β_1 = Concrete stress block parameter
- ρ = Reinforcement ratio = $A_s / b \cdot d$
- ρ_b = Balanced steel ratio



- (2) การออกแบบโครงสร้างเหล็กโดยวิธีหน่วยแรงที่ยอมให้ (Allowable Stress Design-ASD) ตามกฎกระทรวงและมาตรฐาน (AISC)

สัญลักษณ์ (Symbols)

DL	=	ผลที่เกิดจากน้ำหนักบรรทุกคงที่ (Dead Load)
LL	=	ผลที่เกิดจากน้ำหนักบรรทุกจร (Live Load)
WL	=	ผลที่เกิดจากแรงลม (Wind Load)
E	=	ผลที่เกิดจากแรงแผ่นดินไหว (Seismic Load Effects)

กำลังที่ต้องการ

U	=	DL + LL
U	=	0.75(DL + LL + WL)
U	=	0.75(DL + LL + EQ)
U	=	1.0DL + 0.7EQ (มยพ.1302-52 และ มยพ. 1301/1302-61)
U	=	1.0DL + 0.75LL + 0.525EQ (มยพ.1302-52 และ มยพ. 1301/1302-61)
U	=	0.6DL + 0.7EQ (มยพ.1302-52 และ มยพ. 1301/1302-61)

Allowable Flexural Stress

1. Members with Unbraced length not exceed the value of L_c

$$F_b = 0.66F_y$$

$$\text{Where } L_c = \frac{637b_f}{\sqrt{F_y}} \quad \text{or} \quad \frac{1406000}{(d/A_f)F_y}$$

Whichever is smaller



2. Members with Unbraced length greater than L_c

$$\text{When } \sqrt{\frac{717 \times 10^4 C_b}{F_y}} < \frac{I}{r_T} < \sqrt{\frac{3585 \times 10^4 C_b}{F_y}}$$

$$F_b = \left(\frac{2}{3} - \frac{F_y(I/r_T)^2}{10755 \times 10^4 C_b} \right) F_y < 0.60F_y$$

$$\text{When } \frac{I}{r_T} = \sqrt{\frac{3585 \times 10^4 C_b}{F_y}}$$

$$F_b = \frac{1195 \times 10^4 C_b F_y}{(I/r_T)^2} < 0.60F_y$$

F_t	=	Allowable axial tensile stress (kg/cm^2)
F_v	=	Allowable shear stress (kg/cm^2)
F_y	=	Specified minimum yield stress of the type of steel being used (kg/cm^2)
K	=	Effective length factor
b_f	=	Flange width of rolled beam (cm)
d	=	depth of beam (cm)
l	=	Unbraced length of member (cm)
r	=	radius of gyration (cm)
r_T	=	radius of gyration of a section comprising the compression flange plus 1/3 of the compression web area, taken about an axis in the plane of the web (cm).





รายงานการออกแบบ Design Note รายการคำนวณงานโครงสร้าง

(สัญญาก่อสร้างอาคารทิศตะวันตก Final Detailed Design)

(ส่วนงานโครงสร้าง งานสถาปัตยกรรม และงานระบบหลัก)

โครงการพัฒนาพื้นที่ส่วนขยายศูนย์ราชการเฉลิมพระเกียรติ ๘๐ พรรษา ๕ ธันวาคม ๒๕๕๐ พื้นที่โซน C

2. รายการคำนวณเสา, กำแพง



DYNAMIC ENGINEERING CONSULTANT CO., LTD.

Column Whit Axial Force and Moment X - X

(Ultimate Stress Design method in accordance with ACI 318)

Job No. : 193018

Rev. : 0

Initial : CKJ

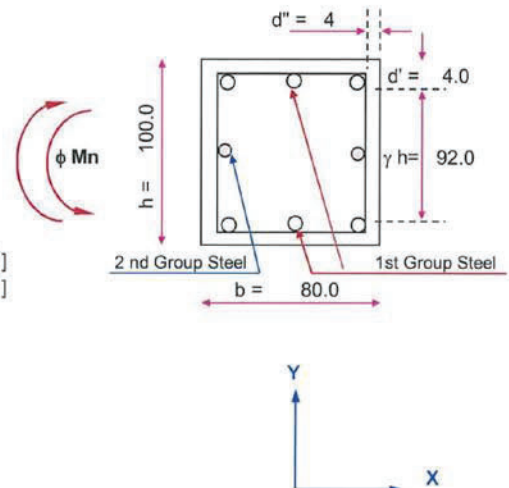
Date : 23-Dec-20

Column No. C-1 1st

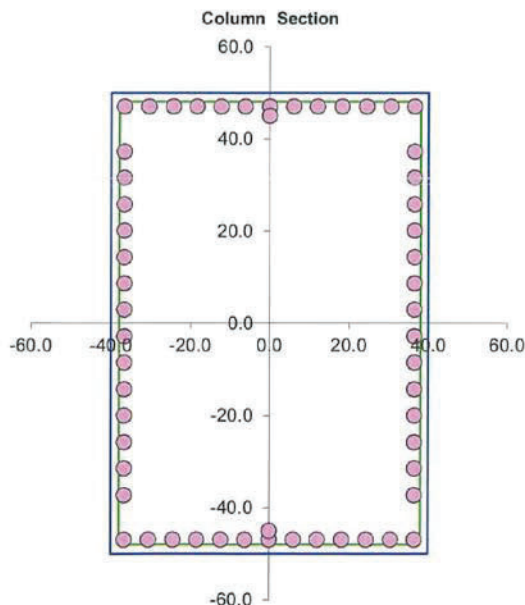
Project : อาคารทิศตะวันตก

filename : COLUMN

Concrete Strength	f_c'	=	350	[kg/cm ²]
	f_y SD	=	4000	[kg/cm ²]
	f_y RD	=	2400	[kg/cm ²]
Column Dimension	b	=	80	[cm]
	h	=	100	[cm]
	d'	=	4	[cm]
	d''	=	4	[cm]
Load	ϕP_n	=	1550	[T]
Moment	ϕM_n	=	155	[T-m]
Separate Steel 2 group	1 st.	=	28	$A_s = 172.4$ [cm ²]
	2 nd.	=	28	$A_s = 172.4$ [cm ²]
Steel Reinforcement	No.	=	56	
	d	=	96	[cm]
	C_b	=	58.055	[cm]
	ρ of Steel	=	0.043	OK
Main Steel Used	56 DB 28			DB 28
Stirrup	DB 12 @ 0.400			DB 12
e_b	=	0.47		[cm]

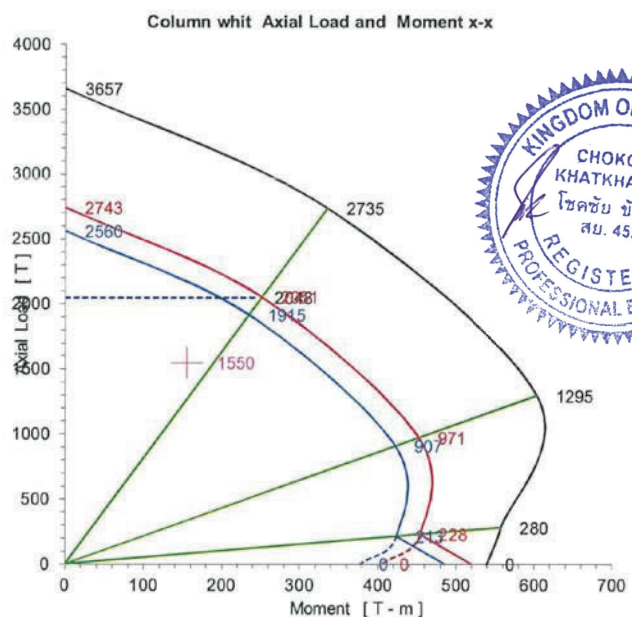


Column (80 x 100)
Steel 56 DB 28
Stirrup DB 12 @ 0.400



Column C-1 (80 x 100)

Boundary of tie stirrup Column
Boundary of spiral stirrup Column
Boundary of Ultimate Capacity



DYNAMIC ENGINEERING CONSULTANT CO., LTD.

Column Whit Axial Force and Moment X - X

(Ultimate Stress Design method in accordance with ACI 318)

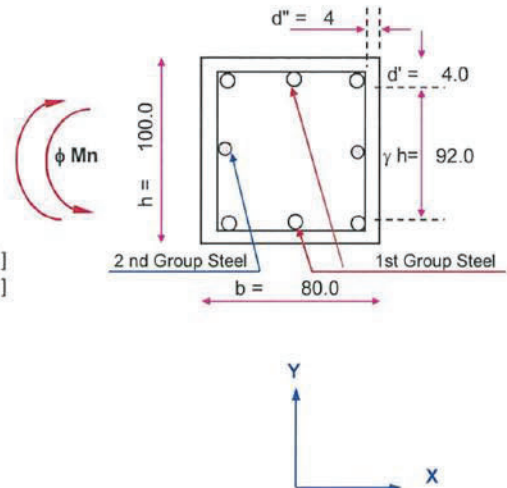
Job No. : 193018
Rev. : 0
Initial : CKJ
Date : 23-Dec-20

Column No. C-1 2nd-3rd

Project : อาคารทิศตะวันตก

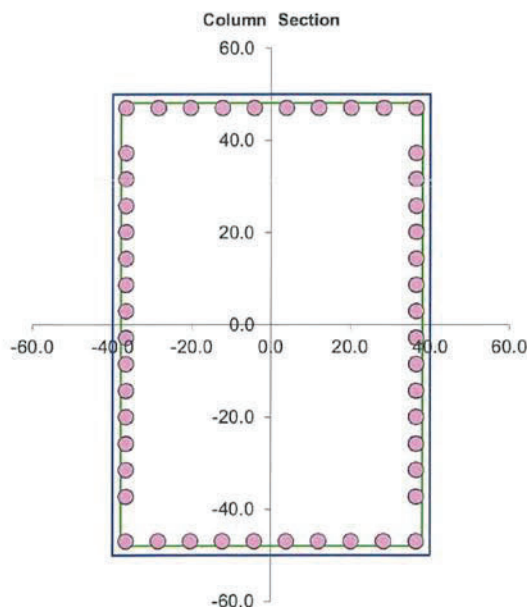
filename : COLUMN

Concrete Strength	f_c' =	350	[kg/cm ²]
	f_y SD =	4000	[kg/cm ²]
	f_y RD =	2400	[kg/cm ²]
Column Dimension	b =	80	[cm]
	h =	100	[cm]
	d' =	4	[cm]
	d'' =	4	[cm]
Load	ϕP_n =	1450	[T]
Moment	ϕM_n =	145	[T-m]
Separate Steel 2 group	1 st. =	20	$A_s = 123.2$ [cm ²]
	2 nd. =	28	$A_s = 172.4$ [cm ²]
Steel Reinforcement	No. =	48	
	d =	96	[cm]
$d(eu/(ey+eu))$	C_b =	58.055	[cm]
	ρ of Steel =	0.037	OK
Main Steel Used	48 DB 28		DB 28
Stirrup	DB 12 @ 0.400		DB 12
e/b =	0.40	[cm]	

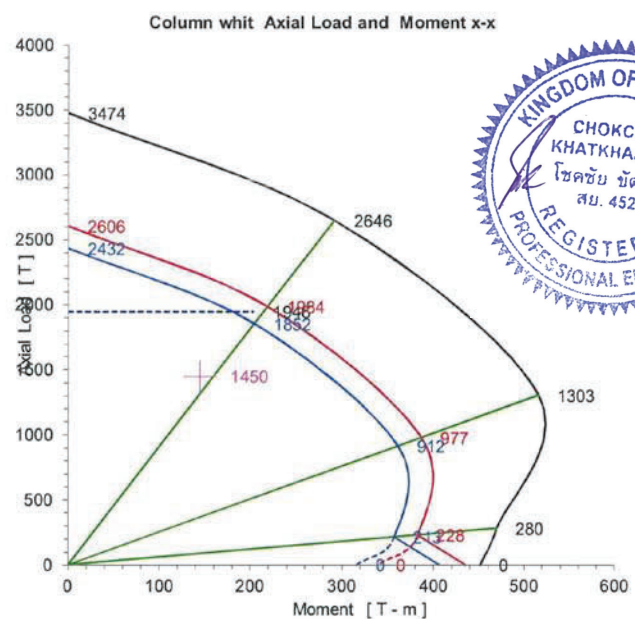


Column (80 x 100)
Steel 48 DB 28
Stirrup DB 12 @ 0.400

— Boundary of tie stirrup Column
— Boundary of spiral stirrup Column
— Boundary of Ultimate Capacity



Column C-1 (80 x 100)



DYNAMIC ENGINEERING CONSULTANT CO., LTD.

Column Whit Axial Force and Moment X - X

(Ultimate Stress Design method in accordance with ACI 318)

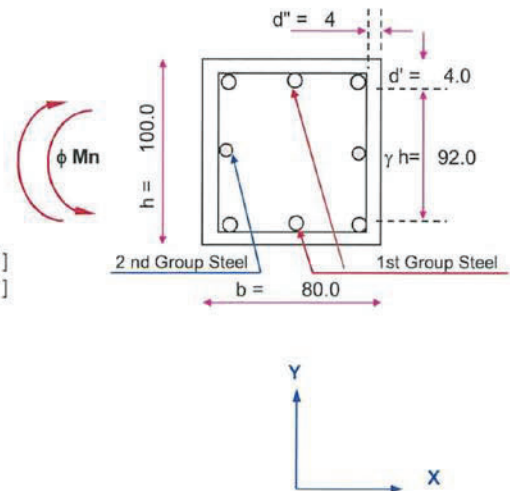
Job No. : 193018
Rev. : 0
Initial : CKJ
Date : 23-Dec-20

Column No. C-1 4th-5th

Project : อาคารทิศตะวันตก

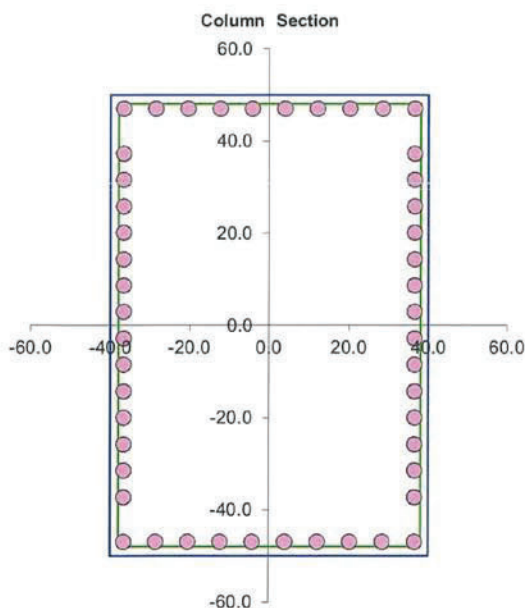
filename : COLUMN

Concrete Strength	f_c' =	350	[kg/cm ²]
	f_y SD =	4000	[kg/cm ²]
	f_y RD =	2400	[kg/cm ²]
Column Dimension	b =	80	[cm]
	h =	100	[cm]
	d' =	4	[cm]
	d'' =	4	[cm]
Load	ϕP_n =	1180	[T]
Moment	ϕM_n =	118	[T-m]
Separate Steel 2 group	1 st. =	20	$A_s = 98.2$ [cm ²]
	2 nd. =	28	$A_s = 137.4$ [cm ²]
Steel Reinforcement	No. =	48	
	d =	96	[cm]
	C_b =	58.055	[cm]
	p of Steel =	0.029	OK
Main Steel Used	48 DB 25		DB 25
Stirrup	RB 9 @ 0.400		RB 9
e b =	0.37		[cm]

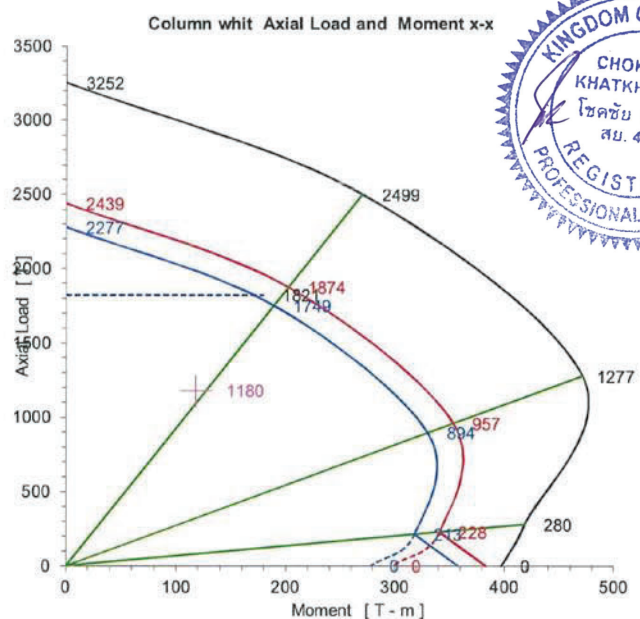


Column (80 x 100)
Steel 48 DB 25
Stirrup RB 9 @ 0.400

Boundary of tie stirrup Column
Boundary of spiral stirrup Column
Boundary of Ultimate Capacity



Column C-1 (80 x 100)



DYNAMIC ENGINEERING CONSULTANT CO., LTD.

Column Whit Axial Force and Moment X - X

(Ultimate Stress Design method in accordance with ACI 318)

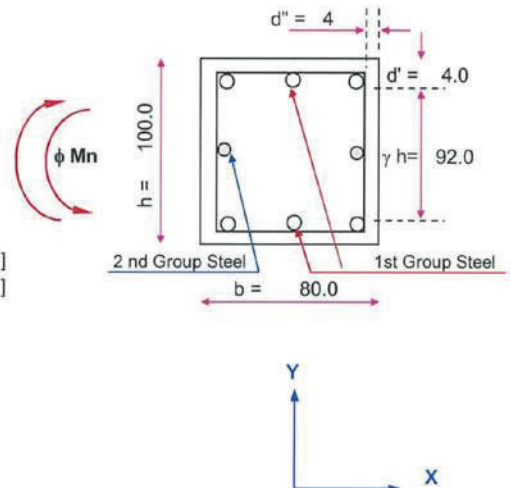
Job No. : 193018
Rev. : 0
Initial : CKJ
Date : 23-Dec-20

Column No. C-1 6th-7th

Project : อาคารทิศตะวันตก

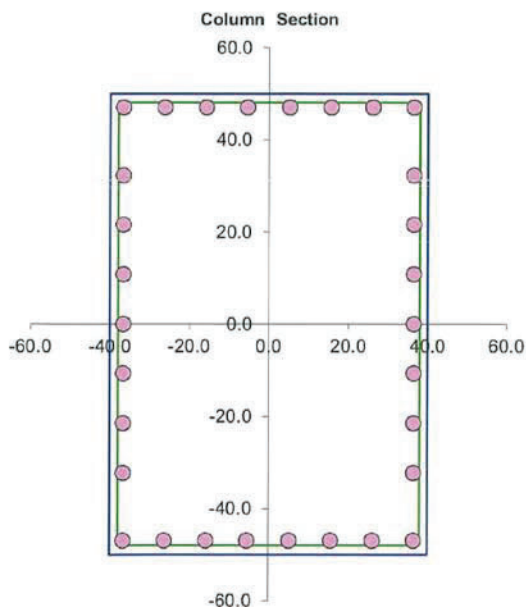
filename : COLUMN

Concrete Strength	f_c' =	350	[kg/cm ²]
	f_y SD =	4000	[kg/cm ²]
	f_y RD =	2400	[kg/cm ²]
Column Dimension	b =	80	[cm]
	h =	100	[cm]
	d' =	4	[cm]
	d'' =	4	[cm]
Load	ϕP_n =	910	[T]
Moment	ϕM_n =	91	[T-m]
Separate Steel 2 group	1 st. =	16	$A_s = 78.5$ [cm ²]
	2 nd. =	14	$A_s = 68.7$ [cm ²]
Steel Reinforcement	No. =	30	
	d =	96	[cm]
	C_b =	58.055	[cm]
	ρ of Steel =	0.018	OK
Main Steel Used	30 DB 25		DB 25
Stirrup	RB 9 @ 0.400		RB 9
e/b =	0.36		[cm]

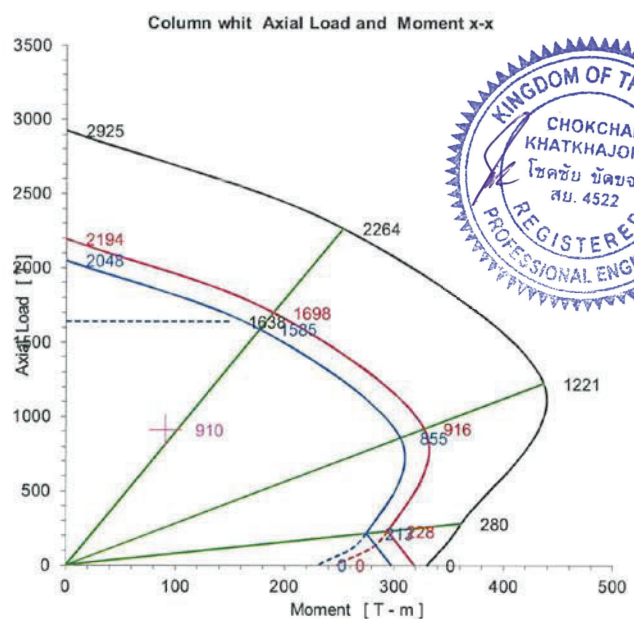


Column (80 x 100)
Steel 30 DB 25
Stirrup RB 9 @ 0.400

Boundary of tie stirrup Column
Boundary of spiral stirrup Column
Boundary of Ultimate Capacity



Column C-1 (80 x 100)



DYNAMIC ENGINEERING CONSULTANT CO., LTD.

Column Whit Axial Force and Moment X - X

(Ultimate Stress Design method in accordance with ACI 318)

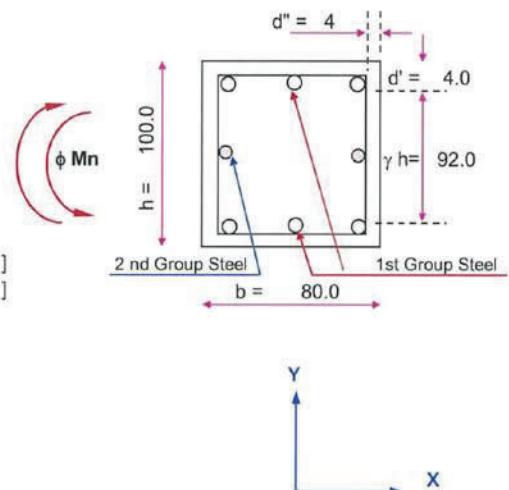
Job No. : 193018
Rev. : 0
Initial : CKJ
Date : 23-Dec-20

Column No. C-1 8th-Roof

Project : อาคารทิศตะวันตก

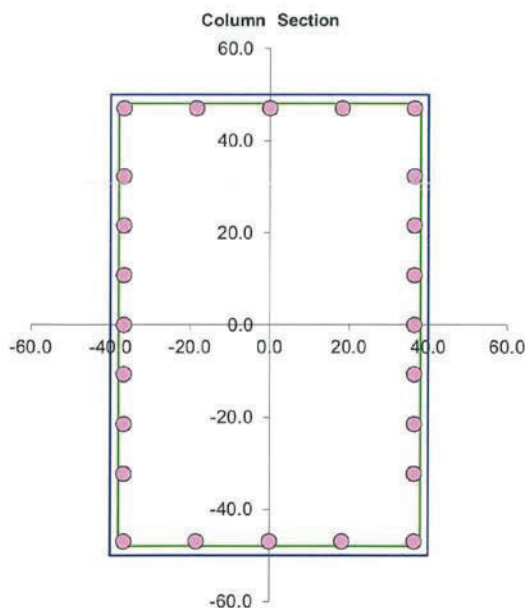
filename : COLUMN

Concrete Strength	f_c' =	350	[kg/cm ²]
	f_y SD =	4000	[kg/cm ²]
	f_y RD =	2400	[kg/cm ²]
Column Dimension	b =	80	[cm]
	h =	100	[cm]
	d' =	4	[cm]
	d'' =	4	[cm]
Load	ϕP_n =	640	[T]
Moment	ϕM_n =	64	[T-m]
Separate Steel 2 group	1 st. =	10	$A_s = 49.1$ [cm ²]
	2 nd. =	14	$A_s = 68.7$ [cm ²]
Steel Reinforcement	No. =	24	
	d =	96	[cm]
	C_b =	58.055	[cm]
$d(\epsilon_u / (\epsilon_y + \epsilon_u))$	p of Steel =	0.015	OK
Main Steel Used	24 DB 25		
Stirrup	RB 9 @ 0.400		
e_b =	0.31	[cm]	

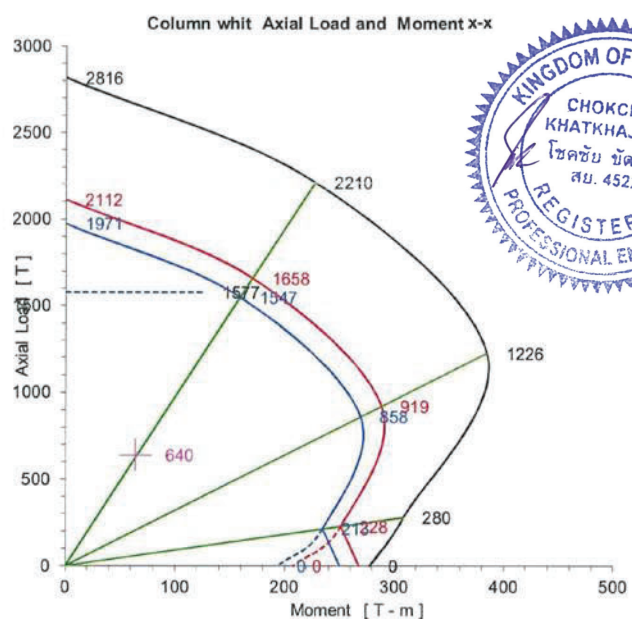


Column (80 x 100)
Steel 24 DB 25
Stirrup RB 9 @ 0.400

Boundary of tie stirrup Column
Boundary of spiral stirrup Column
Boundary of Ultimate Capacity



Column C-1 (80 x 100)



DYNAMIC ENGINEERING CONSULTANT CO., LTD.

Column Whit Axial Force and Moment X - X

(Ultimate Stress Design method in accordance with ACI 318)

Job No. : 193018
Rev. : 0
Initial : CKJ
Date : 23-Dec-20

Column No. **C-1A** 1st
Project : อาคารทิศตะวันตก

filename : COLUMN

Concrete Strength $f_c' = 350$ [kg/cm²]
 f_y SD = 4000 [kg/cm²]
 f_y RD = 2400 [kg/cm²]

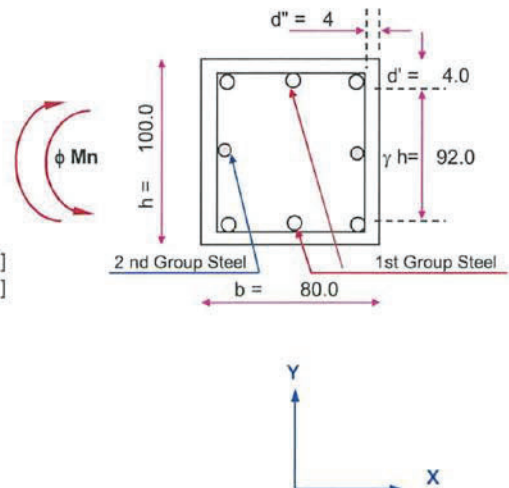
Column Dimension $b = 80$ [cm]
 $h = 100$ [cm]
 $d' = 4$ [cm]
 $d'' = 4$ [cm]

Load $\phi P_n = 1250$ [T]
Moment $\phi M_n = 125$ [T-m]

Separate Steel 2 group 1 st. = 20 $A_s = 123.2$ [cm²]
2 nd. = 14 $A_s = 86.2$ [cm²]

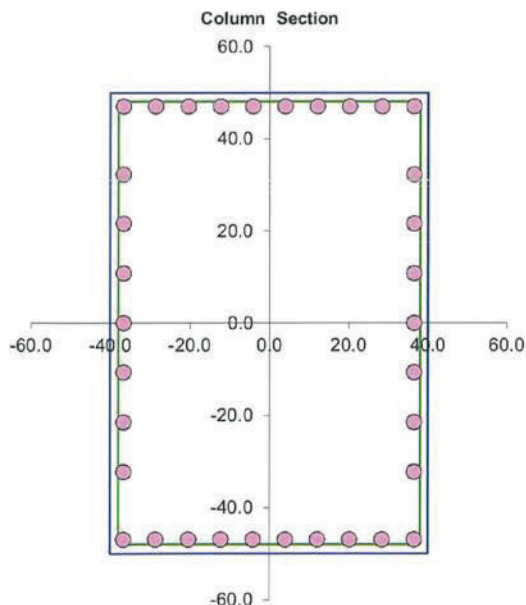
Steel Reinforcement No. = 34
 $d = 96$ [cm]
 $C_b = 58.055$ [cm]
 ρ of Steel = 0.026 OK

Main Steel Used 34 DB 28
Stirrup DB 12 @ 0.400
e b = 0.42 [cm]

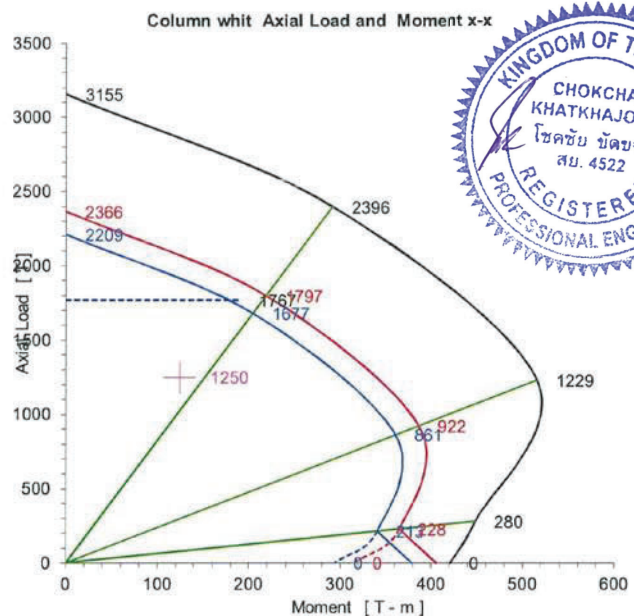


Column (80 x 100)
Steel 34 DB 28
Stirrup DB 12 @ 0.400

— Boundary of tie stirrup Column
— Boundary of spiral stirrup Column
— Boundary of Ultimate Capacity



Column C-1A (80 x 100)



DYNAMIC ENGINEERING CONSULTANT CO., LTD.

Column Whit Axial Force and Moment X - X

(Ultimate Stress Design method in accordance with ACI 318)

Job No. : 193018

Rev. : 0

Initial : CKJ

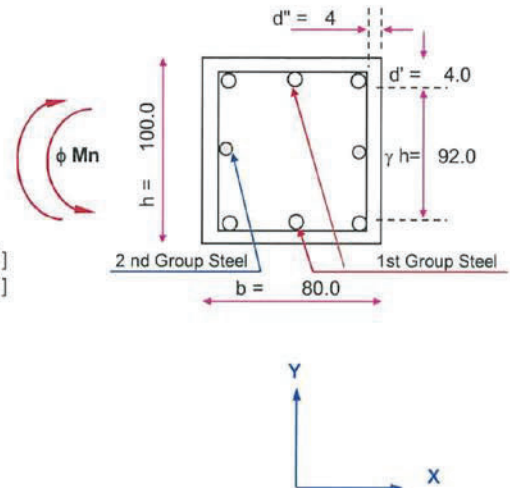
Date : 23-Dec-20

Column No. C-1A 2nd-3rd

Project : อาคารทิศตะวันตก

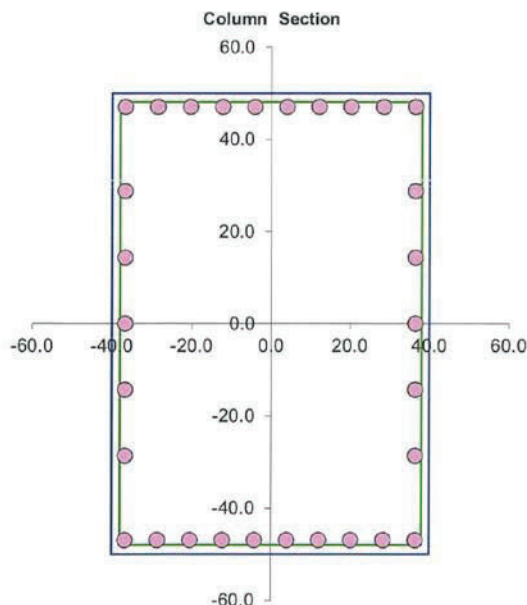
filename : COLUMN

Concrete Strength	$f_c' =$	350	[kg/cm ²]
	f_y SD	4000	[kg/cm ²]
	f_y RD	2400	[kg/cm ²]
Column Dimension	$b =$	80	[cm]
	$h =$	100	[cm]
	$d' =$	4	[cm]
	$d'' =$	4	[cm]
Load	$\phi P_n =$	1145	[T]
Moment	$\phi M_n =$	115	[T-m]
Separate Steel 2 group	1 st.	20	$A_s = 123.2$ [cm ²]
	2 nd.	10	$A_s = 61.6$ [cm ²]
Steel Reinforcement	No.	30	
	$d =$	96	[cm]
	$C_b =$	58.055	[cm]
	ρ of Steel	0.023	OK
Main Steel Used	30 DB 28		DB 28
Stirrup	DB 12 @ 0.400		DB 12
$e_b =$	0.43	[cm]	

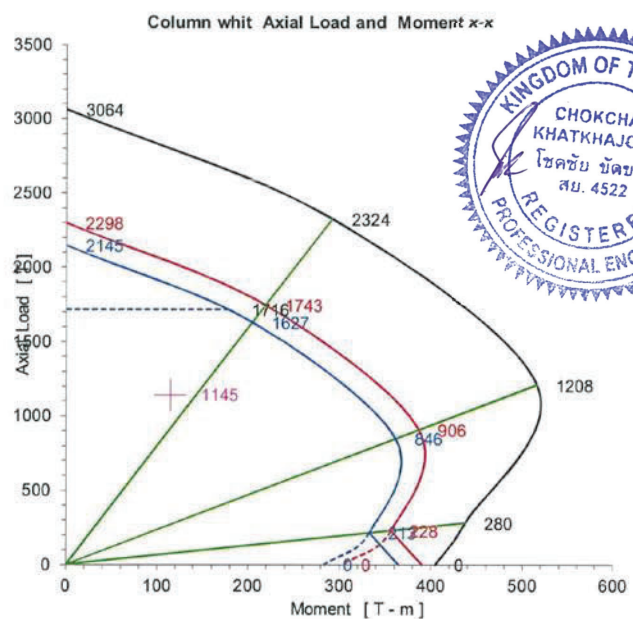


Column (80 x 100)
Steel 30 DB 28
Stirrup DB 12 @ 0.400

— Boundary of tie stirrup Column
— Boundary of spiral stirrup Column
— Boundary of Ultimate Capacity



Column C-1A (80 x 100)



DYNAMIC ENGINEERING CONSULTANT CO., LTD.

Column Whit Axial Force and Moment X - X

(Ultimate Stress Design method in accordance with ACI 318)

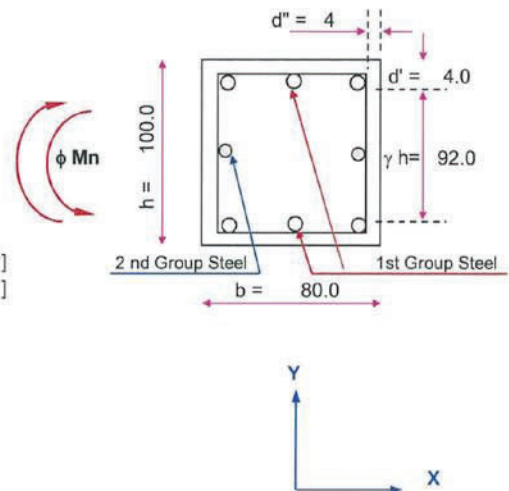
Job No. : 193018
Rev. : 0
Initial : CKJ
Date : 23-Dec-20

Column No. C-1A 4th-5th

Project : อาคารทิศตะวันตก

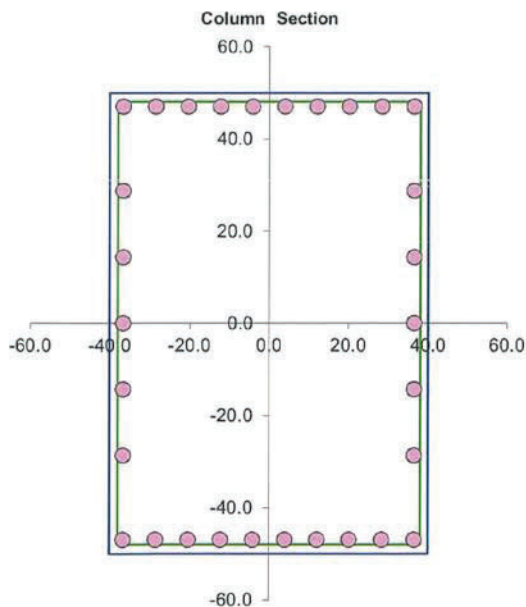
filename : COLUMN

Concrete Strength	f_c' =	350	[kg/cm ²]
	f_y SD =	4000	[kg/cm ²]
	f_y RD =	2400	[kg/cm ²]
Column Dimension	b =	80	[cm]
	h =	100	[cm]
	d' =	4	[cm]
	d'' =	4	[cm]
Load	ϕP_n =	1045	[T]
Moment	ϕM_n =	105	[T-m]
Separate Steel 2 group	1 st. =	20	$A_s = 98.2$ [cm ²]
	2 nd. =	10	$A_s = 49.1$ [cm ²]
Steel Reinforcement	No. =	30	
	d =	96	[cm]
	C_b =	58.055	[cm]
$d(e_u / (e_y + e_u))$	p of Steel =	0.018	OK
Main Steel Used	30 DB 25		DB 25
Stirrup	RB 9 @ 0.400		RB 9
e_b =	0.39	[cm]	

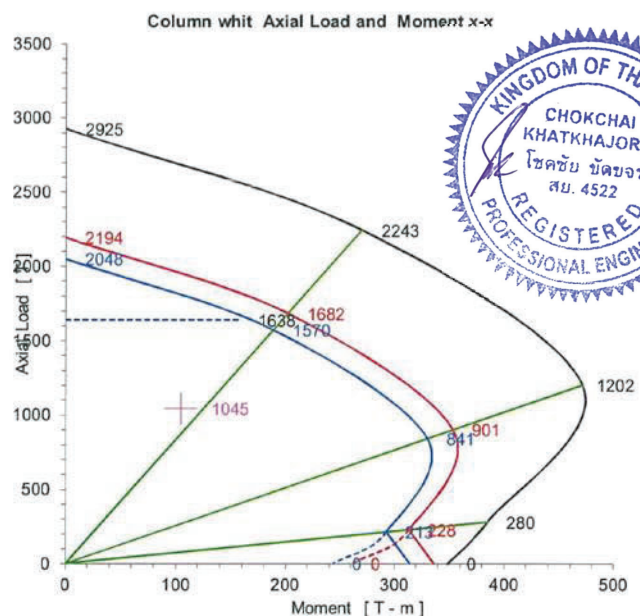


Column (80 x 100)
Steel 30 DB 25
Stirrup RB 9 @ 0.400

Boundary of tie stirrup Column
Boundary of spiral stirrup Column
Boundary of Ultimate Capacity



Column C-1A (80 x 100)



DYNAMIC ENGINEERING CONSULTANT CO., LTD.

Column Whit Axial Force and Moment X - X

(Ultimate Stress Design method in accordance with ACI 318)

Job No. : 193018

Rev. : 0

Initial : CKJ

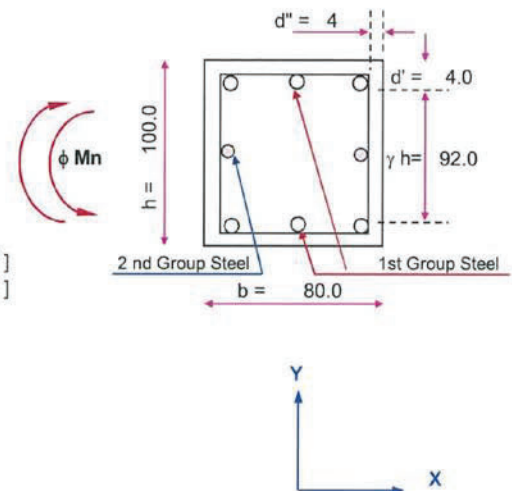
Date : 23-Dec-20

Column No. : C-1A 6th-7th

Project : อาคารทิศตะวันตก

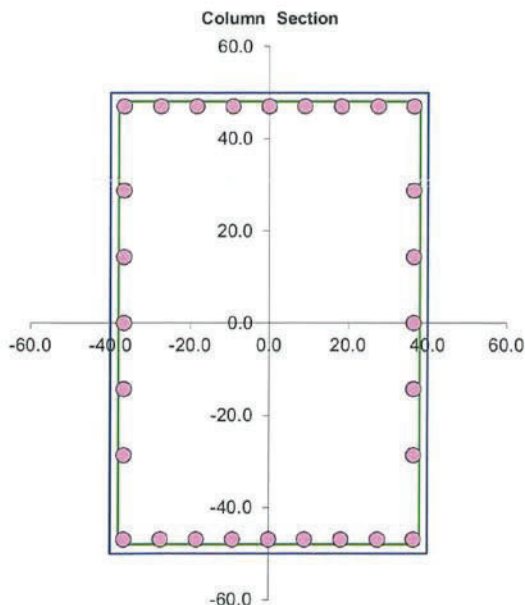
filename : COLUMN

Concrete Strength	f_c' =	350	[kg/cm ²]
	f_y SD =	4000	[kg/cm ²]
	f_y RD =	2400	[kg/cm ²]
Column Dimension	b =	80	[cm]
	h =	100	[cm]
	d' =	4	[cm]
	d'' =	4	[cm]
Load	ϕP_n =	830	[T]
Moment	ϕM_n =	83	[T-m]
Separate Steel 2 group	1 st. =	18	$A_s = 88.4$ [cm ²]
	2 nd. =	10	$A_s = 49.1$ [cm ²]
Steel Reinforcement	No. =	28	
	d =	96	[cm]
	C_b =	58.055	[cm]
	p of Steel =	0.017	OK
Main Steel Used	28 DB 25		
Stirrup	RB 9 @ 0.400		
e_b =	0.38	[cm]	

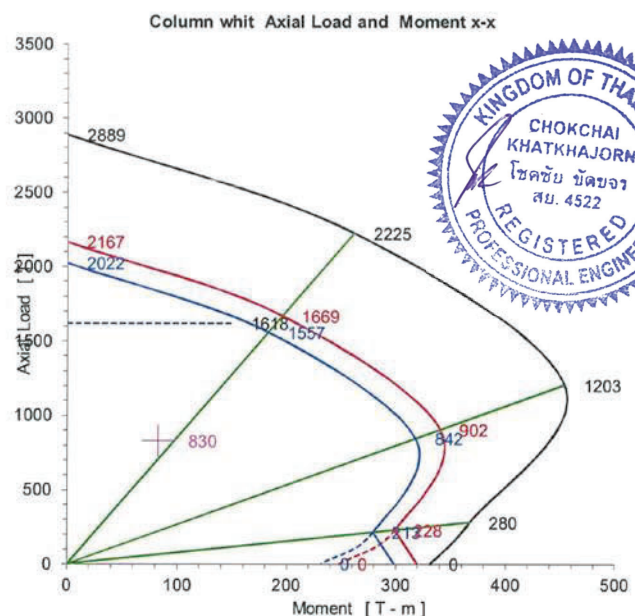


Column (80 x 100)
Steel 28 DB 25
Stirrup RB 9 @ 0.400

— Boundary of tie stirrup Column
— Boundary of spiral stirrup Column
— Boundary of Ultimate Capacity



Column C-1A (80 x 100)



DYNAMIC ENGINEERING CONSULTANT CO., LTD.

Column Whit Axial Force and Moment X - X

(Ultimate Stress Design method in accordance with ACI 318)

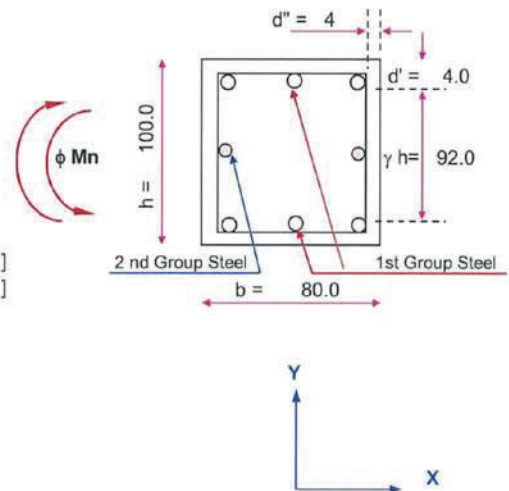
Job No. : 193018
Rev. : 0
Initial : CKJ
Date : 23-Dec-20

Column No. C-1A 8th-Roof

Project : อาคารทิศตะวันตก

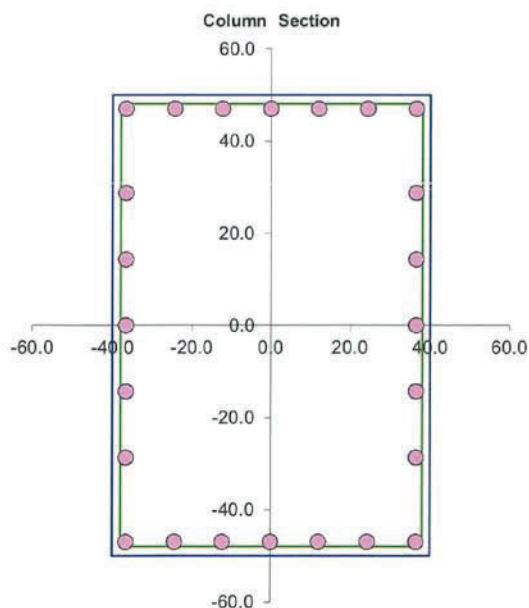
filename : COLUMN

Concrete Strength	f_c' =	350	[kg/cm ²]
	f_y SD =	4000	[kg/cm ²]
	f_y RD =	2400	[kg/cm ²]
Column Dimension	b =	80	[cm]
	h =	100	[cm]
	d' =	4	[cm]
	d'' =	4	[cm]
Load	ϕP_n =	518	[T]
Moment	ϕM_n =	52	[T-m]
Separate Steel 2 group	1 st. =	14	$A_s = 68.7$ [cm ²]
	2 nd. =	10	$A_s = 49.1$ [cm ²]
Steel Reinforcement	No. =	24	
	d =	96	[cm]
	C_b =	58.055	[cm]
$d(\epsilon_u / (\epsilon_y + \epsilon_u))$	p of Steel =	0.015	OK
Main Steel Used	24 DB 25		DB 25
Stirrup	RB 9 @ 0.400		RB 9
e_b =	0.35	[cm]	

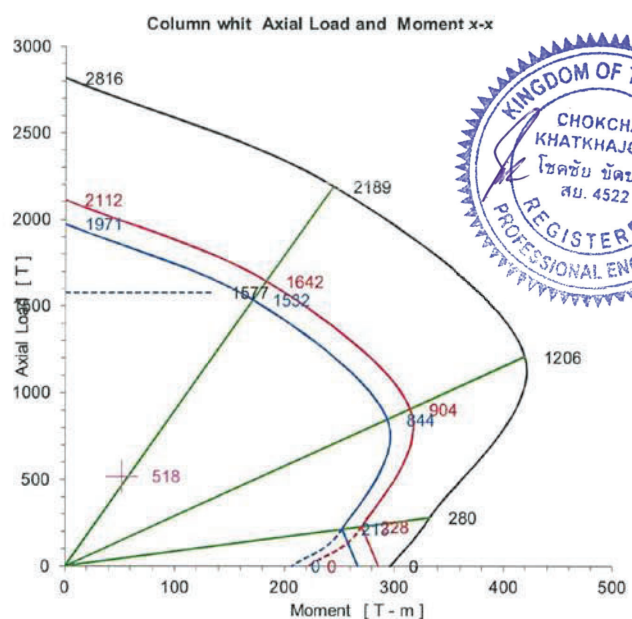


Column (80 x 100)
Steel 24 DB 25
Stirrup RB 9 @ 0.400

Boundary of tie stirrup Column
Boundary of spiral stirrup Column
Boundary of Ultimate Capacity



Column C-1A (80 x 100)



DYNAMIC ENGINEERING CONSULTANT CO., LTD.

Column Whit Axial Force and Moment X - X

(Ultimate Stress Design method in accordance with ACI 318-89)

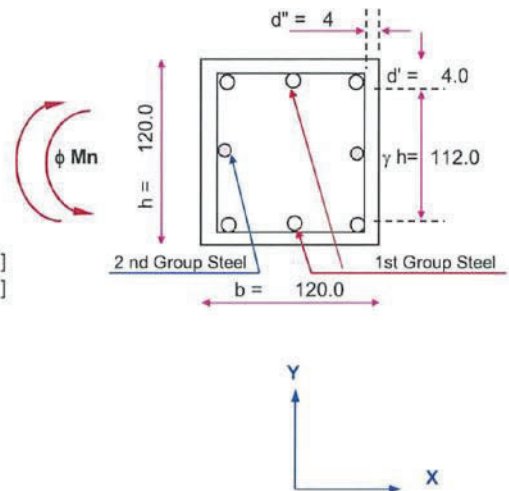
Job No. : 193018
Rev. : 0
Initial : CKJ
Date : 23-Dec-20

Column No. C-2 1st-2nd

Project : อาคารทิศตะวันตก

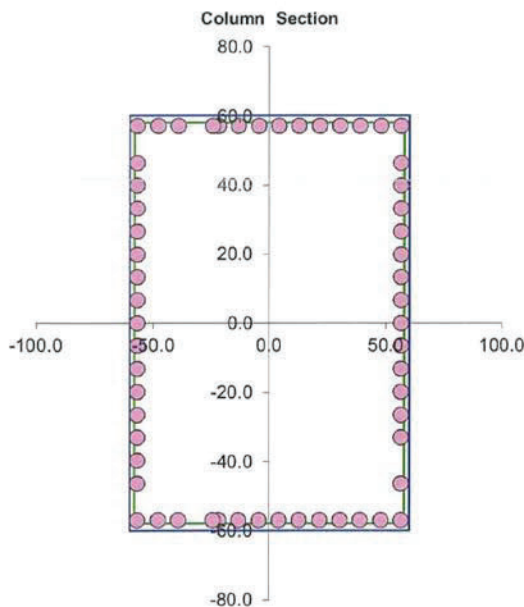
filename : COLUMN

Concrete Strength	$f_c' =$	350	[kg/cm ²]
	f_y SD	4000	[kg/cm ²]
	f_y RD	2400	[kg/cm ²]
Column Dimension	$b =$	120	[cm]
	$h =$	120	[cm]
	$d' =$	4	[cm]
	$d'' =$	4	[cm]
Load	$\phi P_n =$	2867	[T]
Moment	$\phi M_n =$	286	[T-m]
Separate Steel 2 group	1 st.	28	$A_s = 172.4$ [cm ²]
	2 nd.	36	$A_s = 221.7$ [cm ²]
Steel Reinforcement	No.	64	
	$d =$	116	[cm]
	$C_b =$	70.150	[cm]
$d(\epsilon_u / (\epsilon_y + \epsilon_u))$	p of Steel	0.027	OK
Main Steel Used	64 DB 28		DB 28
Stirrup	DB 12 @ 0.400		DB 12
$e_b =$	0.44		[cm]

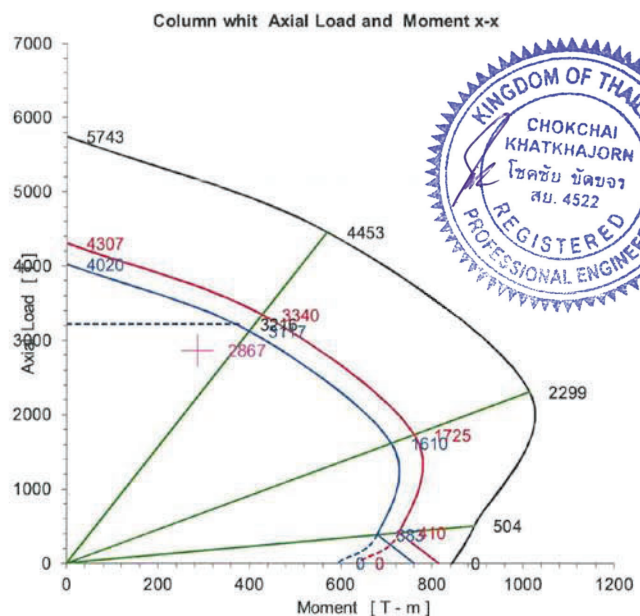


Column (120 x 120)
Steel 64 DB 28
Stirrup DB 12 @ 0.400

— Boundary of tie stirrup Column
— Boundary of spiral stirrup Column
— Boundary of Ultimate Capacity



Column C-2 (120 x 120)



DYNAMIC ENGINEERING CONSULTANT CO., LTD.

Column Whit Axial Force and Moment X - X

(Ultimate Stress Design method in accordance with ACI 318)

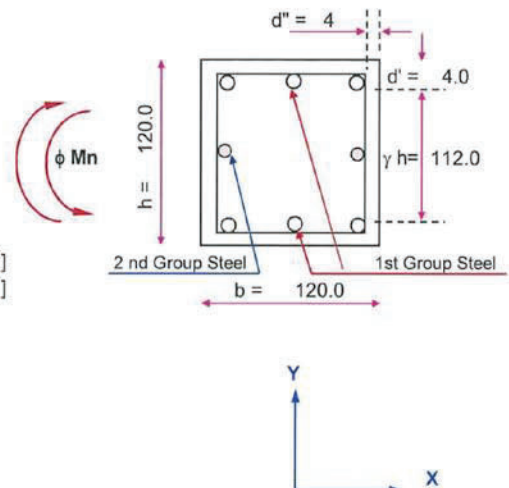
Job No. : 193018
Rev. : 0
Initial : CKJ
Date : 23-Dec-20

Column No. C-2 3rd-5th

Project : อาคารทิศตะวันตก

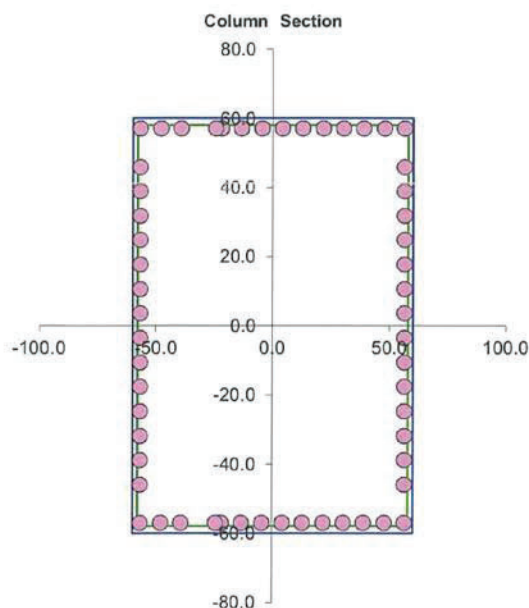
filename : COLUMN

Concrete Strength	f_c' =	350	[kg/cm ²]
	f_y SD =	4000	[kg/cm ²]
	f_y RD =	2400	[kg/cm ²]
Column Dimension	b =	120	[cm]
	h =	120	[cm]
	d' =	4	[cm]
	d'' =	4	[cm]
Load	ϕP_n =	2712	[T]
Moment	ϕM_n =	271	[T-m]
Separate Steel 2 group	1 st. =	28	$A_s = 172.4$ [cm ²]
	2 nd. =	28	$A_s = 172.4$ [cm ²]
Steel Reinforcement	No. =	56	
	d =	116	[cm]
	C_b =	70.150	[cm]
	p of Steel =	0.024	OK
Main Steel Used	56 DB 28		DB 28
Stirrup	DB 12 @ 0.400		DB 12
e/b =	0.45		[cm]

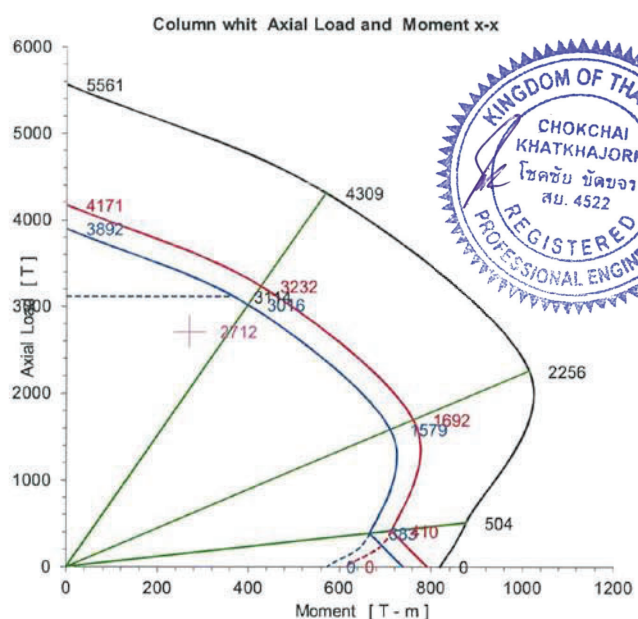


Column (120 x 120)
Steel 56 DB 28
Stirrup DB 12 @ 0.400

Boundary of tie stirrup Column
Boundary of spiral stirrup Column
Boundary of Ultimate Capacity



Column C-2 (120 x 120)



DYNAMIC ENGINEERING CONSULTANT CO., LTD.

Column Whit Axial Force and Moment X - X

(Ultimate Stress Design method in accordance with ACI 318)

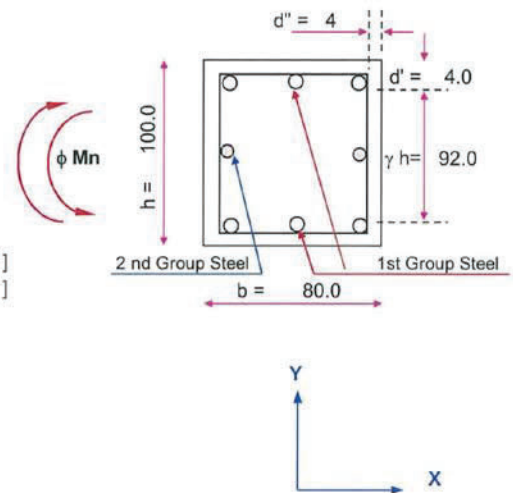
Job No. : 193018
Rev. : 0
Initial : CKJ
Date : 23-Dec-20

Column No. C-2 4th-5th

Project : อาคารทิศตะวันตก

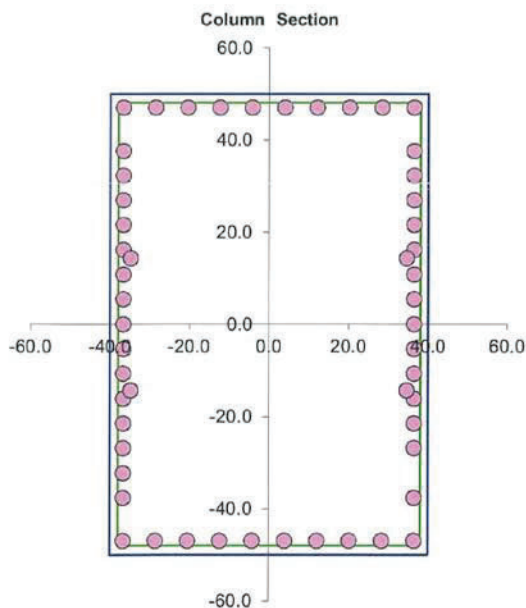
filename : COLUMN

Concrete Strength	$f_c' =$	350	[kg/cm ²]
	f_y SD	4000	[kg/cm ²]
	f_y RD	2400	[kg/cm ²]
Column Dimension	$b =$	80	[cm]
	$h =$	100	[cm]
	$d' =$	4	[cm]
	$d'' =$	4	[cm]
Load	$\phi P_n =$	1200	[T]
Moment	$\phi M_n =$	120	[T-m]
Separate Steel 2 group	1 st.	20	$A_s = 98.2$ [cm ²]
	2 nd.	36	$A_s = 176.7$ [cm ²]
Steel Reinforcement	No.	56	
	$d =$	96	[cm]
	$C_b =$	58.055	[cm]
	p of Steel	0.034	OK
Main Steel Used	56 DB 25		
Stirrup	RB 9 @ 0.400		
$e/b =$	0.36		[cm]

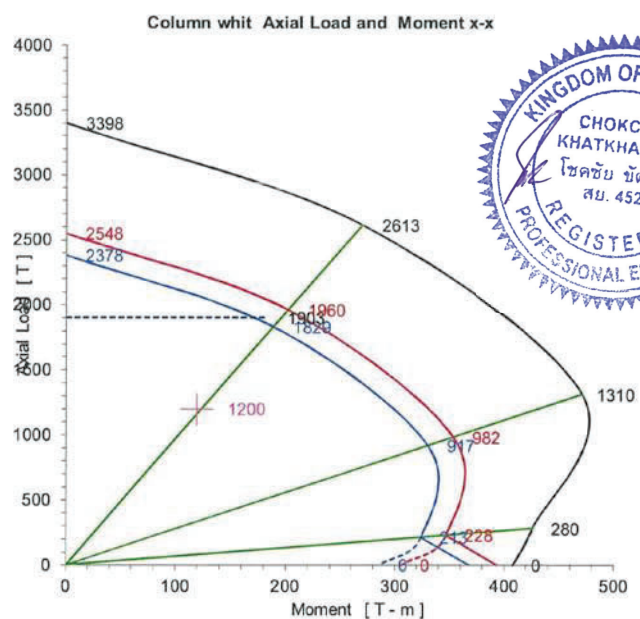


Column (80 x 100)
Steel 56 DB 25
Stirrup RB 9 @ 0.400

Boundary of tie stirrup Column
Boundary of spiral stirrup Column
Boundary of Ultimate Capacity



Column C-2 (80 x 100)



DYNAMIC ENGINEERING CONSULTANT CO., LTD.

Column Whit Axial Force and Moment X - X

(Ultimate Stress Design method in accordance with ACI 318)

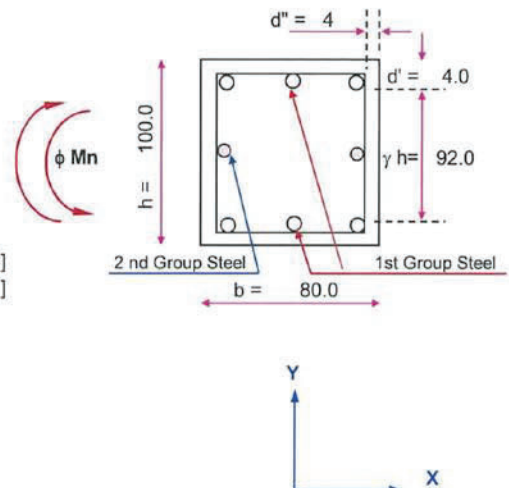
Job No. : 193018
Rev. : 0
Initial : CKJ
Date : 23-Dec-20

Column No. C-2 6th-7th

Project : อาคารทิศตะวันตก

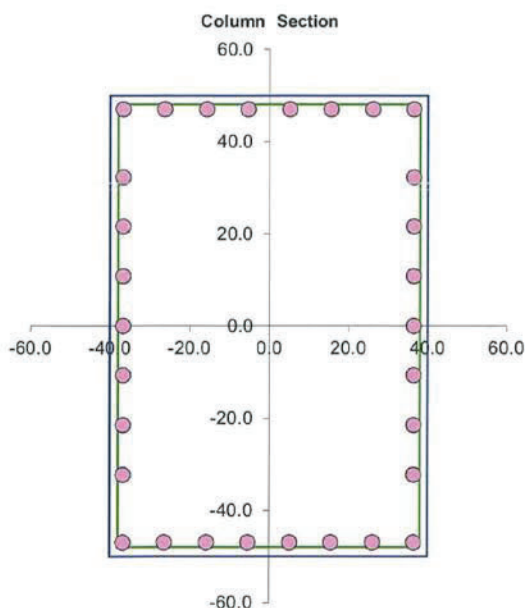
filename : COLUMN

Concrete Strength	$f_c' =$	350	[kg/cm ²]
	f_y SD	4000	[kg/cm ²]
	f_y RD	2400	[kg/cm ²]
Column Dimension	$b =$	80	[cm]
	$h =$	100	[cm]
	$d' =$	4	[cm]
	$d'' =$	4	[cm]
Load	$\phi P_n =$	930	[T]
Moment	$\phi M_n =$	93	[T-m]
Separate Steel 2 group	1 st.	16	$A_s = 78.5$ [cm ²]
	2 nd.	14	$A_s = 68.7$ [cm ²]
Steel Reinforcement	No.	30	
	$d =$	96	[cm]
	$C_b =$	58.055	[cm]
	p of Steel	0.018	OK
Main Steel Used	30 DB 25		
Stirrup	RB 9 @ 0.400		
$e b =$	0.36	[cm]	

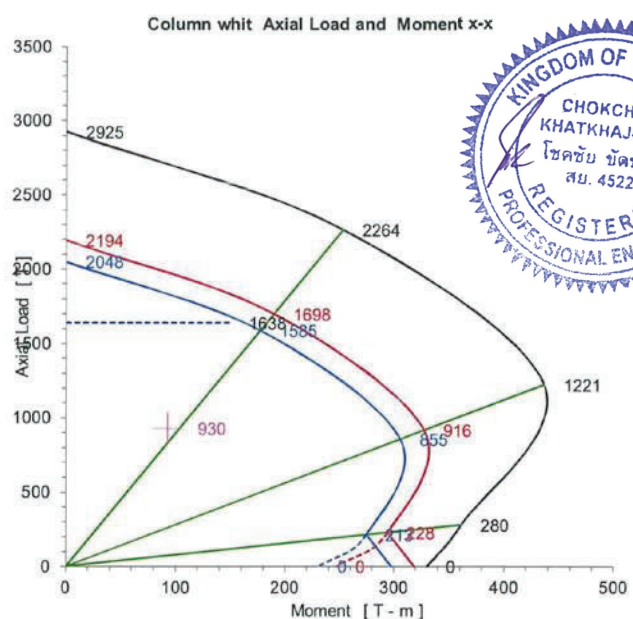


Column (80 x 100)
Steel 30 DB 25
Stirrup RB 9 @ 0.400

Boundary of tie stirrup Column
Boundary of spiral stirrup Column
Boundary of Ultimate Capacity



Column C-2 (80 x 100)



DYNAMIC ENGINEERING CONSULTANT CO., LTD.

Column Whit Axial Force and Moment X - X

(Ultimate Stress Design method in accordance with ACI 318)

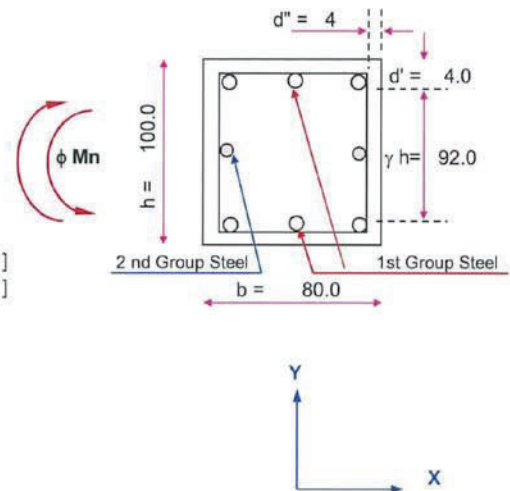
Job No. : 193018
Rev. : 0
Initial : CKJ
Date : 23-Dec-20

Column No. C-2 8th-Roof

Project : อาคารทิศตะวันตก

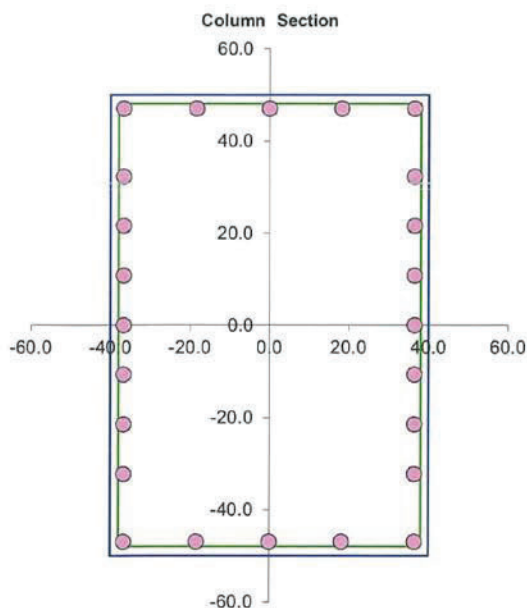
filename : COLUMN

Concrete Strength	$f_c' =$	350	[kg/cm ²]
	f_y SD	4000	[kg/cm ²]
	f_y RD	2400	[kg/cm ²]
Column Dimension	$b =$	80	[cm]
	$h =$	100	[cm]
	$d' =$	4	[cm]
	$d'' =$	4	[cm]
Load	$\phi P_n =$	660	[T]
Moment	$\phi M_n =$	66	[T-m]
Separate Steel 2 group	1 st.	10	$A_s = 49.1$ [cm ²]
	2 nd.	14	$A_s = 68.7$ [cm ²]
Steel Reinforcement	No.	24	
	$d =$	96	[cm]
	$C_b =$	58.055	[cm]
	$d(\epsilon_u / (\epsilon_y + \epsilon_u))$	0.015	OK
	p of Steel		
Main Steel Used	24 DB 25		
Stirrup	RB 9 @ 0.400		
e b =	0.31	[cm]	

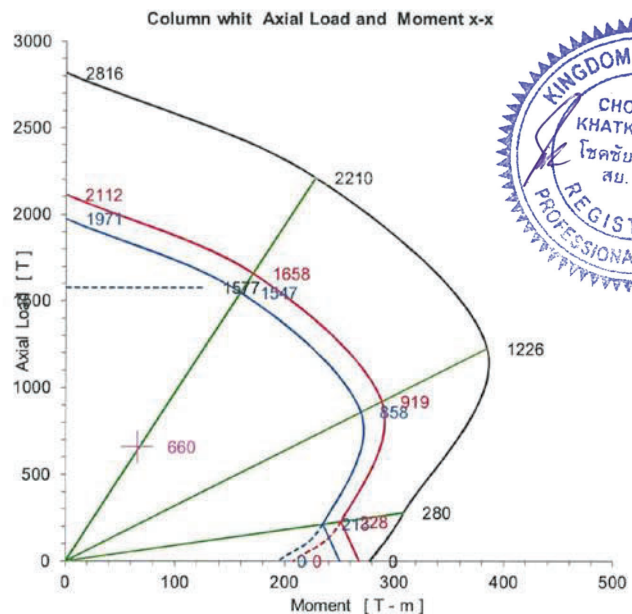


Column (80 x 100)
Steel 24 DB 25
Stirrup RB 9 @ 0.400

Boundary of tie stirrup Column
Boundary of spiral stirrup Column
Boundary of Ultimate Capacity



Column C-2 (80 x 100)



DYNAMIC ENGINEERING CONSULTANT CO., LTD.

Column Whit Axial Force and Moment X - X

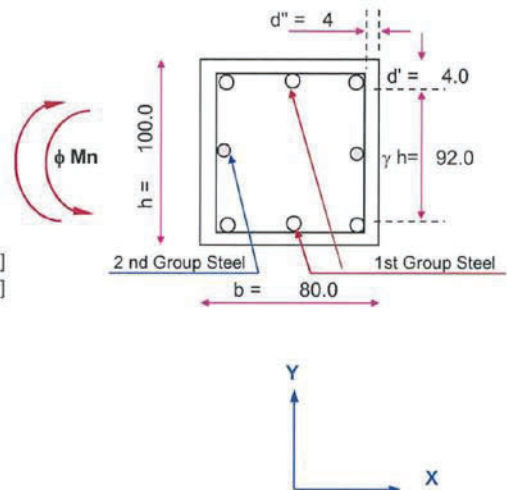
(Ultimate Stress Design method in accordance with ACI 318)

Job No. : 193018
Rev. : 0
Initial : CKJ
Date : 23-Dec-20

Column No. : C-3 1st
Project : อาคารทิศตะวันตก

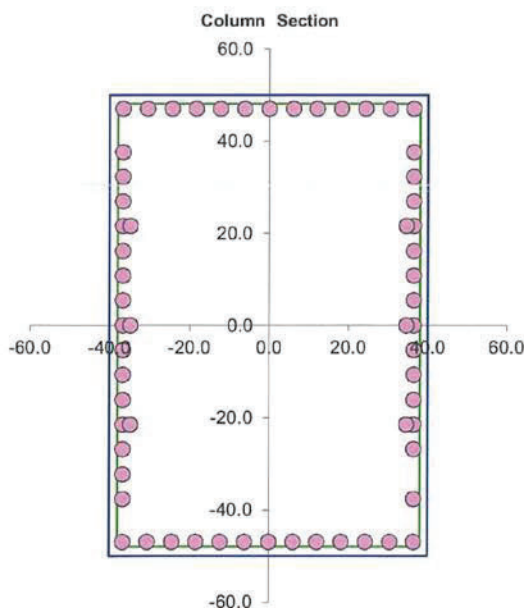
filename : COLUMN

Concrete Strength	$f_c' =$	350	[kg/cm ²]
	f_y SD	4000	[kg/cm ²]
	f_y RD	2400	[kg/cm ²]
Column Dimension	$b =$	80	[cm]
	$h =$	100	[cm]
	$d' =$	4	[cm]
	$d'' =$	4	[cm]
Load	$\phi P_n =$	1605	[T]
Moment	$\phi M_n =$	160	[T-m]
Separate Steel 2 group	1 st.	26	$A_s = 160.1$ [cm ²]
	2 nd.	36	$A_s = 221.7$ [cm ²]
Steel Reinforcement	No.	62	
	$d =$	96	[cm]
	$C_b =$	58.055	[cm]
$d(\epsilon_u / (\epsilon_y + \epsilon_u))$	ρ of Steel	0.048	OK
Main Steel Used	62 DB 28		
Stirrup	DB 12 @ 0.400		
$e/b =$	0.43		[cm]

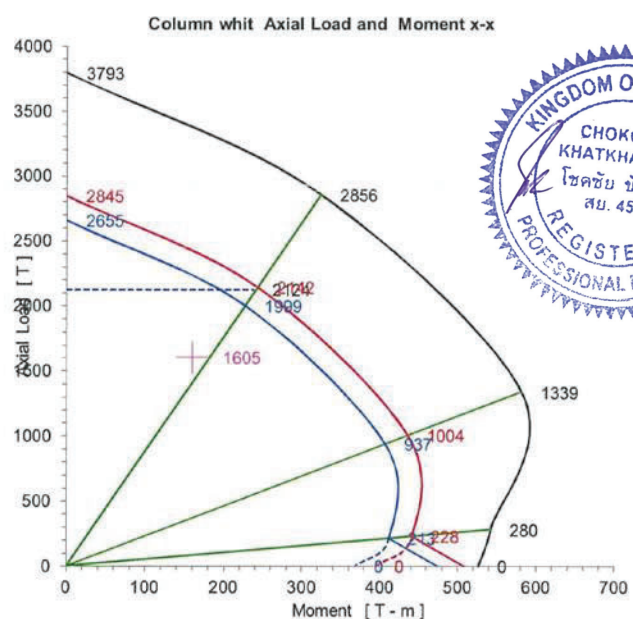


Column (80 x 100)
Steel 62 DB 28
Stirrup DB 12 @ 0.400

Boundary of tie stirrup Column
Boundary of spiral stirrup Column
Boundary of Ultimate Capacity



Column C-3 (80 x 100)



DYNAMIC ENGINEERING CONSULTANT CO., LTD.

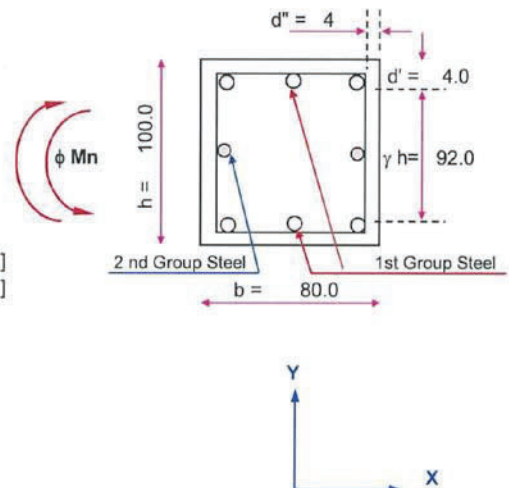
Column Whit Axial Force and Moment X - X
(Ultimate Stress Design method in accordance with ACI 318)

Job No. : 193018
Rev. : 0
Initial : CKJ
Date : 23-Dec-20

Column No. **C-3** 2nd-3rd
Project : อาคารทิศตะวันตก

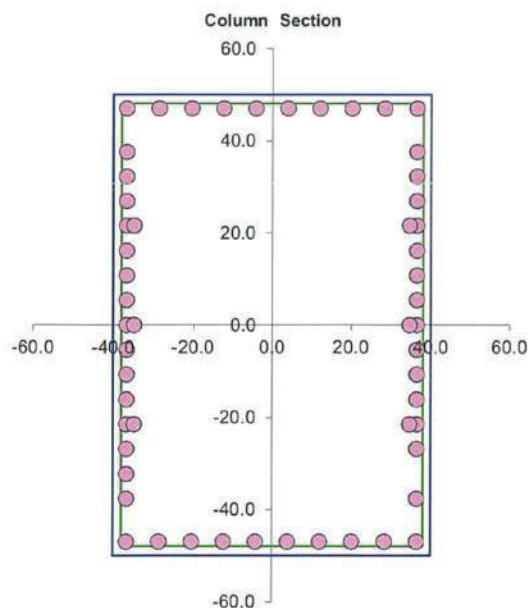
filename : COLUMN

Concrete Strength $f_c' = 350$ [kg/cm²]
 f_y SD = 4000 [kg/cm²]
 f_y RD = 2400 [kg/cm²]
Column Dimension $b = 80$ [cm]
 $h = 100$ [cm]
 $d' = 4$ [cm]
 $d'' = 4$ [cm]
Load $\phi P_n = 1470$ [T]
Moment $\phi M_n = 147$ [T-m]
Separate Steel 2 group 1 st. = 20 $A_s = 123.2$ [cm²]
2 nd. = 36 $A_s = 221.7$ [cm²]
Steel Reinforcement No. = 56
 $d = 96$ [cm]
 $d(\epsilon_u / (\epsilon_y + \epsilon_u))$ Cb = 58.055 [cm]
p of Steel = 0.043 OK
Main Steel Used 56 DB 28
Stirrup DB 12 @ 0.400
e b = 0.38 [cm]

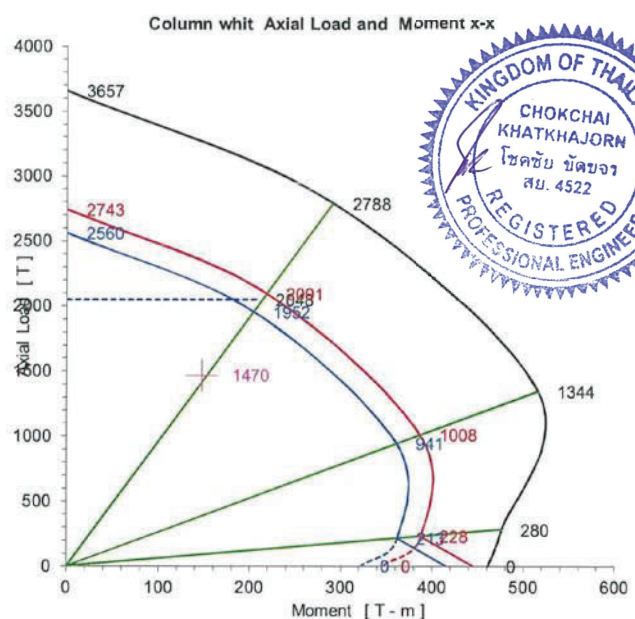


Column (80 x 100)
Steel 56 DB 28
Stirrup DB 12 @ 0.400

Boundary of tie stirrup Column
Boundary of spiral stirrup Column
Boundary of Ultimate Capacity



Column C-3 (80 x 100)



DYNAMIC ENGINEERING CONSULTANT CO., LTD.

Column Whit Axial Force and Moment X - X

(Ultimate Stress Design method in accordance with ACI 318)

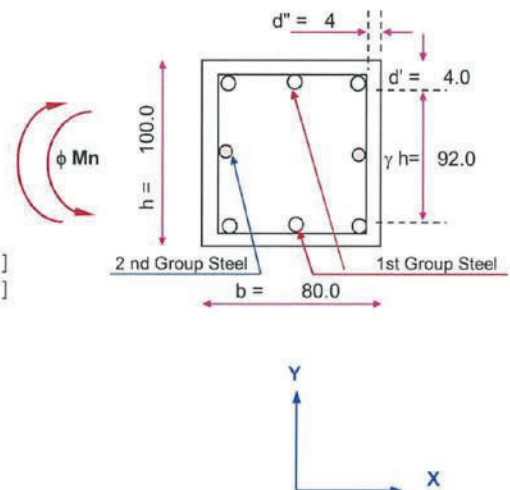
Job No. : 193018
Rev. : 0
Initial : CKJ
Date : 23-Dec-20

Column No. : C-3 4h-5th

Project : อาคารทิศตะวันตก

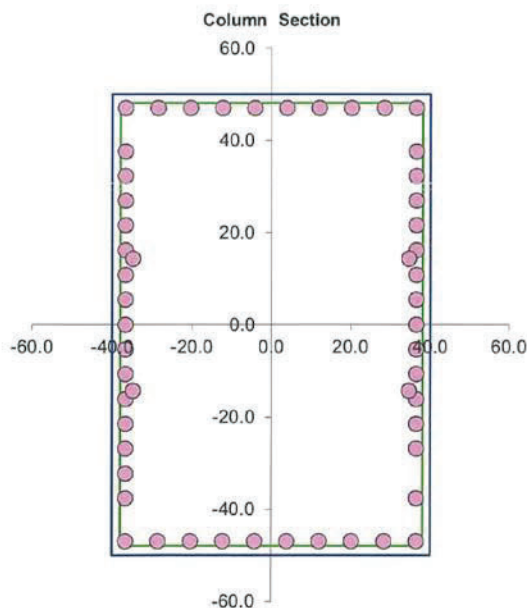
filename : COLUMN

Concrete Strength	$f_c' =$	350	[kg/cm ²]
	f_y SD	4000	[kg/cm ²]
	f_y RD	2400	[kg/cm ²]
Column Dimension	$b =$	80	[cm]
	$h =$	100	[cm]
	$d' =$	4	[cm]
	$d'' =$	4	[cm]
Load	$\phi P_n =$	1200	[T]
Moment	$\phi M_n =$	120	[T-m]
Separate Steel 2 group	1 st.	20	$A_s = 98.2$ [cm ²]
	2 nd.	36	$A_s = 176.7$ [cm ²]
Steel Reinforcement	No.	56	
	$d =$	96	[cm]
	$C_b =$	58.055	[cm]
	p of Steel	0.034	OK
Main Steel Used	56 DB 25		DB 25
Stirrup	RB 9 @ 0.400		RB 9
$e/b =$	0.36		[cm]

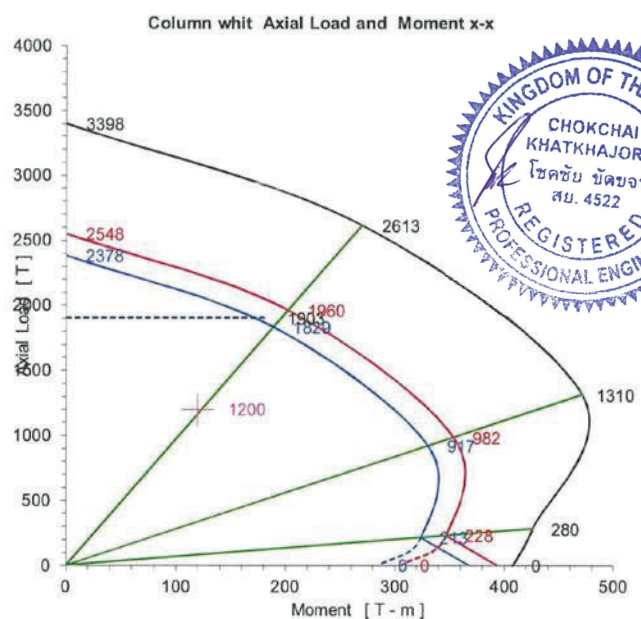


Column (80 x 100)
Steel 56 DB 25
Stirrup RB 9 @ 0.400

Boundary of tie stirrup Column
Boundary of spiral stirrup Column
Boundary of Ultimate Capacity



Column C-3 (80 x 100)



DYNAMIC ENGINEERING CONSULTANT CO., LTD.

Column Whit Axial Force and Moment X - X

(Ultimate Stress Design method in accordance with ACI 318)

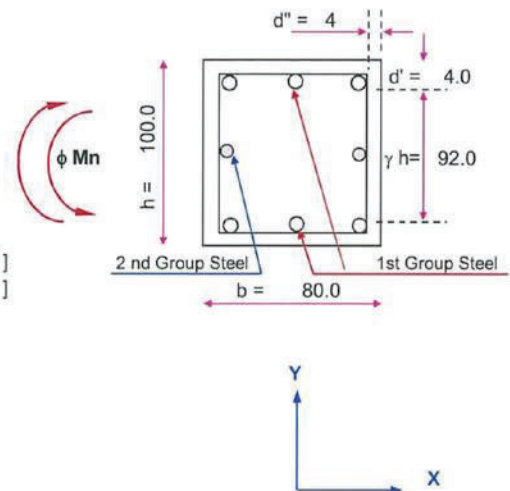
Job No. : 193018
Rev. : 0
Initial : CKJ
Date : 23-Dec-20

Column No. C-3 6th-7th

Project : อาคารทิศตะวันตก

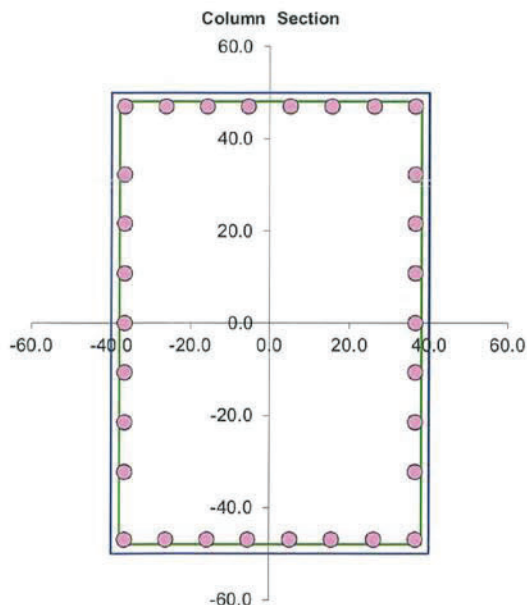
filename : COLUMN

Concrete Strength	$f_c' =$	350	[kg/cm ²]
	f_y SD	4000	[kg/cm ²]
	f_y RD	2400	[kg/cm ²]
Column Dimension	$b =$	80	[cm]
	$h =$	100	[cm]
	$d' =$	4	[cm]
	$d'' =$	4	[cm]
Load	$\phi P_n =$	930	[T]
Moment	$\phi M_n =$	93	[T-m]
Separate Steel 2 group	1 st.	16	$A_s = 78.5$ [cm ²]
	2 nd.	14	$A_s = 68.7$ [cm ²]
Steel Reinforcement	No.	30	
	$d =$	96	[cm]
	$C_b =$	58.055	[cm]
$d(\epsilon_u / (\epsilon_y + \epsilon_u))$	p of Steel	0.018	OK
Main Steel Used	30 DB 25		
Stirrup	RB 9 @ 0.400		
$e_b =$	0.36	[cm]	

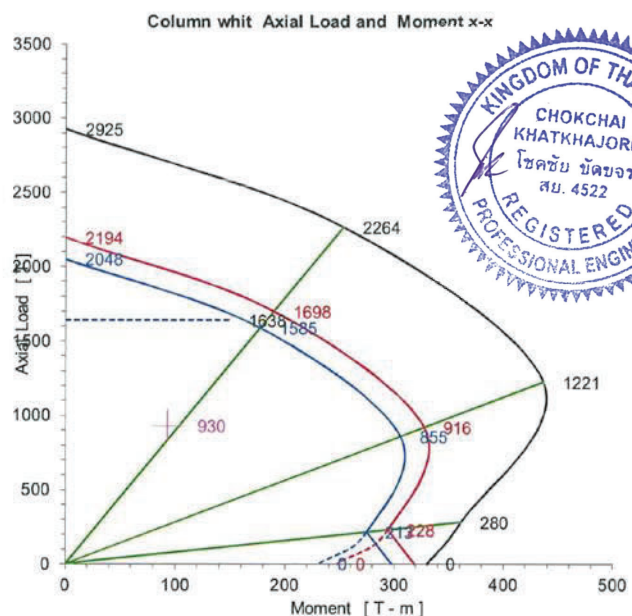


Column (80 x 100)
Steel 30 DB 25
Stirrup RB 9 @ 0.400

Boundary of tie stirrup Column
Boundary of spiral stirrup Column
Boundary of Ultimate Capacity



Column C-3 (80 x 100)



DYNAMIC ENGINEERING CONSULTANT CO., LTD.

Column Whit Axial Force and Moment X - X

(Ultimate Stress Design method in accordance with ACI 318)

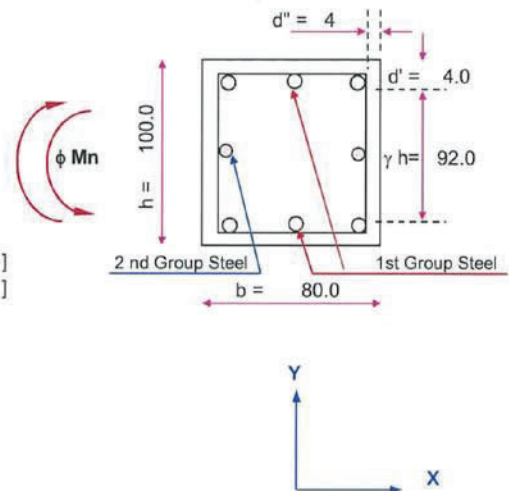
Job No. : 193018
Rev. : 0
Initial : CKJ
Date : 23-Dec-20

Column No. C-3 8th-Roof

Project : อาคารทิศตะวันตก

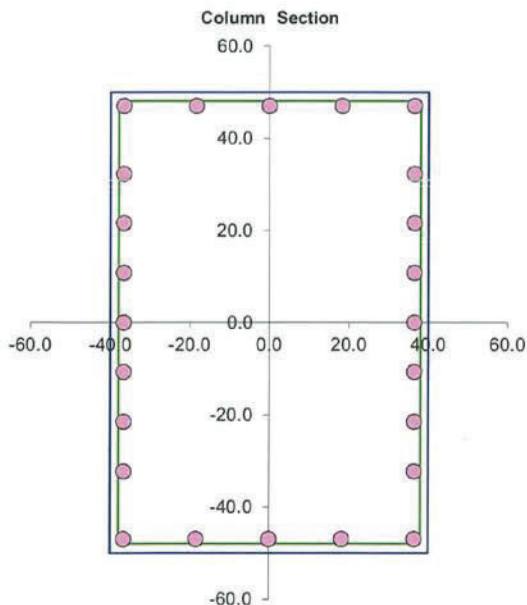
filename : COLUMN

Concrete Strength	f_c' =	350	[kg/cm ²]
	f_y SD =	4000	[kg/cm ²]
	f_y RD =	2400	[kg/cm ²]
Column Dimension	b =	80	[cm]
	h =	100	[cm]
	d' =	4	[cm]
	d'' =	4	[cm]
Load	ϕP_n =	660	[T]
Moment	ϕM_n =	66	[T-m]
Separate Steel 2 group	1 st. =	10	$A_s = 49.1$ [cm ²]
	2 nd. =	14	$A_s = 68.7$ [cm ²]
Steel Reinforcement	No. =	24	
	d =	96	[cm]
	C_b =	58.055	[cm]
	ρ of Steel =	0.015	OK
Main Steel Used	24 DB 25		DB 25
Stirrup	RB 9 @ 0.400		RB 9
e_b =	0.31		[cm]

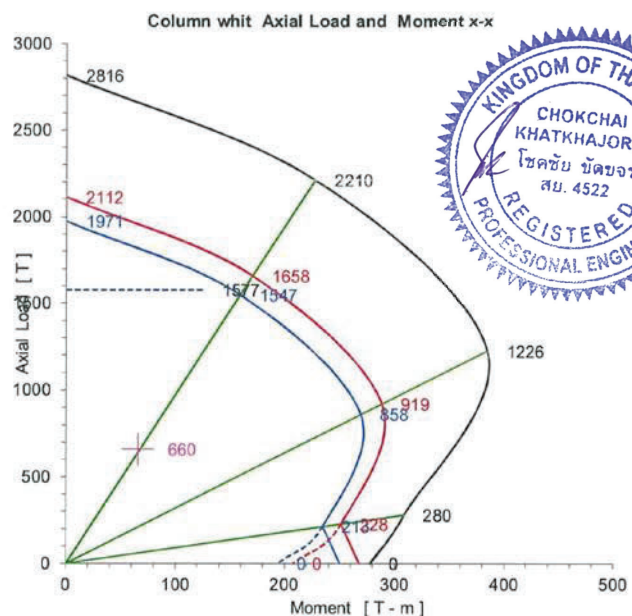


Column (80 x 100)
Steel 24 DB 25
Stirrup RB 9 @ 0.400

Boundary of tie stirrup Column
Boundary of spiral stirrup Column
Boundary of Ultimate Capacity



Column C-3 (80 x 100)



DYNAMIC ENGINEERING CONSULTANT CO., LTD.

Column Whit Axial Force and Moment X - X

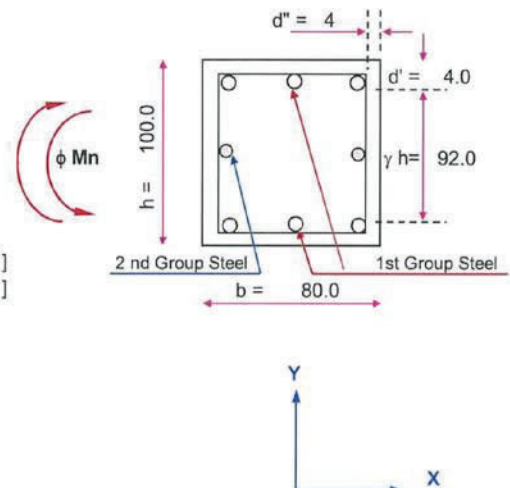
(Ultimate Stress Design method in accordance with ACI 318)

Job No. : 193018
Rev. : 0
Initial : CKJ
Date : 23-Dec-20

Column No. C-4 1st
Project : อาคารทิศตะวันตก

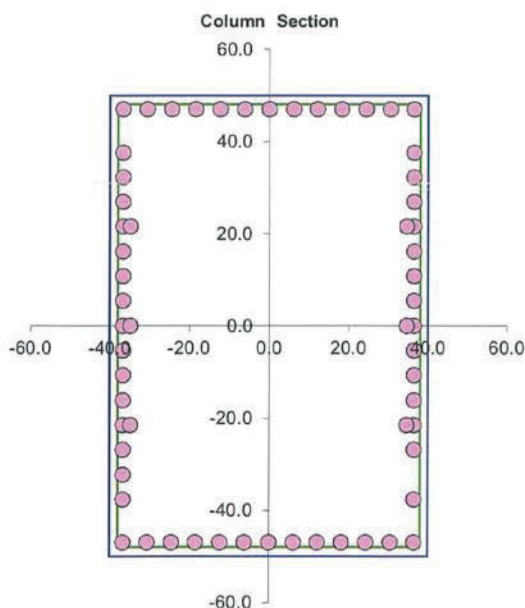
filename : COLUMN

Concrete Strength	$f_c' =$	350	[kg/cm ²]
	f_y SD	4000	[kg/cm ²]
	f_y RD	2400	[kg/cm ²]
Column Dimension	$b =$	80	[cm]
	$h =$	100	[cm]
	$d' =$	4	[cm]
	$d'' =$	4	[cm]
Load	$\phi P_n =$	1600	[T]
Moment	$\phi M_n =$	160	[T-m]
Separate Steel 2 group	1 st.	26	$A_s = 160.1$ [cm ²]
	2 nd.	36	$A_s = 221.7$ [cm ²]
Steel Reinforcement	No.	62	
	$d =$	96	[cm]
	$C_b =$	58.055	[cm]
$d(e_u / (e_y + e_u))$	p of Steel =	0.048	OK
Main Steel Used	62 DB 28		
Stirrup	DB 12 @ 0.400		
e b =	0.43	[cm]	

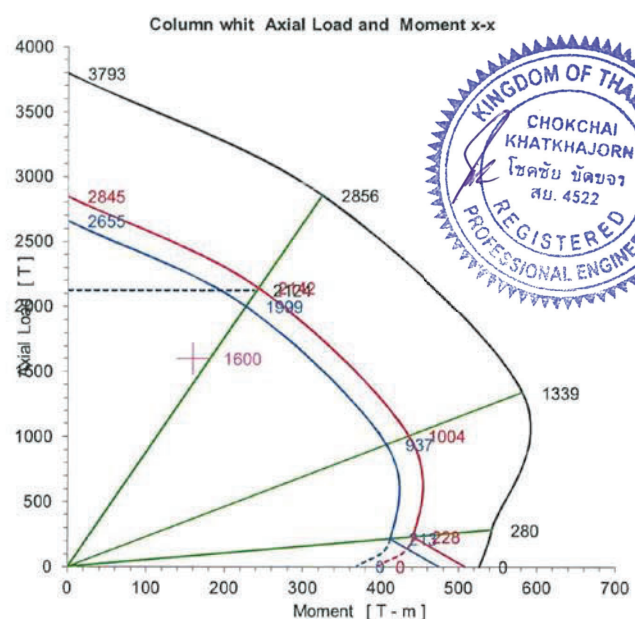


Column (80 x 100)
Steel 62 DB 28
Stirrup DB 12 @ 0.400

Boundary of tie stirrup Column
Boundary of spiral stirrup Column
Boundary of Ultimate Capacity



Column C-4 (80 x 100)



DYNAMIC ENGINEERING CONSULTANT CO., LTD.

Column Whit Axial Force and Moment X - X

(Ultimate Stress Design method in accordance with ACI 318)

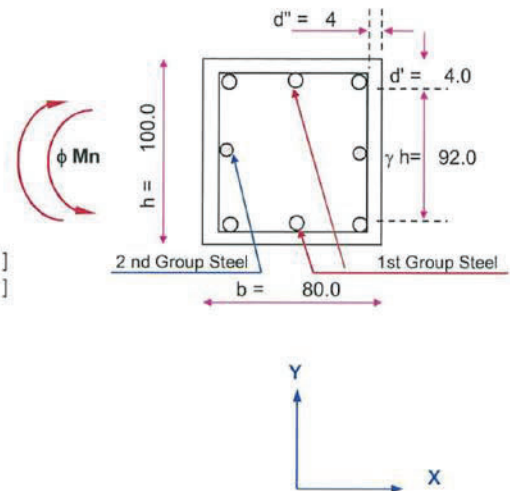
Job No. : 193018
Rev. : 0
Initial : CKJ
Date : 23-Dec-20

Column No. C-4 2nd-3rd

Project : อาคารทิศตะวันตก

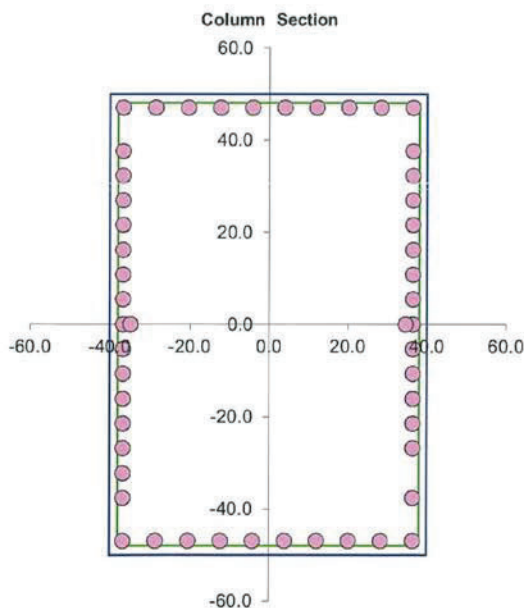
filename : COLUMN

Concrete Strength	f_c' =	350	[kg/cm ²]
	f_y SD =	4000	[kg/cm ²]
	f_y RD =	2400	[kg/cm ²]
Column Dimension	b =	80	[cm]
	h =	100	[cm]
	d' =	4	[cm]
	d'' =	4	[cm]
Load	ϕP_n =	1470	[T]
Moment	ϕM_n =	147	[T-m]
Separate Steel 2 group	1 st. =	20	$A_s = 123.2$ [cm ²]
	2 nd. =	32	$A_s = 197.0$ [cm ²]
Steel Reinforcement	No. =	52	
	d =	96	[cm]
	C_b =	58.055	[cm]
$d(\epsilon_u / (\epsilon_y + \epsilon_u))$	p of Steel =	0.040	OK
Main Steel Used	52 DB 28		DB 28
Stirrup	DB 12 @ 0.400		DB 12
e_b =	0.39	[cm]	

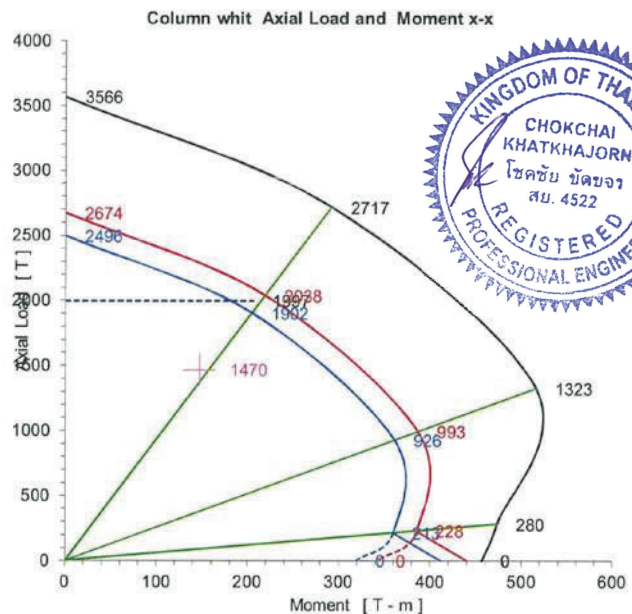


Column (80 x 100)
Steel 52 DB 28
Stirrup DB 12 @ 0.400

— Boundary of tie stirrup Column
— Boundary of spiral stirrup Column
— Boundary of Ultimate Capacity



Column C-4 (80 x 100)



DYNAMIC ENGINEERING CONSULTANT CO., LTD.

Column Whit Axial Force and Moment X - X

(Ultimate Stress Design method in accordance with ACI 318)

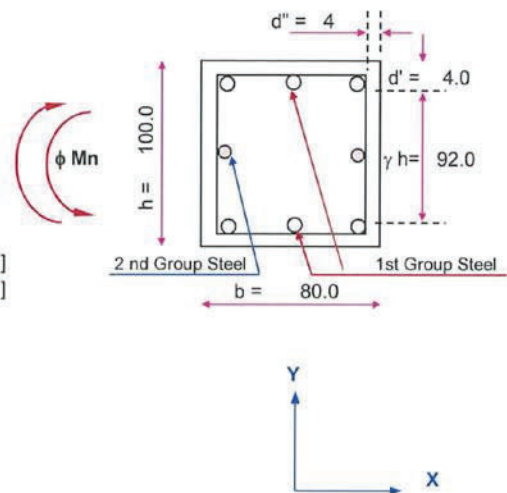
Job No. : 193018
Rev. : 0
Initial : CKJ
Date : 23-Dec-20

Column No. C-4 4th-5th

Project : อาคารทิศตะวันตก

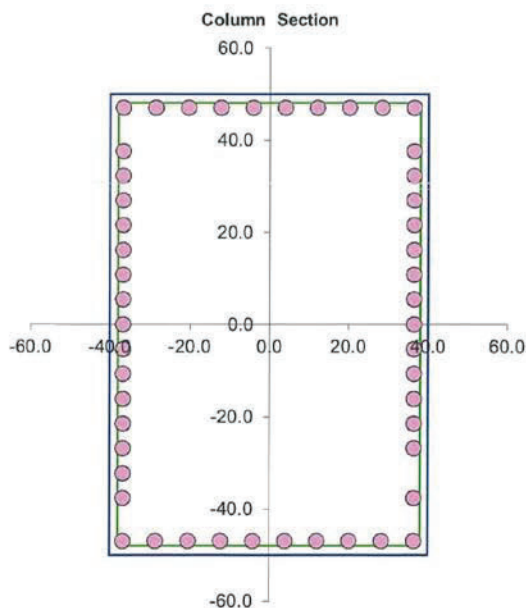
filename : COLUMN

Concrete Strength	f_c' =	350	[kg/cm ²]
	f_y SD =	4000	[kg/cm ²]
	f_y RD =	2400	[kg/cm ²]
Column Dimension	b =	80	[cm]
	h =	100	[cm]
	d' =	4	[cm]
	d'' =	4	[cm]
Load	ϕP_n =	1200	[T]
Moment	ϕM_n =	120	[T-m]
Separate Steel 2 group	1 st. =	20	$A_s = 98.2$ [cm ²]
	2 nd. =	32	$A_s = 157.1$ [cm ²]
Steel Reinforcement	No. =	52	
	d =	96	[cm]
	C_b =	58.055	[cm]
$d(\epsilon_u / (\epsilon_y + \epsilon_u))$	p of Steel =	0.032	OK
Main Steel Used	52 DB 25		DB 25
Stirrup	RB 9 @ 0.400		RB 9
e/b =	0.36		[cm]

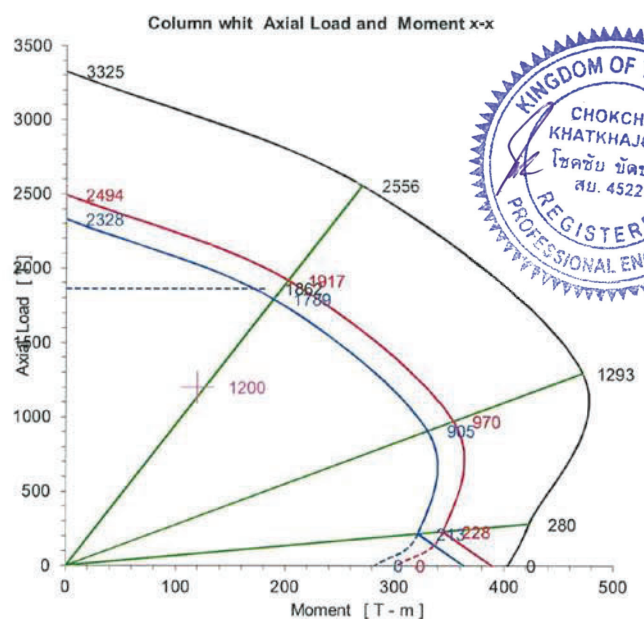


Column (80 x 100)
Steel 52 DB 25
Stirrup RB 9 @ 0.400

Boundary of tie stirrup Column
Boundary of spiral stirrup Column
Boundary of Ultimate Capacity



Column C-4 (80 x 100)



DYNAMIC ENGINEERING CONSULTANT CO., LTD.

Column Whit Axial Force and Moment X - X

(Ultimate Stress Design method in accordance with ACI 318)

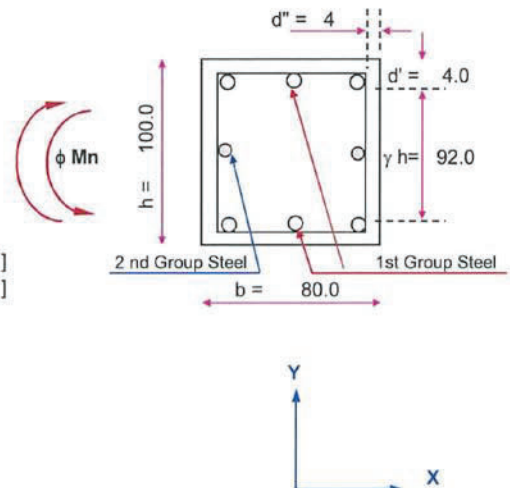
Job No. : 193018
Rev. : 0
Initial : CKJ
Date : 23-Dec-20

Column No. C-4 6th-7th

Project : อาคารทิศตะวันตก

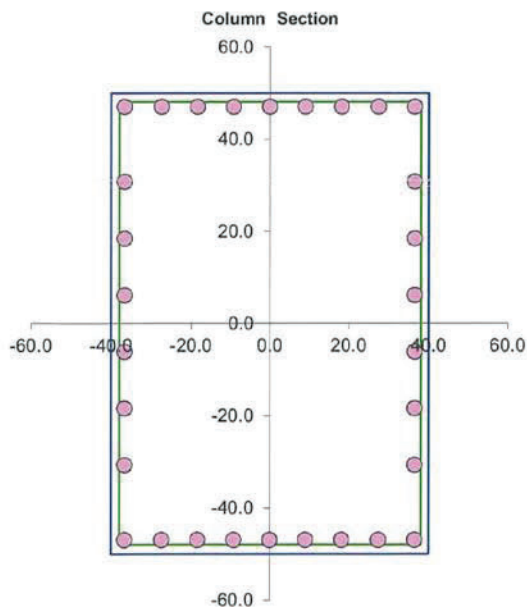
filename : COLUMN

Concrete Strength	f_c' =	350	[kg/cm ²]
	f_y SD =	4000	[kg/cm ²]
	f_y RD =	2400	[kg/cm ²]
Column Dimension	b =	80	[cm]
	h =	100	[cm]
	d' =	4	[cm]
	d'' =	4	[cm]
Load	ϕP_n =	930	[T]
Moment	ϕM_n =	93	[T-m]
Separate Steel 2 group	1 st. =	18	$A_s = 88.4$ [cm ²]
	2 nd. =	12	$A_s = 58.9$ [cm ²]
Steel Reinforcement	No. =	30	
	d =	96	[cm]
	C_b =	58.055	[cm]
	p of Steel =	0.018	OK
Main Steel Used	30 DB 25		DB 25
Stirrup	RB 9 @ 0.400		RB 9
e b =	0.37		[cm]

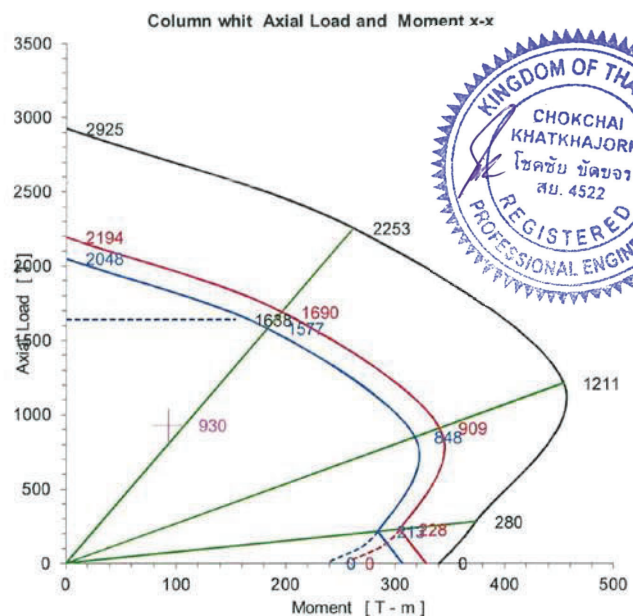


Column (80 x 100)
Steel 30 DB 25
Stirrup RB 9 @ 0.400

Boundary of tie stirrup Column
Boundary of spiral stirrup Column
Boundary of Ultimate Capacity



Column C-4 (80 x 100)



DYNAMIC ENGINEERING CONSULTANT CO., LTD.

Column Whit Axial Force and Moment X - X

(Ultimate Stress Design method in accordance with ACI 318-89)

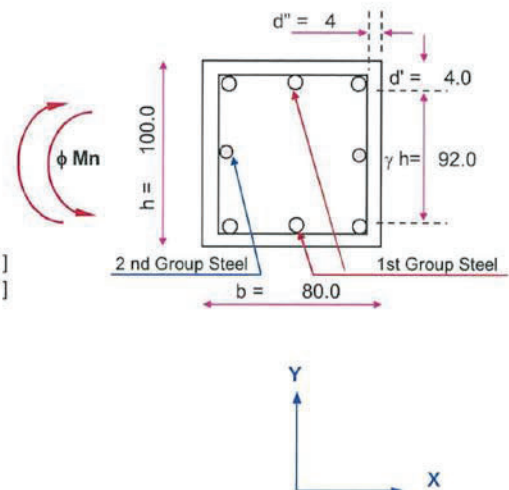
Job No. : 193018
Rev. : 0
Initial : CKJ
Date : 23-Dec-20

Column No. C-4 8th-Roof

Project : อาคารทิศตะวันตก

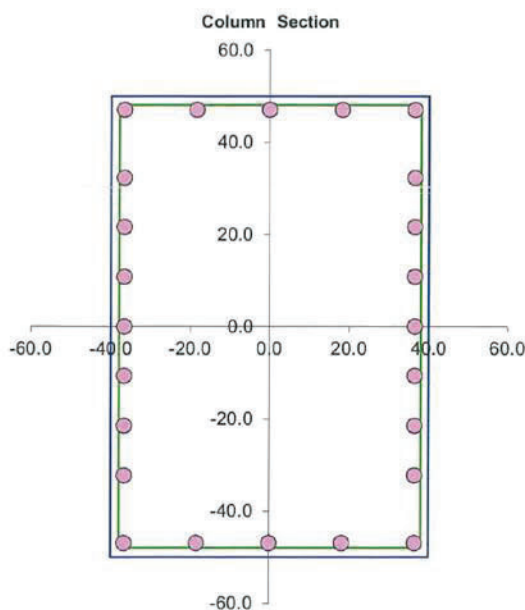
filename : COLUMN

Concrete Strength	$f_c' =$	350	[kg/cm ²]
	f_y SD	4000	[kg/cm ²]
	f_y RD	2400	[kg/cm ²]
Column Dimension	$b =$	80	[cm]
	$h =$	100	[cm]
	$d' =$	4	[cm]
	$d'' =$	4	[cm]
Load	$\phi P_n =$	660	[T]
Moment	$\phi M_n =$	66	[T-m]
Separate Steel 2 group	1 st.	10	As = 49.1 [cm ²]
	2 nd.	14	As = 68.7 [cm ²]
Steel Reinforcement	No.	24	
	$d =$	96	[cm]
$d(\epsilon_u / (\epsilon_y + \epsilon_u))$	$C_b =$	58.055	[cm]
	ρ of Steel	0.015	OK
Main Steel Used	24 DB 25		
Stirrup	RB 9 @ 0.400		
$e/b =$	0.31		[cm]

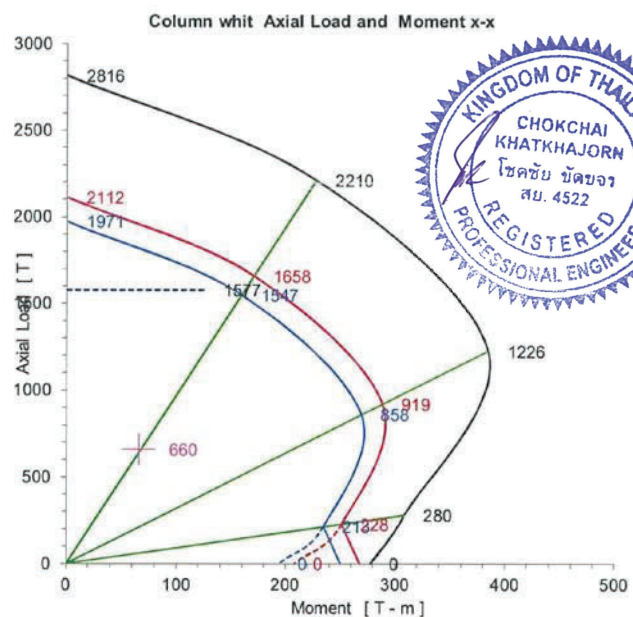


Column (80 x 100)
Steel 24 DB 25
Stirrup RB 9 @ 0.400

Boundary of tie stirrup Column
Boundary of spiral stirrup Column
Boundary of Ultimate Capacity



Column C-4 (80 x 100)



DYNAMIC ENGINEERING CONSULTANT CO., LTD.

Column Whit Axial Force and Moment X - X

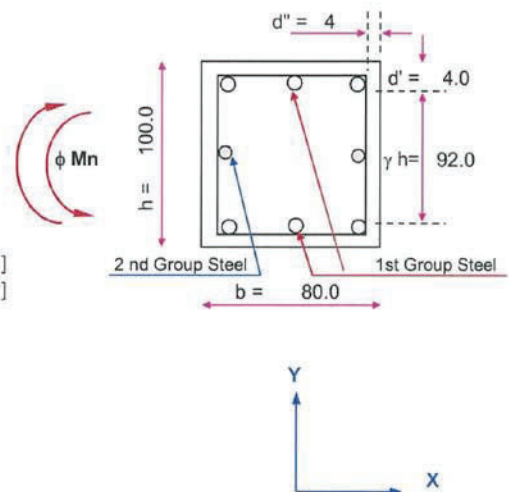
(Ultimate Stress Design method in accordance with ACI 318)

Job No. : 193018
Rev. : 0
Initial : CKJ
Date : 23-Dec-20

Column No. C-5 1st
Project : อาคารทิศตะวันตก

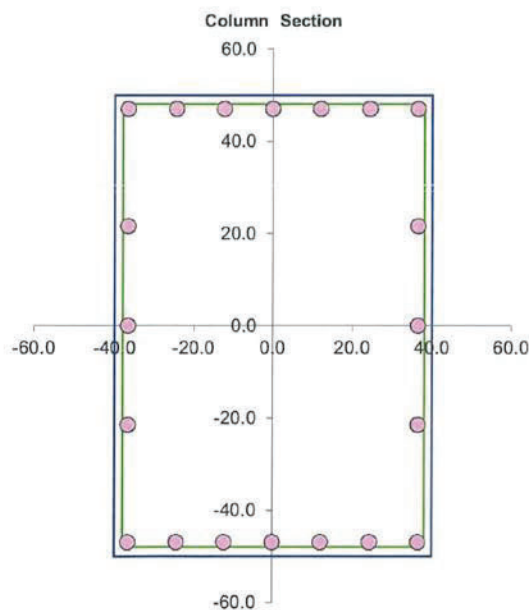
filename : COLUMN

Concrete Strength	$f_c' =$	350	[kg/cm ²]
	f_y SD	4000	[kg/cm ²]
	f_y RD	2400	[kg/cm ²]
Column Dimension	$b =$	80	[cm]
	$h =$	100	[cm]
	$d' =$	4	[cm]
	$d'' =$	4	[cm]
Load	$\phi P_n =$	330	[T]
Moment	$\phi M_n =$	33	[T-m]
Separate Steel 2 group	1 st.	14	$A_s = 68.7$ [cm ²]
	2 nd.	6	$A_s = 29.5$ [cm ²]
Steel Reinforcement	No.	20	
	$d =$	96	[cm]
$d(\epsilon_u / (\epsilon_y + \epsilon_u))$	$C_b =$	58.055	[cm]
	ρ of Steel =	0.012	OK
Main Steel Used	20 DB 25		DB 25
Stirrup	DB 12 @ 0.400		DB 12
$e_b =$	0.35		[cm]

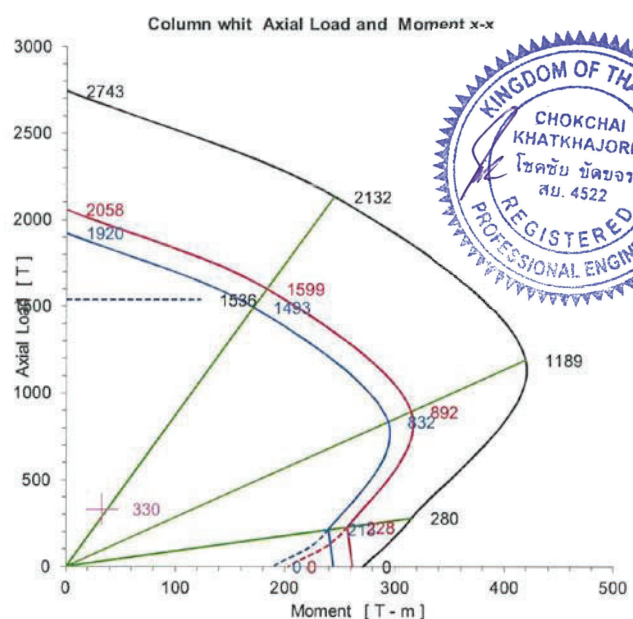


Column (80 x 100)
Steel 20 DB 25
Stirrup DB 12 @ 0.400

Boundary of tie stirrup Column
Boundary of spiral stirrup Column
Boundary of Ultimate Capacity



Column C-5 (80 x 100)



DYNAMIC ENGINEERING CONSULTANT CO., LTD.

Column Whit Axial Force and Moment X - X

(Ultimate Stress Design method in accordance with ACI 318)

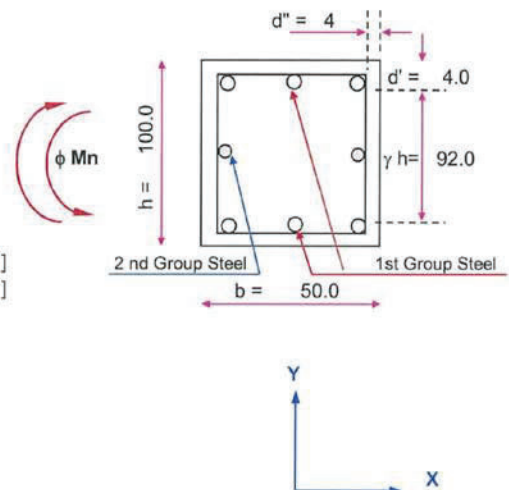
Job No. : 193018
Rev. : 0
Initial : CKJ
Date : 23-Dec-20

Column No. C-5 2nd-3rd

Project : อาคารทิศตะวันตก

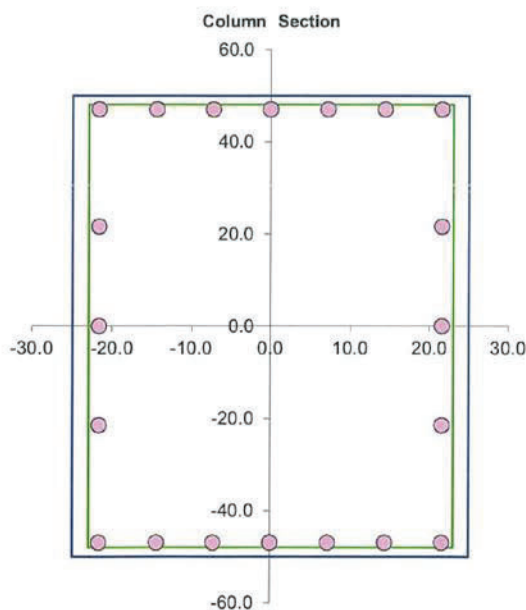
filename : COLUMN

Concrete Strength	f_c' =	350	[kg/cm ²]
	f_y SD =	4000	[kg/cm ²]
	f_y RD =	2400	[kg/cm ²]
Column Dimension	b =	50	[cm]
	h =	100	[cm]
	d' =	4	[cm]
	d'' =	4	[cm]
Load	ϕP_n =	165	[T]
Moment	ϕM_n =	16	[T-m]
Separate Steel 2 group	1 st. =	14	$A_s = 68.7$ [cm ²]
	2 nd. =	6	$A_s = 29.5$ [cm ²]
Steel Reinforcement	No. =	20	
	d =	96	[cm]
	C_b =	58.055	[cm]
	ρ of Steel =	0.020	OK
Main Steel Used	20 DB 25		DB 25
Stirrup	DB 12 @ 0.400		DB 12
e_b =	0.41		[cm]

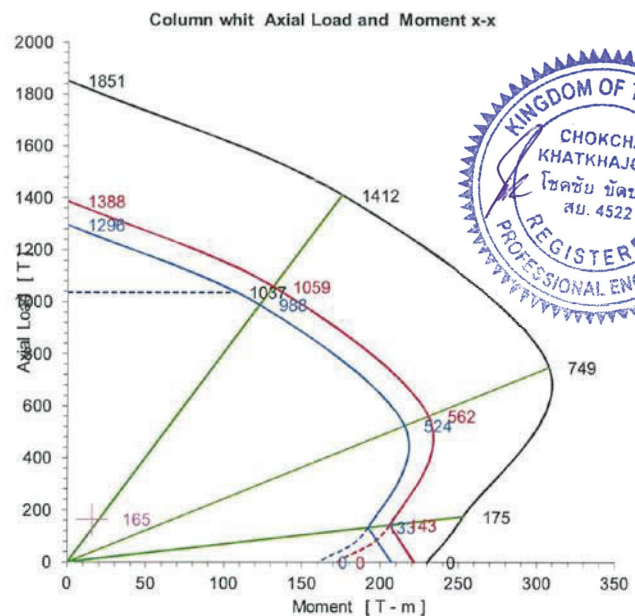


Column (50 x 100)
Steel 20 DB 25
Stirrup DB 12 @ 0.400

Boundary of tie stirrup Column
Boundary of spiral stirrup Column
Boundary of Ultimate Capacity



Column C-5 (50 x 100)



DYNAMIC ENGINEERING CONSULTANT CO., LTD.

Column Whit Axial Force and Moment X - X

(Ultimate Stress Design method in accordance with ACI 318)

Job No. : 193018

Rev. : 0

Initial : CKJ

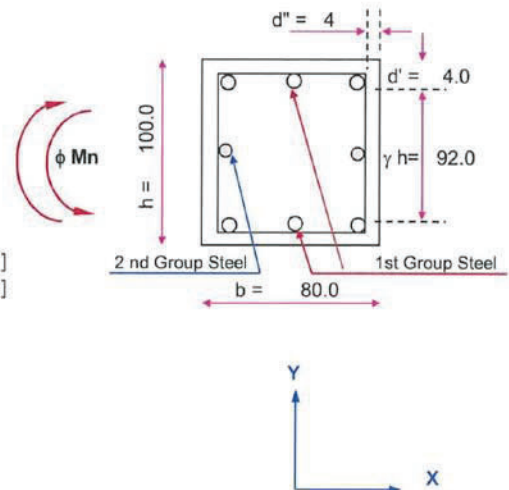
Date : 23-Dec-20

Column No. C-6 1st

Project : อาคารทิศตะวันตก

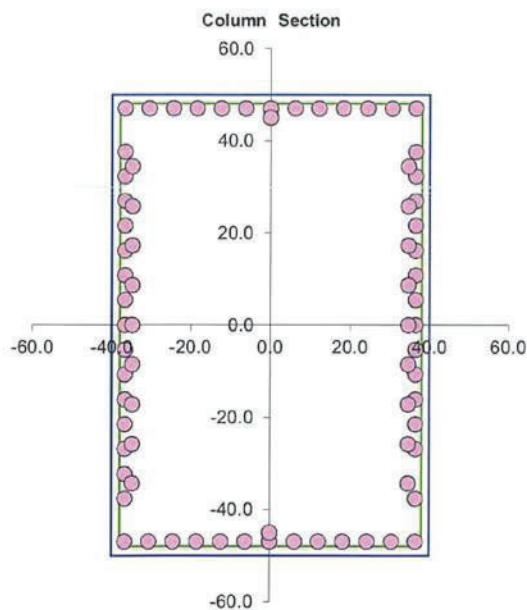
filename : COLUMN

Concrete Strength	$f_c' =$	350	[kg/cm ²]
	f_y SD	4000	[kg/cm ²]
	f_y RD	2400	[kg/cm ²]
Column Dimension	$b =$	80	[cm]
	$h =$	100	[cm]
	$d' =$	4	[cm]
	$d'' =$	4	[cm]
Load	$\phi P_n =$	2080	[T]
Moment	$\phi M_n =$	208	[T-m]
Separate Steel 2 group	1 st.	28	$A_s = 172.4$ [cm ²]
	2 nd.	48	$A_s = 295.6$ [cm ²]
Steel Reinforcement	No.	76	
	$d =$	96	[cm]
$d(\epsilon_u / (\epsilon_y + \epsilon_u))$	$C_b =$	58.055	[cm]
	p of Steel =	0.058	OK
Main Steel Used	76 DB 28		
Stirrup	DB 12 @ 0.400		
$e/b =$	0.43		[cm]

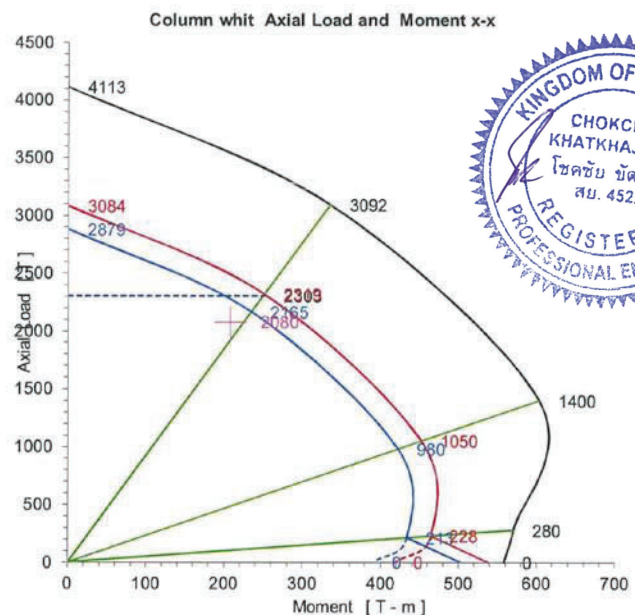


Column (80 x 100)
Steel 76 DB 28
Stirrup DB 12 @ 0.400

Boundary of tie stirrup Column
Boundary of spiral stirrup Column
Boundary of Ultimate Capacity



Column C-6 (80 x 100)



DYNAMIC ENGINEERING CONSULTANT CO., LTD.

Column Whit Axial Force and Moment X - X

(Ultimate Stress Design method in accordance with ACI 318)

Job No. : 193018

Rev. : 0

Initial : CKJ

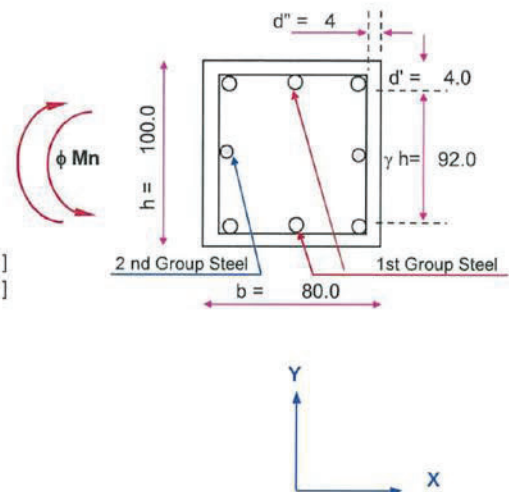
Date : 23-Dec-20

Column No. : C-6 2nd-3rd

Project : อาคารทิศตะวันตก

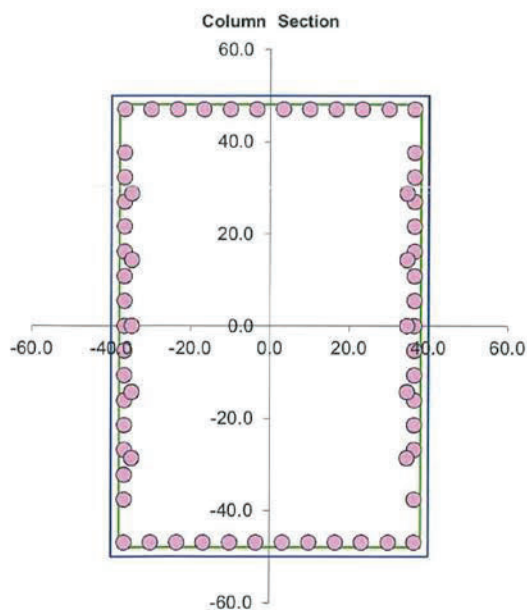
filename : COLUMN

Concrete Strength	f_c' =	350	[kg/cm ²]
	f_y SD =	4000	[kg/cm ²]
	f_y RD =	2400	[kg/cm ²]
Column Dimension	b =	80	[cm]
	h =	100	[cm]
	d' =	4	[cm]
	d'' =	4	[cm]
Load	ϕP_n =	1834	[T]
Moment	ϕM_n =	183	[T-m]
Separate Steel 2 group	1 st. =	24	$A_s = 147.8$ [cm ²]
	2 nd. =	40	$A_s = 246.3$ [cm ²]
Steel Reinforcement	No. =	64	
	d =	96	[cm]
$d(\epsilon_u/(\epsilon_y+\epsilon_u))$	C_b =	58.055	[cm]
	ρ of Steel =	0.049	OK
Main Steel Used	64 DB 28		DB 28
Stirrup	DB 12 @ 0.400		DB 12
e/b =	0.41		[cm]

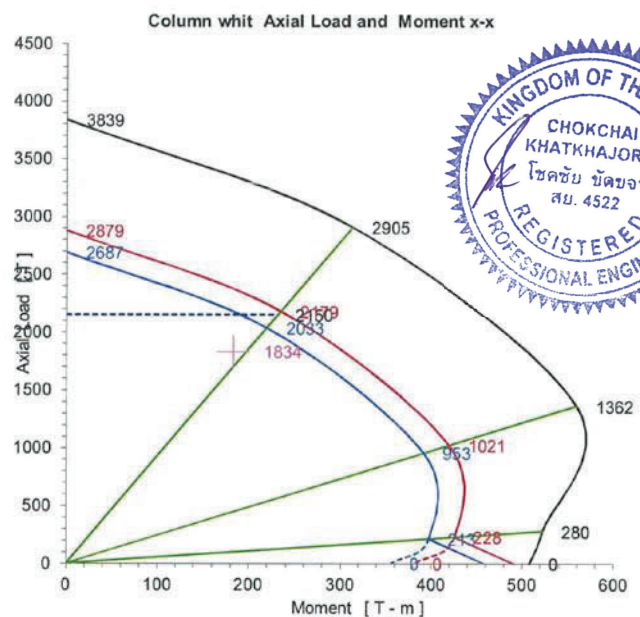


Column (80 x 100)
Steel 64 DB 28
Stirrup DB 12 @ 0.400

Boundary of tie stirrup Column
Boundary of spiral stirrup Column
Boundary of Ultimate Capacity



Column C-6 (80 x 100)



DYNAMIC ENGINEERING CONSULTANT CO., LTD.

Column Whit Axial Force and Moment X - X

(Ultimate Stress Design method in accordance with ACI 318)

Job No. : 193018

Rev. : 0

Initial : CKJ

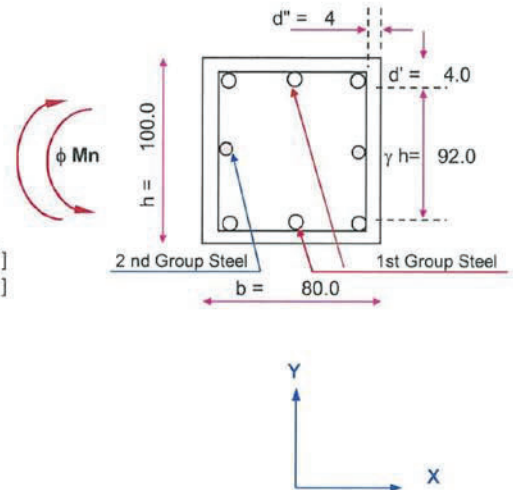
Date : 23-Dec-20

Column No. C-6 4th-5th

Project : อาคารทิศตะวันตก

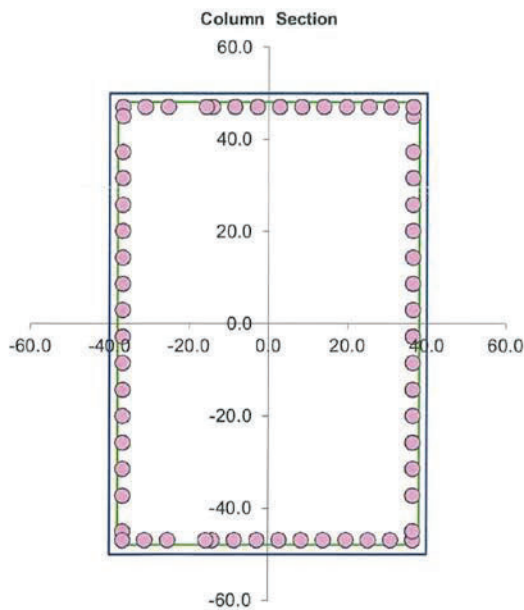
filename : COLUMN

Concrete Strength	$f_c' =$	350	[kg/cm ²]
	f_y SD	4000	[kg/cm ²]
	f_y RD	2400	[kg/cm ²]
Column Dimension	$b =$	80	[cm]
	$h =$	100	[cm]
	$d' =$	4	[cm]
	$d'' =$	4	[cm]
Load	$\phi P_n =$	1600	[T]
Moment	$\phi M_n =$	160	[T-m]
Separate Steel 2 group	1 st.	32	$A_s = 157.1$ [cm ²]
	2 nd.	28	$A_s = 137.4$ [cm ²]
Steel Reinforcement	No.	60	
	$d =$	96	[cm]
$d(\epsilon_u / (\epsilon_y + \epsilon_u))$	$C_b =$	58.055	[cm]
	p of Steel	0.037	OK
Main Steel Used	60 DB 25		DB 25
Stirrup	RB 9 @ 0.400		RB 9
$e/b =$	0.45		[cm]

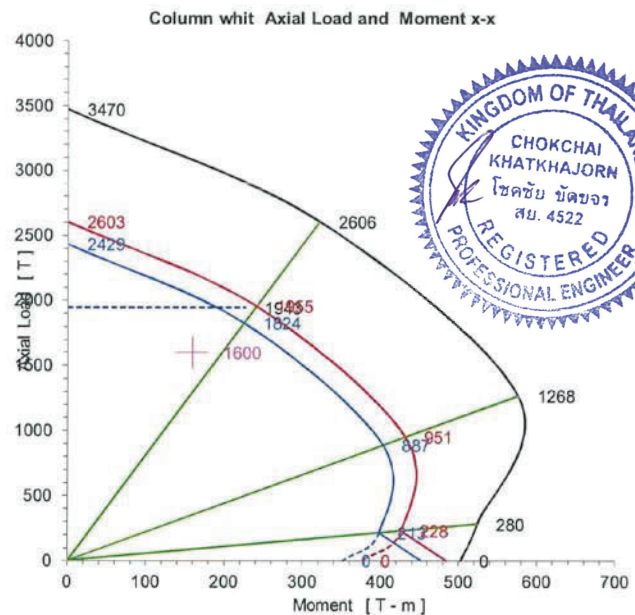


Column (80 x 100)
Steel 60 DB 25
Stirrup RB 9 @ 0.400

Boundary of tie stirrup Column
Boundary of spiral stirrup Column
Boundary of Ultimate Capacity



Column C-6 (80 x 100)



DYNAMIC ENGINEERING CONSULTANT CO., LTD.

Column Whit Axial Force and Moment X - X

(Ultimate Stress Design method in accordance with ACI 318)

Job No. : 193018

Rev. : 0

Initial : CKJ

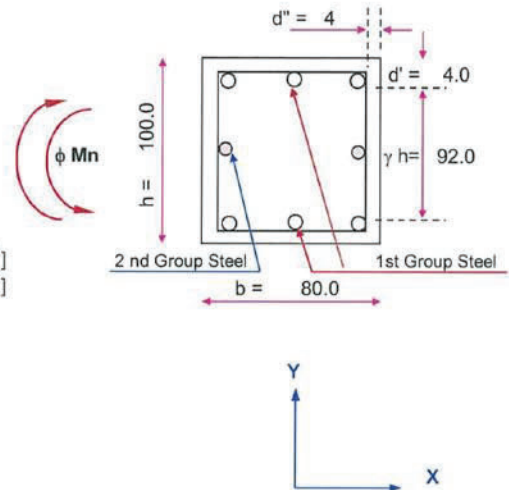
Date : 23-Dec-20

Column No. C-6 6th-7th

Project : อาคารทิศตะวันตก

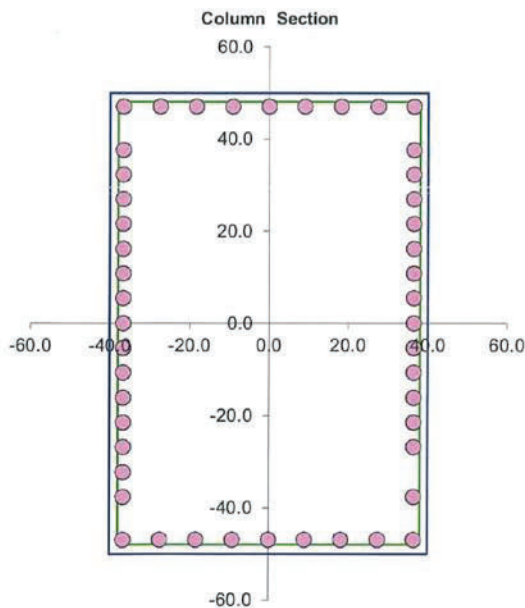
filename : COLUMN

Concrete Strength	$f_c' =$	350	[kg/cm ²]
	f_y SD	4000	[kg/cm ²]
	f_y RD	2400	[kg/cm ²]
Column Dimension	$b =$	80	[cm]
	$h =$	100	[cm]
	$d' =$	4	[cm]
	$d'' =$	4	[cm]
Load	$\phi P_n =$	1350	[T]
Moment	$\phi M_n =$	135	[T-m]
Separate Steel 2 group	1 st.	18	$A_s = 88.4$ [cm ²]
	2 nd.	30	$A_s = 147.3$ [cm ²]
Steel Reinforcement	No.	48	
	$d =$	96	[cm]
$d(e_u / (e_y + e_u))$	$C_b =$	58.055	[cm]
	p of Steel	0.029	OK
Main Steel Used	48 DB 25		
Stirrup	RB 9 @ 0.400		
$e_b =$	0.35		[cm]

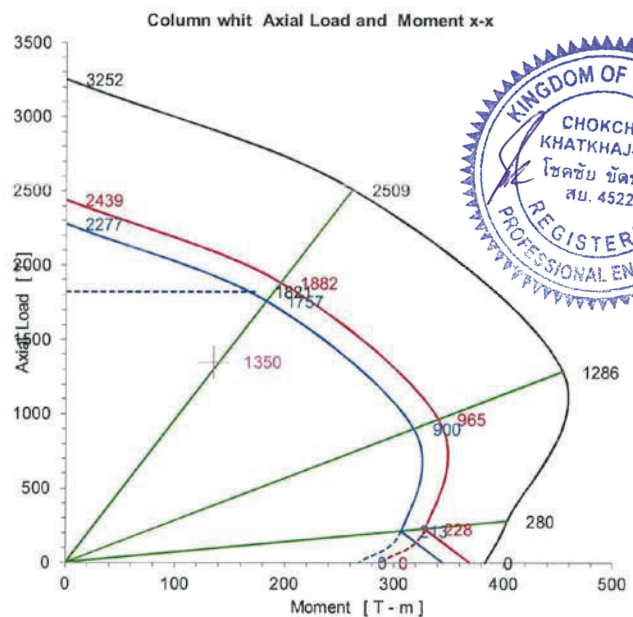


Column (80 x 100)
Steel 48 DB 25
Stirrup RB 9 @ 0.400

Boundary of tie stirrup Column
Boundary of spiral stirrup Column
Boundary of Ultimate Capacity



Column C-6 (80 x 100)



DYNAMIC ENGINEERING CONSULTANT CO., LTD.

Column Whit Axial Force and Moment X - X

(Ultimate Stress Design method in accordance with ACI 318)

Job No. : 193018

Rev. : 0

Initial : CKJ

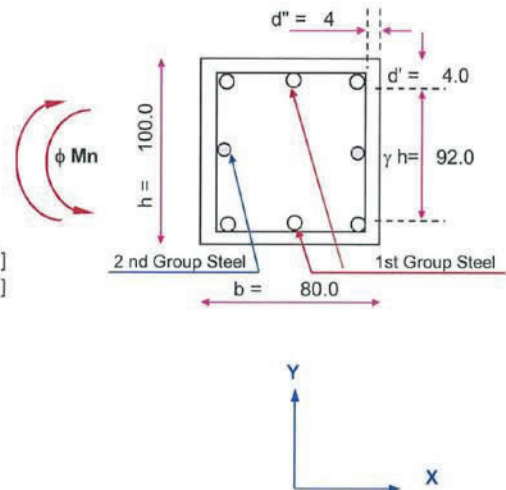
Date : 23-Dec-20

Column No. C-9 1st

Project : อาคารทิศตะวันตก

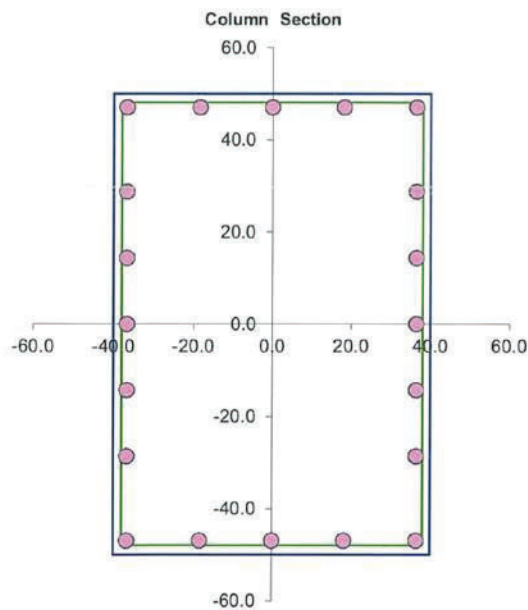
filename : COLUMN

Concrete Strength	$f_c' =$	350	[kg/cm ²]
	f_y SD	4000	[kg/cm ²]
	f_y RD	2400	[kg/cm ²]
Column Dimension	$b =$	80	[cm]
	$h =$	100	[cm]
	$d' =$	4	[cm]
	$d'' =$	4	[cm]
Load	$\phi P_n =$	330	[T]
Moment	$\phi M_n =$	33	[T-m]
Separate Steel 2 group	1 st.	10	$A_s = 49.1$ [cm ²]
	2 nd.	10	$A_s = 49.1$ [cm ²]
Steel Reinforcement	No.	20	
	$d =$	96	[cm]
$d(e_u / (e_y + e_u))$	$C_b =$	58.055	[cm]
	p of Steel	0.012	OK
Main Steel Used	20 DB 25		
Stirrup	DB 12 @ 0.400		
$e_b =$	0.32		[cm]

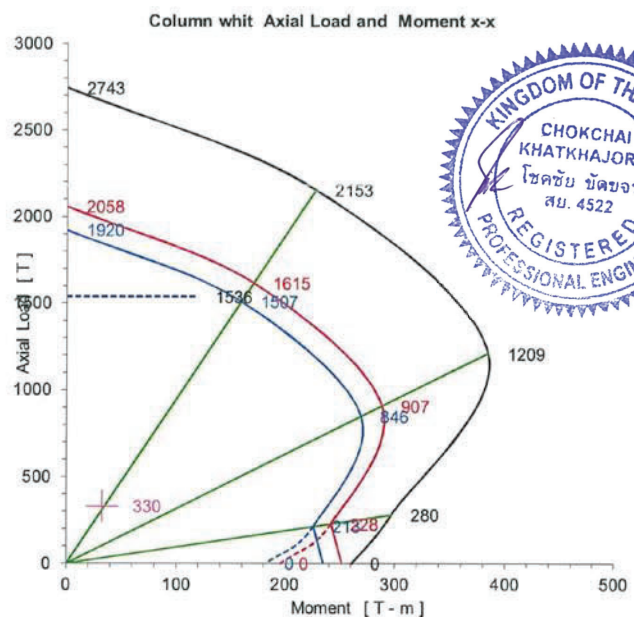


Column (80 x 100)
Steel 20 DB 25
Stirrup DB 12 @ 0.400

Boundary of tie stirrup Column
Boundary of spiral stirrup Column
Boundary of Ultimate Capacity



Column C-9 (80 x 100)



DYNAMIC ENGINEERING CONSULTANT CO., LTD.

Column Whit Axial Force and Moment X - X

(Ultimate Stress Design method in accordance with ACI 318)

Job No. : 193018

Rev. : 0

Initial : CKJ

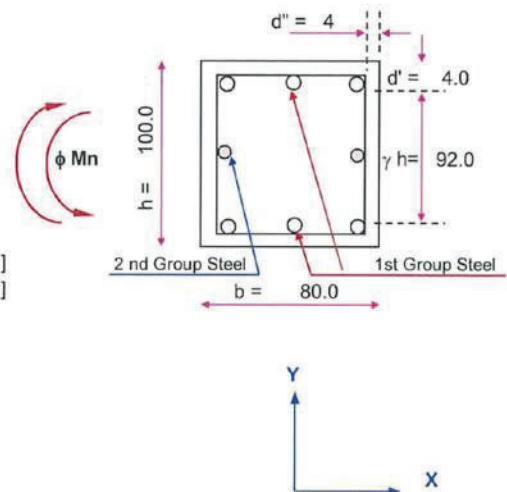
Date : 23-Dec-20

Column No. C-9 2nd-Roof

Project : อาคารทิศตะวันตก

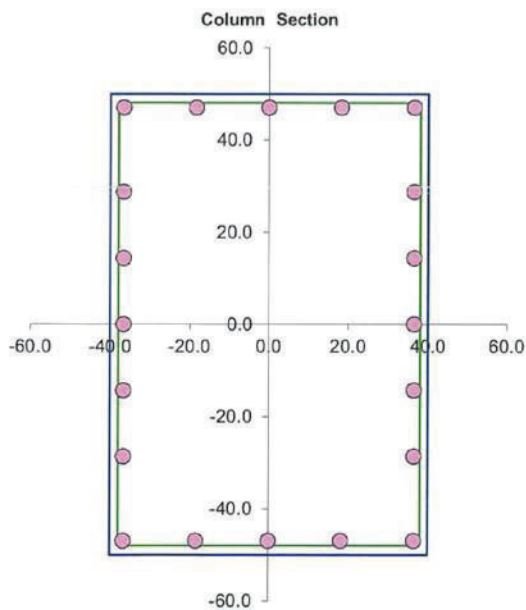
filename : COLUMN

Concrete Strength	f_c' =	350	[kg/cm ²]
	f_y SD =	4000	[kg/cm ²]
	f_y RD =	2400	[kg/cm ²]
Column Dimension	b =	80	[cm]
	h =	100	[cm]
	d' =	4	[cm]
	d'' =	4	[cm]
Load	ϕP_n =	165	[T]
Moment	ϕM_n =	16	[T-m]
Separate Steel 2 group	1 st. =	10	$A_s = 49.1$ [cm ²]
	2 nd. =	10	$A_s = 49.1$ [cm ²]
Steel Reinforcement	No. =	20	
	d =	96	[cm]
$d(\epsilon_u / (\epsilon_y + \epsilon_u))$	C_b =	58.055	[cm]
	p of Steel =	0.012	OK
Main Steel Used	20 DB 25		
Stirrup	RB 9 @ 0.400		
e/b =	0.32		[cm]

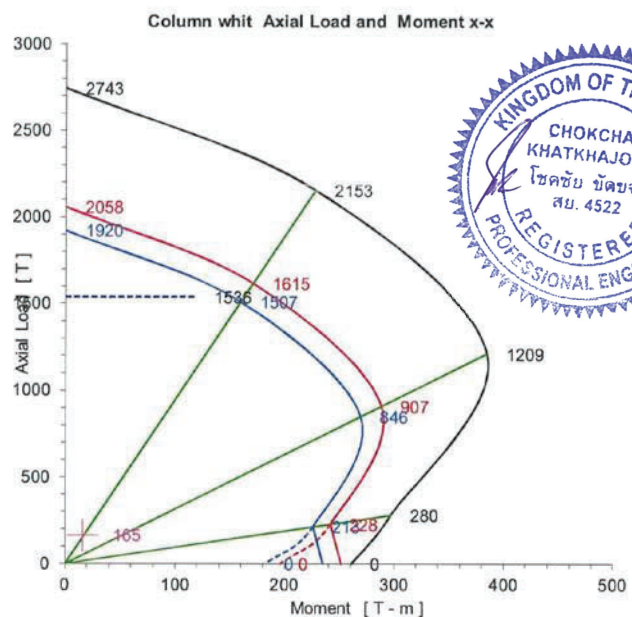


Column (80 x 100)
Steel 20 DB 25
Stirrup RB 9 @ 0.400

Boundary of tie stirrup Column
Boundary of spiral stirrup Column
Boundary of Ultimate Capacity



Column C-9 (80 x 100)



DYNAMIC ENGINEERING CONSULTANT CO., LTD.

Column Whit Axial Force and Moment X - X

(Ultimate Stress Design method in accordance with ACI 318)

Job No. : 193018

Rev. : 0

Initial : CKJ

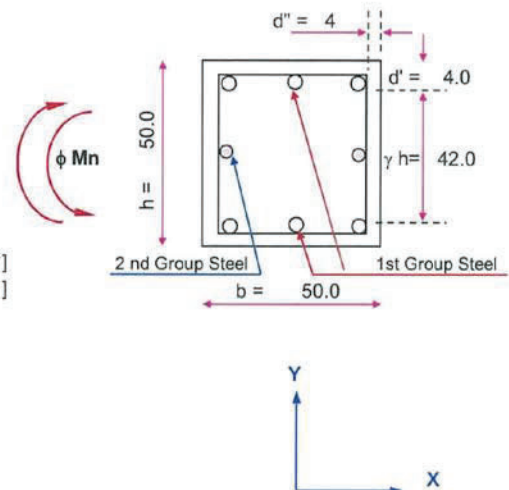
Date : 23-Dec-20

Column No. C-10 1st

Project : อาคารทิศตะวันตก

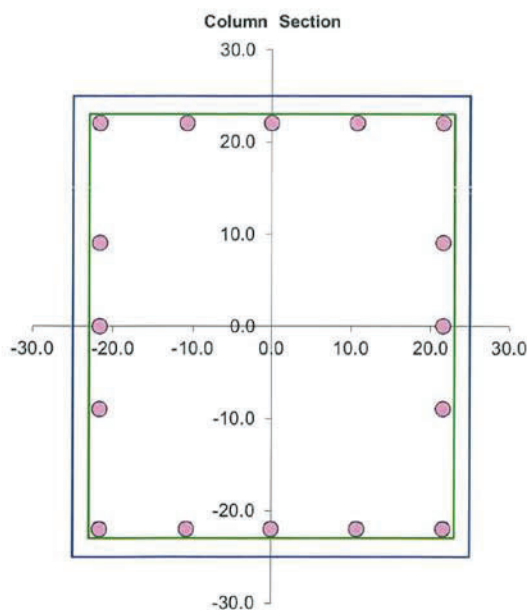
filename : COLUMN

Concrete Strength	f_c' =	350	[kg/cm ²]
	f_y SD =	4000	[kg/cm ²]
	f_y RD =	2400	[kg/cm ²]
Column Dimension	b =	50	[cm]
	h =	50	[cm]
	d' =	4	[cm]
	d'' =	4	[cm]
Load	ϕP_n =	350	[T]
Moment	ϕM_n =	35	[T-m]
Separate Steel 2 group	1 st. =	10	$A_s = 49.1$ [cm ²]
	2 nd. =	6	$A_s = 29.5$ [cm ²]
Steel Reinforcement	No. =	16	
	d =	46	[cm]
$d(e_u / (e_y + e_u))$	C_b =	27.818	[cm]
	ρ of Steel =	0.031	OK
Main Steel Used	16 DB 25		
Stirrup	RB 9 @ 0.400		
e/b =	0.24		[cm]

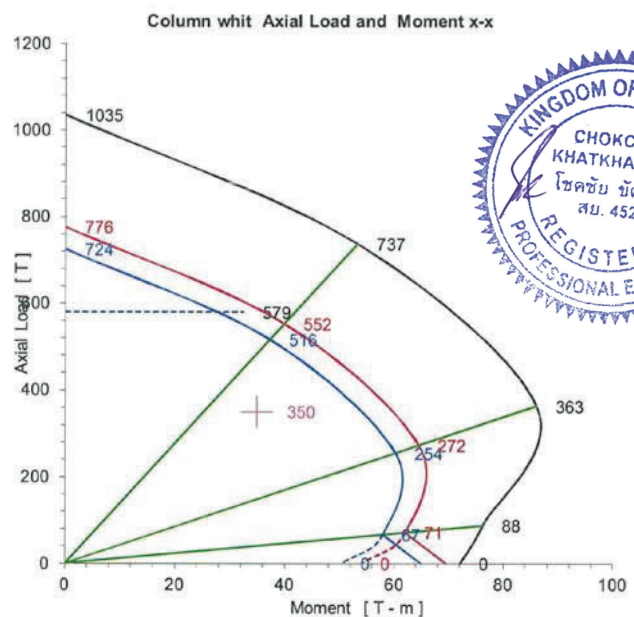


Column (50 x 50)
Steel 16 DB 25
Stirrup RB 9 @ 0.400

Boundary of tie stirrup Column
Boundary of spiral stirrup Column
Boundary of Ultimate Capacity



Column C-10 (50 x 50)



DYNAMIC ENGINEERING CONSULTANT CO., LTD.

Column Whit Axial Force and Moment X - X

(Ultimate Stress Design method in accordance with ACI 318)

Job No. : 193018

Rev. : 0

Initial : CKJ

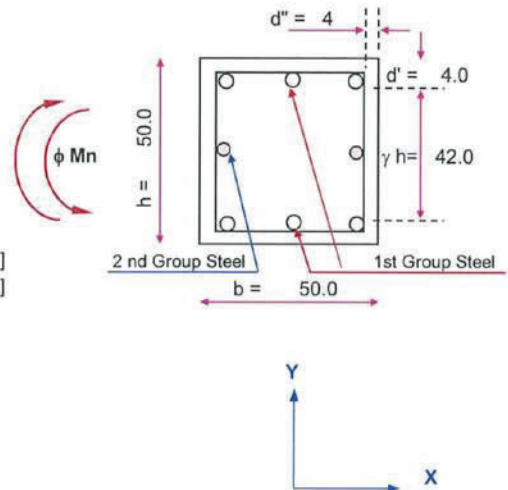
Date : 23-Dec-20

Column No. C-10 2nd-Roof

Project : อาคารทิศตะวันตก

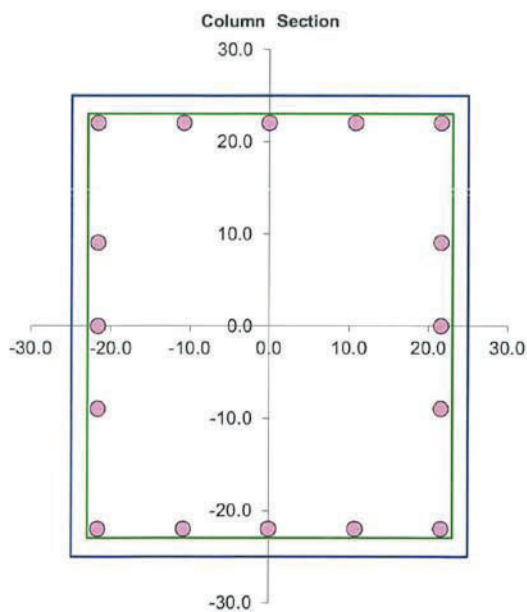
filename : COLUMN

Concrete Strength	$f_c' =$	350	[kg/cm ²]
	f_y SD	4000	[kg/cm ²]
	f_y RD	2400	[kg/cm ²]
Column Dimension	$b =$	50	[cm]
	$h =$	50	[cm]
	$d' =$	4	[cm]
	$d'' =$	4	[cm]
Load	$\phi P_n =$	125	[T]
Moment	$\phi M_n =$	13	[T-m]
Separate Steel 2 group	1 st.	10	$A_s = 49.1$ [cm ²]
	2 nd.	6	$A_s = 29.5$ [cm ²]
Steel Reinforcement	No.	16	
	$d =$	46	[cm]
$d(\epsilon_u/(\epsilon_y + \epsilon_u))$	$C_b =$	27.818	[cm]
	p of Steel =	0.031	OK
Main Steel Used	16 DB 25		
Stirrup	RB 9 @ 0.400		
e b =	0.24		[cm]

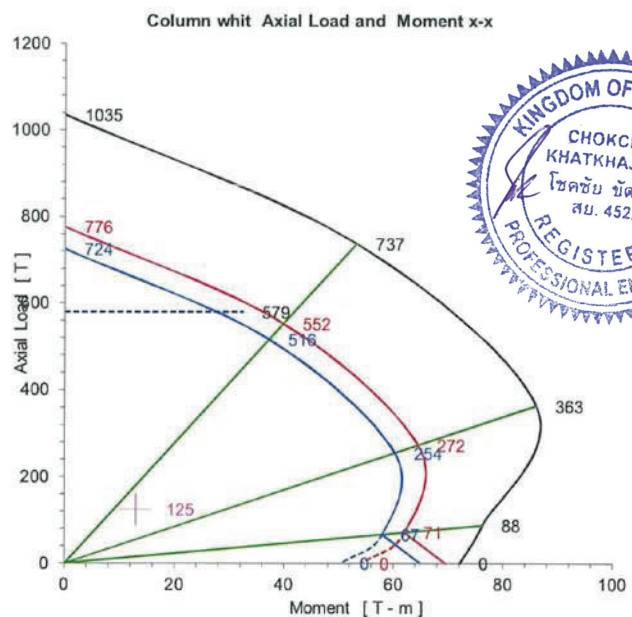


Column (50 x 50)
Steel 16 DB 25
Stirrup RB 9 @ 0.400

Boundary of tie stirrup Column
Boundary of spiral stirrup Column
Boundary of Ultimate Capacity



Column C-10 (50 x 50)



DYNAMIC ENGINEERING CONSULTANT CO., LTD.

Column Whit Axial Force and Moment X - X

(Ultimate Stress Design method in accordance with ACI 318)

Job No. : 193018

Rev. : 0

Initial : CKJ

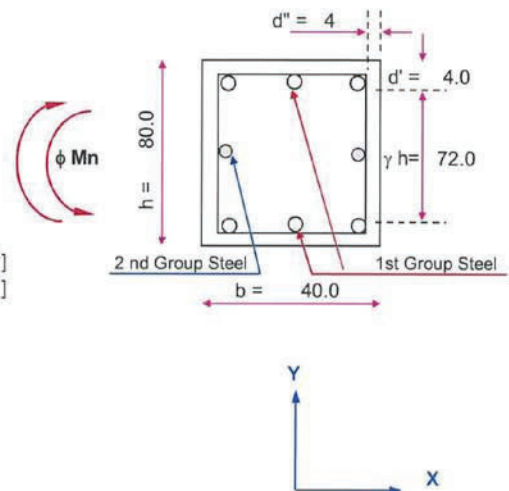
Date : 8-Oct-20

Column No. CC-1 Roof FL.

Project : อาคารทิศตะวันตก

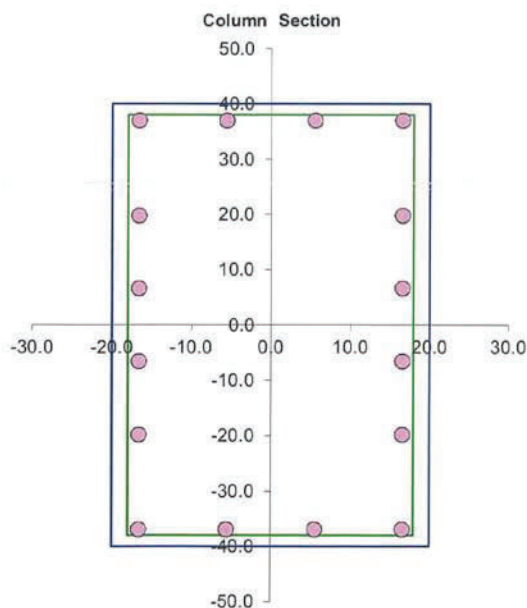
filename : COLUMN

Concrete Strength	$f_c' =$	350	[kg/cm ²]
	f_y SD	4000	[kg/cm ²]
	f_y RD	2400	[kg/cm ²]
Column Dimension	$b =$	40	[cm]
	$h =$	80	[cm]
	$d' =$	4	[cm]
	$d'' =$	4	[cm]
Load	$\phi P_n =$	7.5	[T]
Moment	$\phi M_n =$	0.7	[T-m]
Separate Steel 2 group	1 st.	8	$A_s = 16.1$ [cm ²]
	2 nd.	8	$A_s = 16.1$ [cm ²]
Steel Reinforcement	No.	16	
	$d =$	76	[cm]
	$C_b =$	45.960	[cm]
	p of Steel	0.010	OK
Main Steel Used	16 DB 16		
Stirrup	RB 9 @ 0.250		
$e/b =$	0.25		[cm]

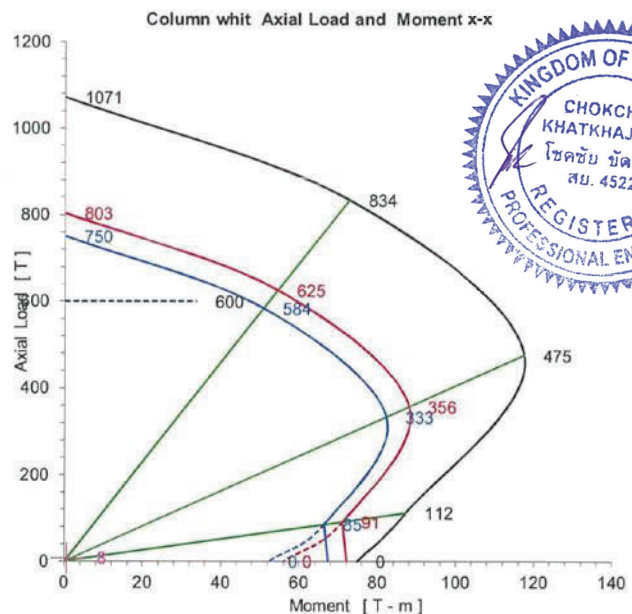


Column (40 x 80)
Steel 16 DB 16
Stirrup RB 9 @ 0.250

— Boundary of tie stirrup Column
— Boundary of spiral stirrup Column
— Boundary of Ultimate Capacity



Column CC-1 (40 x 80)



DYNAMIC ENGINEERING CONSULTANT CO., LTD.

Column Whit Axial Force and Moment X - X

(Ultimate Stress Design method in accordance with ACI 318)

Job No. : 193018

Rev. : 0

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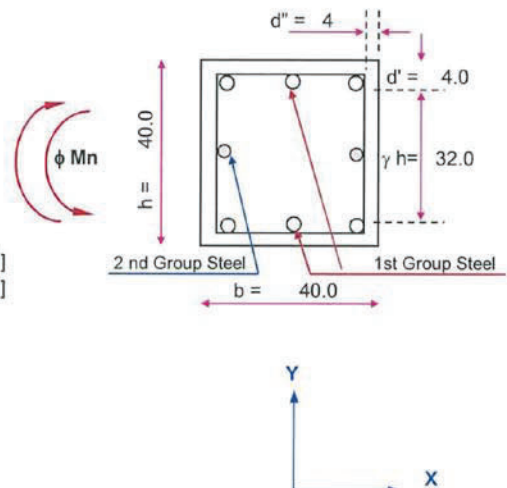
Date : 8-Oct-20

Column No. CT-1 Roof FL.

Project : อาคารทิศตะวันตก

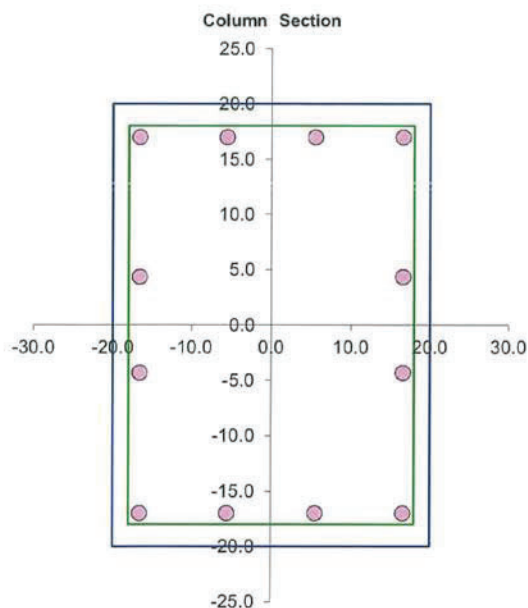
filename : COLUMN

Concrete Strength	f_c' =	350	[kg/cm ²]
	f_y SD =	4000	[kg/cm ²]
	f_y RD =	2400	[kg/cm ²]
Column Dimension	b =	40	[cm]
	h =	40	[cm]
	d' =	4	[cm]
	d'' =	4	[cm]
Load	ϕP_n =	5	[T]
Moment	ϕM_n =	1	[T-m]
Separate Steel 2 group	1 st. =	8	$A_s = 16.1$ [cm ²]
	2 nd. =	4	$A_s = 8.0$ [cm ²]
Steel Reinforcement	No. =	12	
	d =	36	[cm]
	C_b =	21.771	[cm]
	ρ of Steel =	0.015	OK
Main Steel Used	12 DB 16		
Stirrup	RB 9 @ 0.250		
e b =	0.15	[cm]	

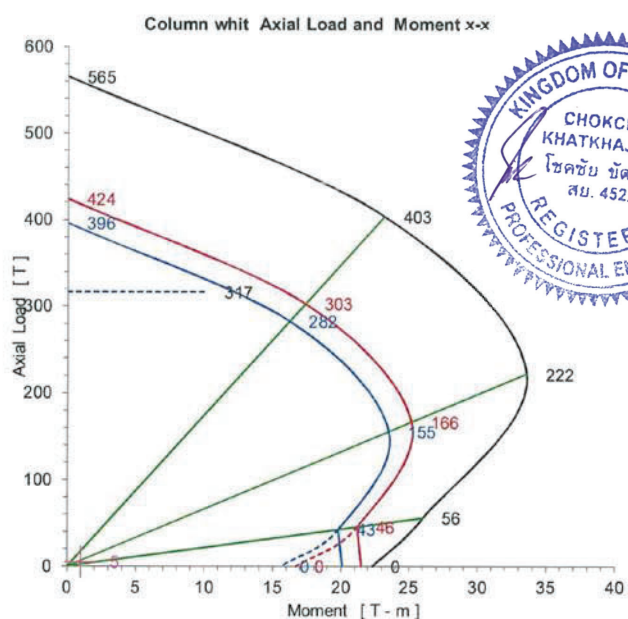


Column (40 x 40)
Steel 12 DB 16
Stirrup RB 9 @ 0.250

Boundary of tie stirrup Column
Boundary of spiral stirrup Column
Boundary of Ultimate Capacity



Column CT-1 (40 x 40)



DYNAMIC ENGINEERING CONSULTANT CO., LTD.

Column Whit Axial Force and Moment X - X

(Ultimate Stress Design method in accordance with ACI 318)

Job No. : 193018

Rev. : 0

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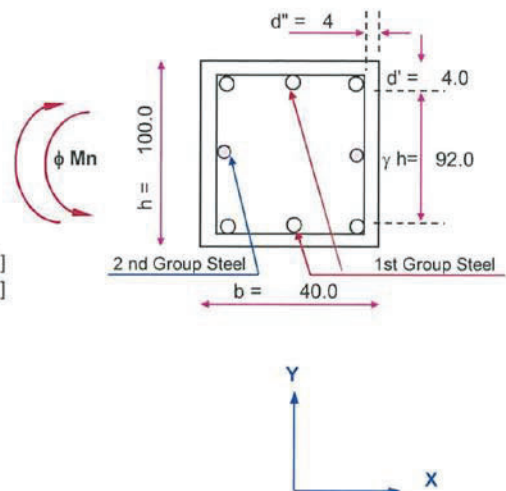
Date : 8-Oct-20

Column No. CR-1 Roof FL.

Project : อาคารทิศตะวันตก

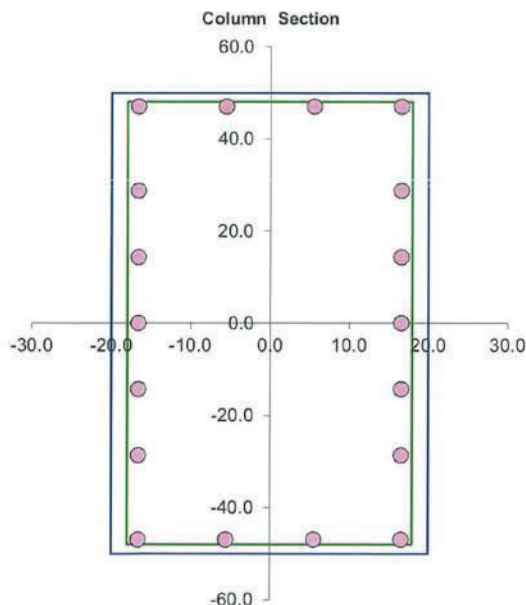
filename : COLUMN

Concrete Strength	$f_c' =$	350	[kg/cm ²]
	f_y SD	4000	[kg/cm ²]
	f_y RD	2400	[kg/cm ²]
Column Dimension	$b =$	40	[cm]
	$h =$	100	[cm]
	$d' =$	4	[cm]
	$d'' =$	4	[cm]
Load	$\phi P_n =$	35	[T]
Moment	$\phi M_n =$	3.5	[T-m]
Separate Steel 2 group	1 st.	8	$A_s = 25.1$ [cm ²]
	2 nd.	10	$A_s = 31.4$ [cm ²]
Steel Reinforcement	No.	18	
	$d =$	96	[cm]
	$C_b =$	58.055	[cm]
	ρ of Steel	0.014	OK
Main Steel Used	18 DB 20		
Stirrup	RB 9 @ 0.300		
$e/b =$	0.32		[cm]

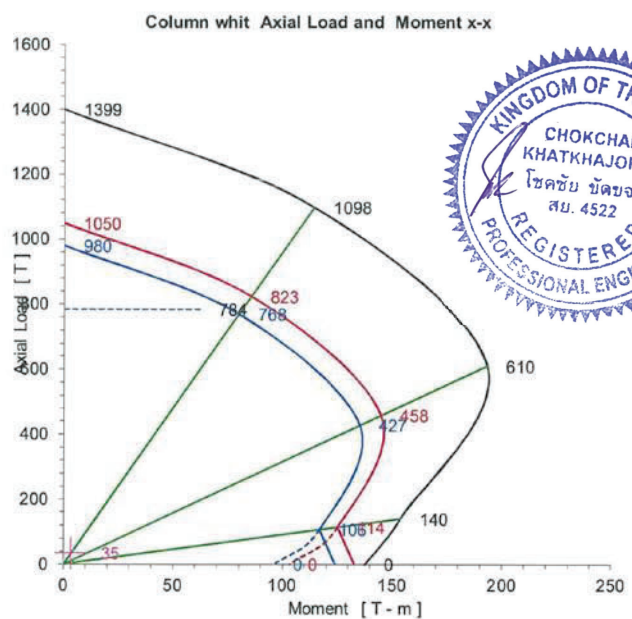


Column (40 x 100)
Steel 18 DB 20
Stirrup RB 9 @ 0.300

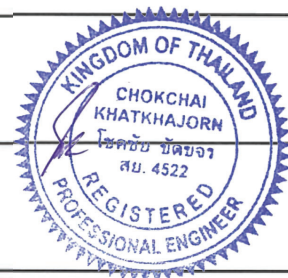
— Boundary of tie stirrup Column
— Boundary of spiral stirrup Column
— Boundary of Ultimate Capacity

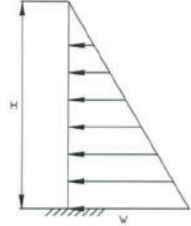


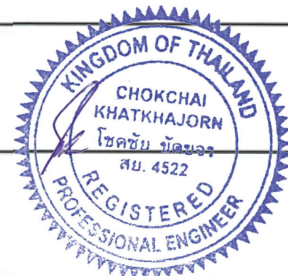
Column CR-1 (40 x 100)



DYNAMIC ENGINEERING CONSULTANTS CO., LTD. 281 SOI PHANIT ANAN 7 SUKHUMVIT 71 BANGKOK 10110 PHONE: (66-2) 713-3888, FAX: (66-2) 713-3889	<table style="width: 100%;"> <tr> <td style="width: 50%;"> Project No. : 193018 Project Name : อาคารทิศตะวันตก Subject : WALL TANK Made by : โชคชัย </td> <td style="width: 50%;"> Date : 10/1/2020 Checked by : โชคชัย </td> </tr> </table>	Project No. : 193018 Project Name : อาคารทิศตะวันตก Subject : WALL TANK Made by : โชคชัย	Date : 10/1/2020 Checked by : โชคชัย																																																														
Project No. : 193018 Project Name : อาคารทิศตะวันตก Subject : WALL TANK Made by : โชคชัย	Date : 10/1/2020 Checked by : โชคชัย																																																																
Member : WT 1 SLAB DESIGN (USD)																																																																	
<table style="width: 100%;"> <tr> <td>Pile Size</td><td>=</td><td>0.00</td><td>cm.</td></tr> <tr> <td>Hight, H</td><td>=</td><td>2.50</td><td>m.</td></tr> <tr> <td>Water Load</td><td>=</td><td>1000</td><td>kg / m²</td></tr> <tr> <td>Soil Load</td><td>=</td><td>0</td><td>kg / m²</td></tr> <tr> <td>W_U = 1.4W</td><td>=</td><td>2072</td><td>kg / m²</td></tr> <tr> <td>Thickness</td><td>=</td><td>20.0</td><td>cm</td></tr> <tr> <td>M-pos.</td><td>=</td><td>863</td><td>kg-m / m</td></tr> <tr> <td>Max. Shear</td><td>=</td><td>2590</td><td>kg / m</td></tr> </table>	Pile Size	=	0.00	cm.	Hight, H	=	2.50	m.	Water Load	=	1000	kg / m ²	Soil Load	=	0	kg / m ²	W _U = 1.4W	=	2072	kg / m ²	Thickness	=	20.0	cm	M-pos.	=	863	kg-m / m	Max. Shear	=	2590	kg / m	<table style="width: 100%;"> <tr> <td>Conc. fc'</td><td>350</td><td>kg / cm²</td></tr> <tr> <td>Steel fy</td><td>4000</td><td>kg / cm²</td></tr> <tr> <td>β₁</td><td>=</td><td>0.80</td></tr> <tr> <td>ρ_b</td><td>=</td><td>0.036</td></tr> <tr> <td>φM_n</td><td>=</td><td>14898</td><td>kg-m / m</td></tr> <tr> <td>Cover (Short Side)</td><td>=</td><td>5.00</td><td>cm</td></tr> <tr> <td>Cover (Long Side)</td><td>=</td><td>5.00</td><td>cm</td></tr> <tr> <td>Required Thickness</td><td>=</td><td>8.61</td><td>cm</td></tr> <tr> <td>Required d</td><td>=</td><td>3.61</td><td>cm</td></tr> </table>	Conc. fc'	350	kg / cm ²	Steel fy	4000	kg / cm ²	β ₁	=	0.80	ρ _b	=	0.036	φM _n	=	14898	kg-m / m	Cover (Short Side)	=	5.00	cm	Cover (Long Side)	=	5.00	cm	Required Thickness	=	8.61	cm	Required d	=	3.61	cm
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 DYNAMIC ENGINEERING CONSULTANTS CO., LTD. 281 SOI PHANIT ANAN 7 SUKHUMMIT 71 BANGKOK 10110 PHONE: (66-2) 713-3888, FAX: (66-2) 713-3889	Project No. : 193018 Project Name : อาคารทิศตะวันตก Subject : กระบะปลูกต้นไม้ Made by : โชคชัย	Date : 10/1/2020 Checked by : โชคชัย																				
Member : W120 SLAB DESIGN (USD)																						
																						
Pile Size = 0.00 cm. Hight, H = 0.75 m. Water Load = 0 kg / m ² Soil Load = 1800 kg / m ² W _U = 1.4W = 3192 kg / m ² Thickness = 20.0 cm M-pos. = 120 kg-m / m Max. Shear = 1197 kg / m	Conc. fc' = 350 kg / cm ² Steel fy = 4000 kg / cm ² β ₁ = 0.80 ρ _b = 0.036 Cover (Short Side) = 4.00 cm Cover (Long Side) = 4.00 cm Required Thickness = 5.34 cm Required d = 1.34 cm	R = 73.57 kg / cm ² φM _n = 16951 kg-m / m																				
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รายงานการออกแบบ Design Note รายการคำนวณงานโครงสร้าง

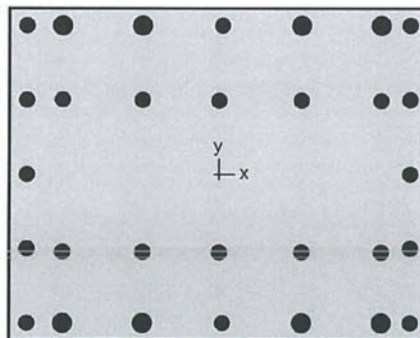
(สัญญาก่อสร้างอาคารทิศตะวันตก Final Detailed Design)

(ส่วนงานโครงสร้าง งานสถาปัตยกรรม และงานระบบหลัก)

โครงการพัฒนาพื้นที่ส่วนขยายศูนย์ราชการเฉลิมพระเกียรติ ๘๐ พรรษา ๕ ธันวาคม ๒๕๕๐ พื้นที่โซน C



spColumn v6.50
Computer program for the Strength Design of Reinforced Concrete Sections
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Contents

1. General Information	3
2. Material Properties	3
2.1. Concrete	3
2.2. Steel	3
3. Section	3
3.1. Shape and Properties	3
3.2. Section Figure	4
3.3. Exterior Points	4
4. Reinforcement	4
4.1. Bar Set: ASTM A615	4
4.2. Confinement and Factors	4
4.3. Arrangement	4
4.4. Bars Provided	5
5. Factored Loads and Moments with Corresponding Capacity Ratios	5
6. Diagrams	6
6.1. PM at $\theta=26$ [deg]	6
6.2. MM at $P=12770$ [kN]	7

List of Figures

Figure 1: Column section	4
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Page | 3
9/18/2020
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1. General Information

File Name	C:\193018\GCDT\SPcolumn\10-09-63(C1 building)\SP(column)\C1-L2(revised).col
Project	---
Column	---
Engineer	---
Code	ACI 318-14
Bar Set	ASTM A615
Units	Metric
Run Option	Investigation
Run Axis	Biaxial
Slenderness	Not Considered
Column Type	Structural
Capacity Method	Critical capacity

2. Material Properties

2.1. Concrete

Type	Standard
f_c	34 MPa
E_c	27405.5 MPa
f_c	28.9 MPa
ϵ_u	0.003 mm/mm
β_1	0.803444

2.2. Steel

Type	Standard
f_y	400 MPa
E_s	200000 MPa
ϵ_{yt}	0.002 mm/mm

3. Section

3.1. Shape and Properties

Type	Irregular
A_g	800000 mm ²
I_x	4.26667e+010 mm ⁴
I_y	6.66667e+010 mm ⁴
r_x	230.94 mm
r_y	288.675 mm
X_o	0 mm
Y_o	0 mm



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Page | 4
9/18/2020
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3.2. Section Figure

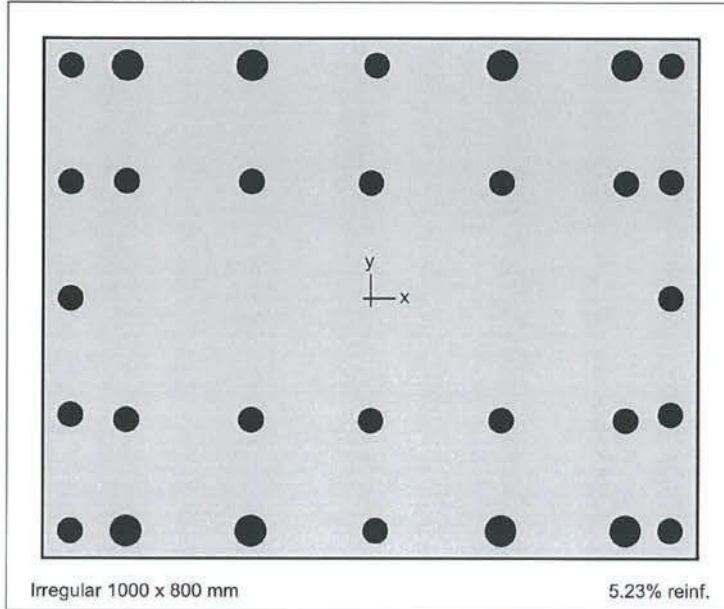


Figure 1: Column section

3.3. Exterior Points

Points	X mm	Y mm	Points	X mm	Y mm	Points	X mm	Y mm
1	-500.0	-400.0	2	500.0	-400.0	3	500.0	400.0
4	-500.0	400.0						

4. Reinforcement

4.1. Bar Set: ASTM A615

Bar	Diameter mm	Area mm ²	Bar	Diameter mm	Area mm ²	Bar	Diameter mm	Area mm ²
#3	9.53	70.97	#4	12.70	129.03	#5	15.88	200.00
#6	19.05	283.87	#7	22.23	387.10	#8	25.40	509.68
#9	28.65	645.16	#10	32.26	819.35	#11	35.81	1006.45
#14	43.00	1451.61	#18	57.33	2580.64			

4.2. Confinement and Factors

Confinement type	Tied
For #10 bars or less	#3 ties
For larger bars	#4 ties
Capacity Reduction Factors	
Axial compression, (a)	0.8
Tension controlled ϕ , (b)	0.9
Compression controlled ϕ , (c)	0.65

4.3. Arrangement

Pattern	Irregular
Bar layout	---
Cover to	---
Clear cover	---



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Page | 5

9/18/2020

1:32 PM

Bars	---
Total steel area, A_s	41820 mm ²
Rho	5.23 %
Minimum clear spacing	25 mm

4.4. Bars Provided

Area mm ²	X mm	Y mm	Area mm ²	X mm	Y mm	Area mm ²	X mm	Y mm
1230.0	-458.0	-358.0	1230.0	-458.0	-179.0	1230.0	-458.0	0.0
1230.0	-458.0	179.0	1230.0	-458.0	358.0	1230.0	458.0	-358.0
1230.0	458.0	-179.0	1230.0	458.0	0.0	1230.0	458.0	179.0
1230.0	458.0	358.0	1845.0	-373.0	358.0	1845.0	-182.5	358.0
1230.0	8.0	358.0	1845.0	198.5	358.0	1845.0	389.0	358.0
1845.0	-373.0	-358.0	1845.0	-182.5	-358.0	1230.0	8.0	-358.0
1845.0	198.5	-358.0	1845.0	389.0	-358.0	1230.0	-373.0	-186.5
1230.0	-182.5	-187.0	1230.0	198.5	-187.8	1230.0	389.0	-188.2
1230.0	-373.0	180.3	1230.0	-182.5	179.5	1230.0	198.5	177.7
1230.0	389.0	176.9	1230.0	0.0	-188.0	1230.0	0.0	177.5

5. Factored Loads and Moments with Corresponding Capacity Ratios

NOTE: Calculations are based on "Critical Capacity" Method.

No.	Demand			Capacity			Parameters at Capacity			Capacity Ratio
	P_u	M_{ux}	M_{uy}	ϕP_n	ϕM_{nx}	ϕM_{ny}	NA Depth	ϵ_t	ϕ	
	kN	kNm	kNm	kN	kNm	kNm	mm			
1	-4570.00	23.90	127.50	-10707.41	353.64	1886.58	95	0.03196	0.900	0.48
2	12770.00	62.10	30.30	20092.49	62.10	30.30	1038	-0.00014	0.650	0.64
3	6550.00	165.00	638.00	12513.11	881.96	3410.23	863	0.00112	0.650	0.38
4	6962.00	334.00	182.00	20092.49	334.00	182.00	1056	-0.00011	0.650	0.35
5	8518.00	340.00	51.00	20092.49	340.00	51.00	924	-0.00033	0.650	0.42
6	8110.00	161.00	647.00	14732.07	768.06	3086.56	952	0.00071	0.650	0.42



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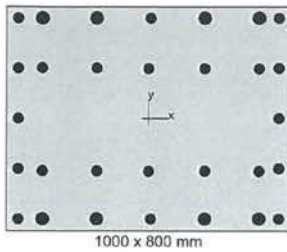
Page | 6

9/18/2020

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6. Diagrams

6.1. PM at $\theta=26$ [deg]



General Information

Project	---
Column	---
Engineer	---
Code	ACI 318-14
Bar Set	ASTM A615
Units	Metric
Run Option	Investigation
Run Axis	Biaxial
Slenderness	Not Considered
Column Type	Structural
Capacity Method	Critical capacity

Materials

f_c	34 MPa
E_c	27405.5 MPa
f_y	400 MPa
E_s	200000 MPa

Section

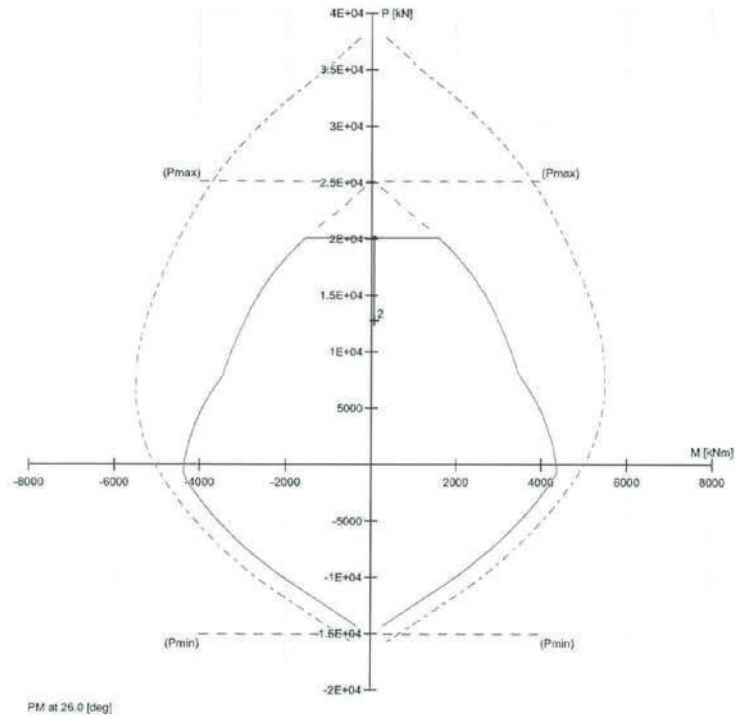
Type	Irregular
A_g	800000 mm ²
I_x	4.26667e+010 mm ⁴
I_y	6.66667e+010 mm ⁴

Reinforcement

Pattern	Irregular
Bar layout	---
Cover to	---
Clear cover	---
Bars	---

Confinement type

Confinement type	Tied
Total steel area, A_s	41820 mm ²
Rho	5.23 %
Min. clear spacing	25 mm



PM at 26.0 [deg]

No.	P_u kN	M_{ux} kNm	M_{uy} kNm	ϕP_n kN	ϕM_{nx} kNm	ϕM_{ny} kNm	Capacity Ratio
2	12770.0	62.1	30.3	20092.49	62.10	30.30	0.64

Max. Capacity Ratio: 0.64



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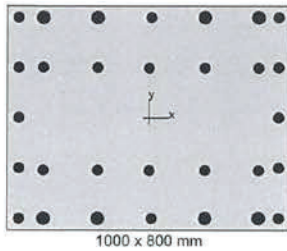
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Page | 7

9/18/2020

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6.2. MM at P=12770 [kN]



General Information

Project	---
Column	---
Engineer	---
Code	ACI 318-14
Bar Set	ASTM A615
Units	Metric
Run Option	Investigation
Run Axis	Biaxial
Slenderness	Not Considered
Column Type	Structural
Capacity Method	Critical capacity

Materials

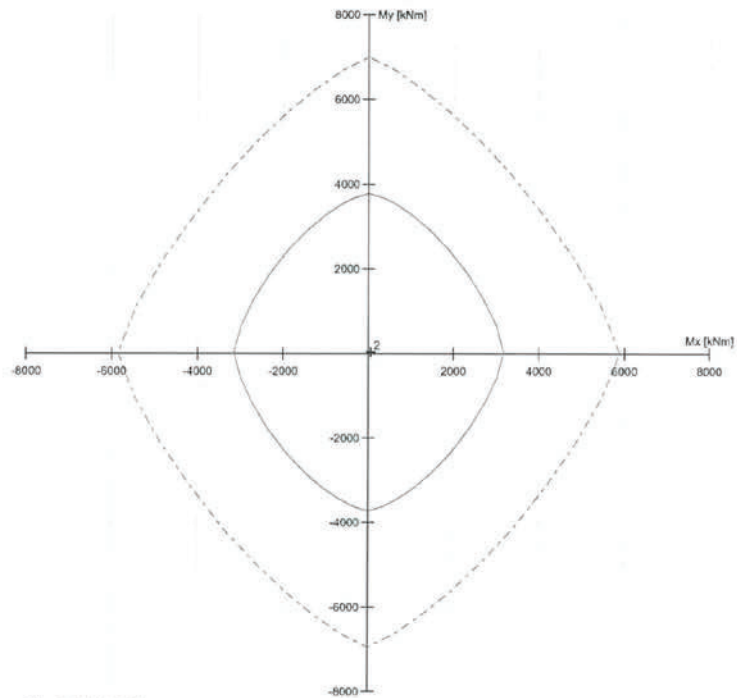
f_c	34 MPa
E_c	27405.5 MPa
f_y	400 MPa
E_s	200000 MPa

Section

Type	Irregular
A_g	800000 mm ²
I_x	4.26667e+010 mm ⁴
I_y	6.66667e+010 mm ⁴

Reinforcement

Pattern	Irregular
Bar layout	---
Cover to	---
Clear cover	---
Bars	---
Confinement type	Tied
Total steel area, A_s	41820 mm ²
Rho	5.23 %
Min. clear spacing	25 mm



No.	P_u kN	M_{ux} kNm	M_{uy} kNm	ϕP_n kN	ϕM_{nx} kNm	ϕM_{ny} kNm	Capacity Ratio
2	12770.0	62.1	30.3	20092.49	62.10	30.30	0.64

Max. Capacity Ratio: 0.64





รายงานการออกแบบ Design Note รายการคำนวณงานโครงสร้าง

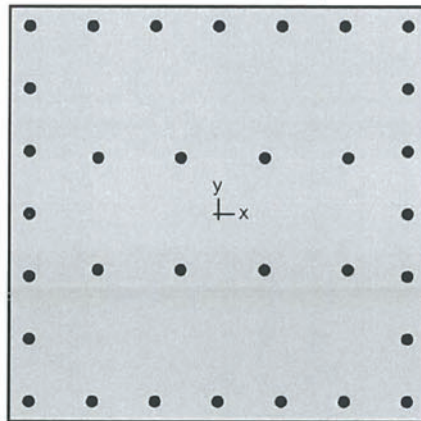
(สัญญาก่อสร้างอาคารทิศตะวันตก Final Detailed Design)

(ส่วนงานโครงสร้าง งานสถาปัตยกรรม และงานระบบหลัก)

โครงการพัฒนาพื้นที่ส่วนขยายศูนย์ราชการเฉลิมพระเกียรติ ๘๐ พรรษา ๕ ธันวาคม ๒๕๕๐ พื้นที่โซน C



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Contents

1. General Information	3
2. Material Properties	3
2.1. Concrete	3
2.2. Steel	3
3. Section	3
3.1. Shape and Properties	3
3.2. Section Figure	4
3.3. Exterior Points	4
4. Reinforcement	4
4.1. Bar Set: ASTM A615	4
4.2. Confinement and Factors	4
4.3. Arrangement	4
4.4. Bars Provided	5
5. Factored Loads and Moments with Corresponding Capacity Ratios	5
6. Diagrams	6
6.1. PM at $\theta=29$ [deg]	6
6.2. MM at $P=22110$ [kN]	7

List of Figures

Figure 1: Column section	4
--------------------------------	---



1. General Information

File Name	C:\193018\GCDT\SPcolumn\10-09-63(C1 ...)\C2-L2.col
Project	---
Column	---
Engineer	---
Code	ACI 318-14
Bar Set	ASTM A615
Units	Metric
Run Option	Investigation
Run Axis	Biaxial
Slenderness	Not Considered
Column Type	Structural
Capacity Method	Critical capacity

2. Material Properties

2.1. Concrete

Type	Standard
f_c	35 MPa
E_c	27805.6 MPa
f_{ct}	29.75 MPa
ϵ_u	0.003 mm/mm
β_1	0.796192

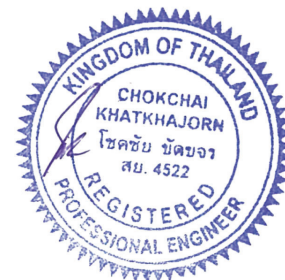
2.2. Steel

Type	Standard
f_y	400 MPa
E_s	200000 MPa
ϵ_{yt}	0.002 mm/mm

3. Section

3.1. Shape and Properties

Type	Irregular
A_g	1.44e+006 mm ²
I_x	1.728e+011 mm ⁴
I_y	1.728e+011 mm ⁴
r_x	346.41 mm
r_y	346.41 mm
X_o	0 mm
Y_o	0 mm



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Page | 4

9/18/2020

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3.2. Section Figure

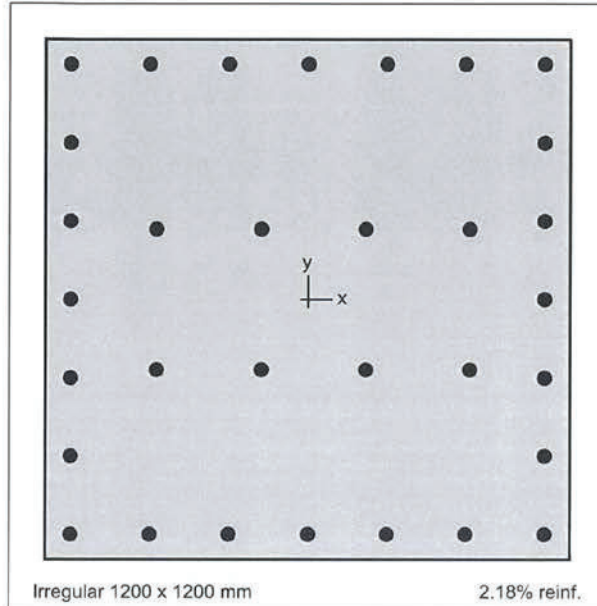


Figure 1: Column section

3.3. Exterior Points

Points	X mm	Y mm	Points	X mm	Y mm	Points	X mm	Y mm
1	-600.0	-600.0	2	600.0	-600.0	3	600.0	600.0
4	-600.0	600.0						

4. Reinforcement

4.1. Bar Set: ASTM A615

Bar	Diameter mm	Area mm ²	Bar	Diameter mm	Area mm ²	Bar	Diameter mm	Area mm ²
#3	9.53	70.97	#4	12.70	129.03	#5	15.88	200.00
#6	19.05	283.87	#7	22.23	387.10	#8	25.40	509.68
#9	28.65	645.16	#10	32.26	819.35	#11	35.81	1006.45
#14	43.00	1451.61	#18	57.33	2580.64			

4.2. Confinement and Factors

Confinement type	Tied
For #10 bars or less	#3 ties
For larger bars	#4 ties
Capacity Reduction Factors	
Axial compression, (a)	0.8
Tension controlled ϕ , (b)	0.9
Compression controlled ϕ , (c)	0.65

4.3. Arrangement

Pattern	Irregular
Bar layout	---
Cover to	---
Clear cover	---



Bars	---
Total steel area, A_s	31424 mm ²
Rho	2.18 %
Minimum clear spacing	137 mm

4.4. Bars Provided

Area mm ²	X mm	Y mm	Area mm ²	X mm	Y mm	Area mm ²	X mm	Y mm
982.0	-542.3	-542.3	982.0	-542.3	-361.5	982.0	-542.3	-180.8
982.0	-542.3	0.0	982.0	-542.3	180.8	982.0	-542.3	361.5
982.0	-542.3	542.3	982.0	-361.5	-542.3	982.0	-180.8	-542.3
982.0	0.0	-542.3	982.0	180.8	-542.3	982.0	361.5	-542.3
982.0	542.3	-542.3	982.0	542.3	-361.5	982.0	542.3	-180.8
982.0	542.3	0.0	982.0	542.3	180.8	982.0	542.3	361.5
982.0	542.3	542.3	982.0	-361.5	542.3	982.0	-180.8	542.3
982.0	0.0	542.3	982.0	180.8	542.3	982.0	361.5	542.3
982.0	-346.0	162.0	982.0	-107.0	162.0	982.0	132.1	162.0
982.0	371.1	162.0	982.0	-346.0	-162.0	982.0	-107.0	-162.0
982.0	132.1	-162.0	982.0	371.1	-162.0			

5. Factored Loads and Moments with Corresponding Capacity Ratios

NOTE: Calculations are based on "Critical Capacity" Method.

No.	Demand			Capacity			Parameters at Capacity			Capacity Ratio
	P_u	M_{ux}	M_{uy}	ϕP_n	ϕM_{nx}	ϕM_{ny}	NA Depth	ϵ_t	ϕ	
	kN	kNm	kNm	kN	kNm	kNm	mm			
1	4447.00	137.00	259.00	0.00	2604.72	4924.26	482	0.00646	0.900	0.18
2	22110.00	155.00	87.50	28326.86	155.00	87.50	1484	0.00006	0.650	0.78
3	14460.00	349.00	3255.00	19904.94	597.68	5574.39	1007	0.00085	0.650	0.64
4	13900.00	1050.00	2640.00	20583.60	1942.03	4882.82	1170	0.00090	0.650	0.57



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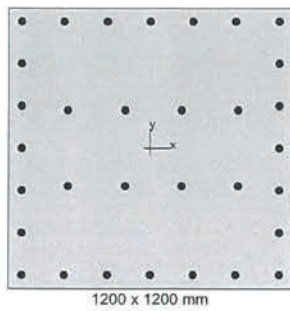
Page | 6

9/18/2020

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6. Diagrams

6.1. PM at $\theta=29$ [deg]



General Information

Project	---
Column	---
Engineer	---
Code	ACI 318-14
Bar Set	ASTM A615
Units	Metric
Run Option	Investigation
Run Axis	Biaxial
Slenderness	Not Considered
Column Type	Structural
Capacity Method	Critical capacity

Materials

f'_c	35 MPa
E_c	27805.6 MPa
f_y	400 MPa
E_s	200000 MPa

Section

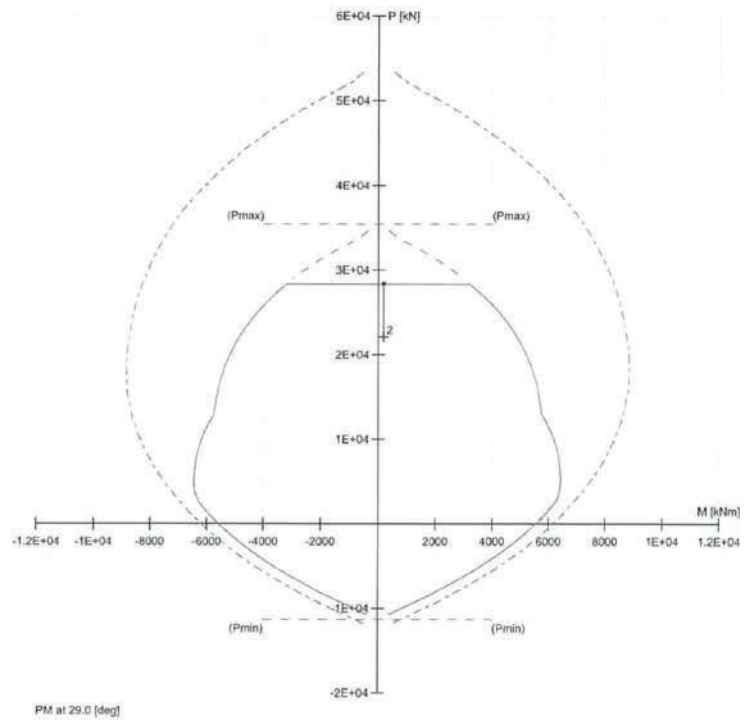
Type	Irregular
A_g	1.44e+006 mm ²
I_x	1.728e+011 mm ⁴
I_y	1.728e+011 mm ⁴

Reinforcement

Pattern	Irregular
Bar layout	---
Cover to	---
Clear cover	---
Bars	---

Confinement type Tied

Total steel area, A_s	31424 mm ²
Rho	2.18 %
Min. clear spacing	137 mm



No.	P_u kN	M_{ux} kNm	M_{uy} kNm	ϕP_u kN	ϕM_{ux} kNm	ϕM_{uy} kNm	Capacity Ratio
2	22110.0	155.0	87.5	28326.86	155.00	87.50	0.78

Max. Capacity Ratio: 0.78



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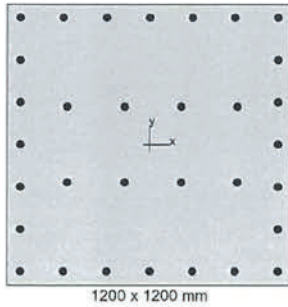
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Page | 7

9/18/2020

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6.2. MM at P=22110 [kN]



1200 x 1200 mm

General Information

Project	---
Column	---
Engineer	---
Code	ACI 318-14
Bar Set	ASTM A615
Units	Metric
Run Option	Investigation
Run Axis	Biaxial
Slenderness	Not Considered
Column Type	Structural
Capacity Method	Critical capacity

Materials

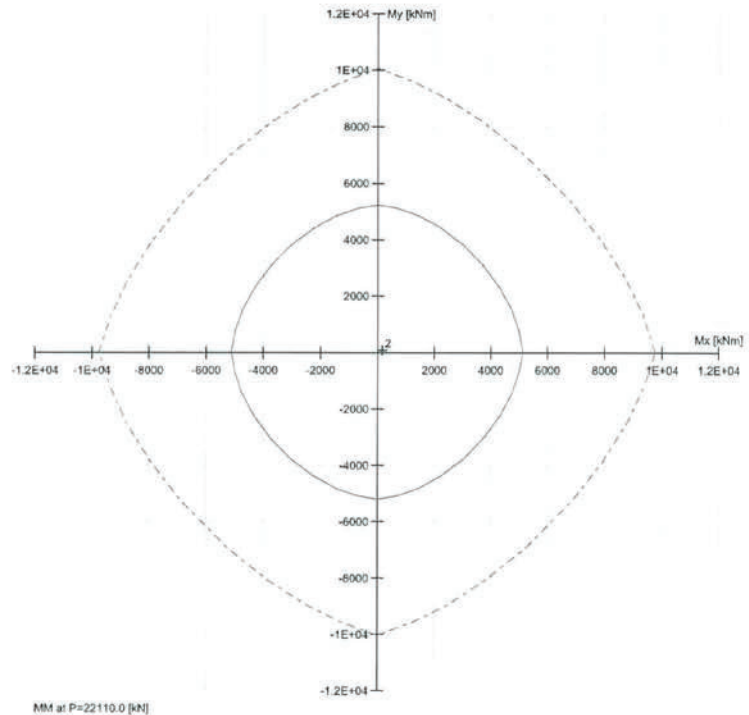
f_c	35 MPa
E_c	27805.6 MPa
f_y	400 MPa
E_s	200000 MPa

Section

Type	Irregular
A_g	1.44e+006 mm ²
I_x	1.728e+011 mm ⁴
I_y	1.728e+011 mm ⁴

Reinforcement

Pattern	Irregular
Bar layout	---
Cover to	---
Clear cover	---
Bars	---
Confinement type	Tied
Total steel area, A_s	31424 mm ²
Rho	2.18 %
Min. clear spacing	137 mm



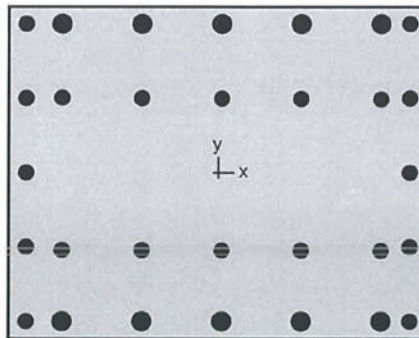
No.	P_u kN	M_{ux} kNm	M_{uy} kNm	ϕP_n kN	ϕM_{nx} kNm	ϕM_{ny} kNm	Capacity Ratio
2	22110.0	155.0	87.5	28326.86	155.00	87.50	0.78

Max. Capacity Ratio: 0.78





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Page | 2

9/18/2020

1:34 PM

Contents

1. General Information	3
2. Material Properties	3
2.1. Concrete	3
2.2. Steel	3
3. Section	3
3.1. Shape and Properties	3
3.2. Section Figure	4
3.3. Exterior Points	4
4. Reinforcement	4
4.1. Bar Set: ASTM A615	4
4.2. Confinement and Factors	4
4.3. Arrangement	4
4.4. Bars Provided	5
5. Factored Loads and Moments with Corresponding Capacity Ratios	5
6. Diagrams	6
6.1. PM at $\theta=42$ [deg]	6
6.2. MM at $P=16420$ [kN]	7

List of Figures

Figure 1: Column section	4
--------------------------------	---



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Page | 3

9/18/2020

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1. General Information

File Name	C:\193018\GCDT\SPcolumn\10-09-63(C1 ...)\C3-L2.col
Project	---
Column	---
Engineer	---
Code	ACI 318-14
Bar Set	ASTM A615
Units	Metric
Run Option	Investigation
Run Axis	Biaxial
Slenderness	Not Considered
Column Type	Structural
Capacity Method	Critical capacity

2. Material Properties

2.1. Concrete

Type	Standard
f'_c	34 MPa
E_c	27405.5 MPa
f_c	28.9 MPa
ϵ_u	0.003 mm/mm
β_1	0.803444

2.2. Steel

Type	Standard
f_y	400 MPa
E_s	200000 MPa
ϵ_{yt}	0.002 mm/mm

3. Section

3.1. Shape and Properties

Type	Irregular
A_g	800000 mm ²
I_x	4.26667e+010 mm ⁴
I_y	6.66667e+010 mm ⁴
r_x	230.94 mm
r_y	288.675 mm
X_o	0 mm
Y_o	0 mm



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Page | 4

9/18/2020

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3.2. Section Figure

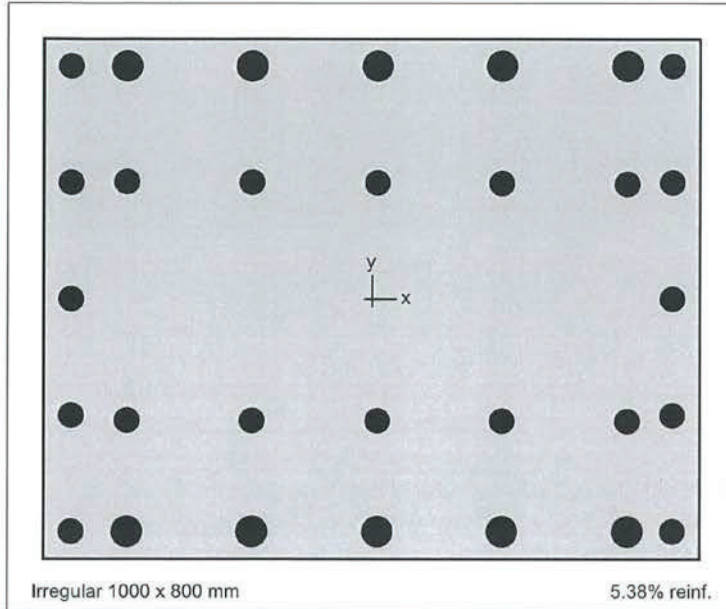


Figure 1: Column section

3.3. Exterior Points

Points	X mm	Y mm	Points	X mm	Y mm	Points	X mm	Y mm
1	-500.0	-400.0	2	500.0	-400.0	3	500.0	400.0
4	-500.0	400.0						

4. Reinforcement

4.1. Bar Set: ASTM A615

Bar	Diameter mm	Area mm ²	Bar	Diameter mm	Area mm ²	Bar	Diameter mm	Area mm ²
#3	9.53	70.97	#4	12.70	129.03	#5	15.88	200.00
#6	19.05	283.87	#7	22.23	387.10	#8	25.40	509.68
#9	28.65	645.16	#10	32.26	819.35	#11	35.81	1006.45
#14	43.00	1451.61	#18	57.33	2580.64			

4.2. Confinement and Factors

Confinement type	Tied
For #10 bars or less	#3 ties
For larger bars	#4 ties
Capacity Reduction Factors	
Axial compression, (a)	0.8
Tension controlled ϕ , (b)	0.9
Compression controlled ϕ , (c)	0.65

4.3. Arrangement

Pattern	Irregular
Bar layout	----
Cover to	----
Clear cover	----



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Page | 5

9/18/2020

1:34 PM

Bars	---
Total steel area, A_s	43050 mm ²
Rho	5.38 %
Minimum clear spacing	25 mm

4.4. Bars Provided

Area mm ²	X mm	Y mm	Area mm ²	X mm	Y mm	Area mm ²	X mm	Y mm
1230.0	-458.0	-358.0	1230.0	-458.0	-179.0	1230.0	-458.0	0.0
1230.0	-458.0	179.0	1230.0	-458.0	358.0	1230.0	458.0	-358.0
1230.0	458.0	-179.0	1230.0	458.0	0.0	1230.0	458.0	179.0
1230.0	458.0	358.0	1845.0	-373.0	358.0	1845.0	-182.5	358.0
1845.0	8.0	358.0	1845.0	198.5	358.0	1845.0	389.0	358.0
1845.0	-373.0	-358.0	1845.0	-182.5	-358.0	1845.0	8.0	-358.0
1845.0	198.5	-358.0	1845.0	389.0	-358.0	1230.0	-373.0	-186.5
1230.0	-182.5	-187.0	1230.0	8.0	-187.4	1230.0	198.5	-187.8
1230.0	389.0	-188.2	1230.0	-373.0	180.3	1230.0	-182.5	179.5
1230.0	8.0	178.6	1230.0	198.5	177.7	1230.0	389.0	176.9

5. Factored Loads and Moments with Corresponding Capacity Ratios

NOTE: Calculations are based on "Critical Capacity" Method.

No.	Demand			Capacity			Parameters at Capacity			Capacity Ratio
	P_u kN	M_{ux} kNm	M_{uy} kNm	ϕP_n kN	ϕM_{nx} kNm	ϕM_{ny} kNm	NA Depth mm	ϵ_t	ϕ	
1	1990.00	17.00	13.00	8297.90	2755.45	2107.11	692	0.00193	0.650	0.15
2	16420.00	21.00	19.00	20329.85	21.00	19.00	1163	-0.00005	0.650	0.81
3	11230.00	218.00	401.00	20329.85	218.00	401.00	1238	-0.00005	0.650	0.55
4	11370.00	339.00	50.00	20329.85	339.00	50.00	925	-0.00034	0.650	0.56
5	12470.00	385.00	341.00	20329.85	385.00	341.00	1159	-0.00005	0.650	0.61
6	12350.00	240.00	460.00	20329.85	240.00	460.00	1238	-0.00005	0.650	0.61



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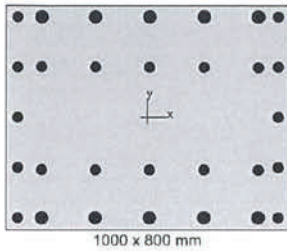
Page | 6

9/18/2020

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6. Diagrams

6.1. PM at $\theta=42$ [deg]



General Information

Project	---
Column	---
Engineer	---
Code	ACI 318-14
Bar Set	ASTM A615
Units	Metric
Run Option	Investigation
Run Axis	Biaxial
Slenderness	Not Considered
Column Type	Structural
Capacity Method	Critical capacity

Materials

f'_c	34 MPa
E_c	27405.5 MPa
f_y	400 MPa
E_s	200000 MPa

Section

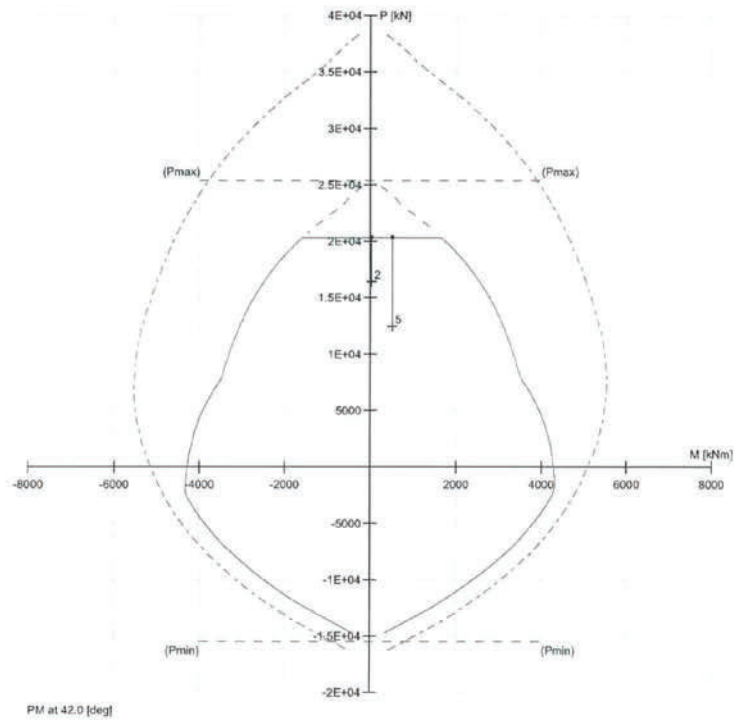
Type	Irregular
A_g	800000 mm ²
I_x	4.26667e+010 mm ⁴
I_y	6.66667e+010 mm ⁴

Reinforcement

Pattern	Irregular
Bar layout	---
Cover to	---
Clear cover	---
Bars	---

Confinement

Confinement type	Tied
Total steel area, A_s	43050 mm ²
Rho	5.38 %
Min. clear spacing	25 mm



No.	P_u kN	M_{ux} kNm	M_{uy} kNm	ϕP_n kN	ϕM_{nx} kNm	ϕM_{ny} kNm	Capacity Ratio
2	16420.0	21.0	19.0	20329.85	21.00	19.00	0.81
5	12470.0	385.0	341.0	20329.85	385.00	341.00	0.61

Max. Capacity Ratio: 0.81



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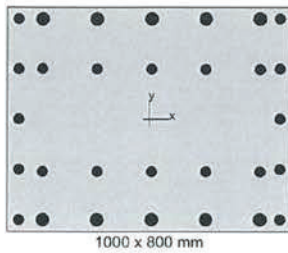
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Page | 7

9/18/2020

1:34 PM

6.2. MM at P=16420 [kN]



General Information

Project	---
Column	---
Engineer	---
Code	ACI 318-14
Bar Set	ASTM A615
Units	Metric
Run Option	Investigation
Run Axis	Biaxial
Slenderness	Not Considered
Column Type	Structural
Capacity Method	Critical capacity

Materials

f'_c	34 MPa
E_c	27405.5 MPa
f_y	400 MPa
E_s	200000 MPa

Section

Type	Irregular
A_g	800000 mm ²
I_x	4.26667e+010 mm ⁴
I_y	6.66667e+010 mm ⁴

Reinforcement

Pattern	Irregular
Bar layout	---
Cover to	---
Clear cover	---
Bars	---

Confinement type

Confinement type	Tied
------------------	------

Total steel area, A_s

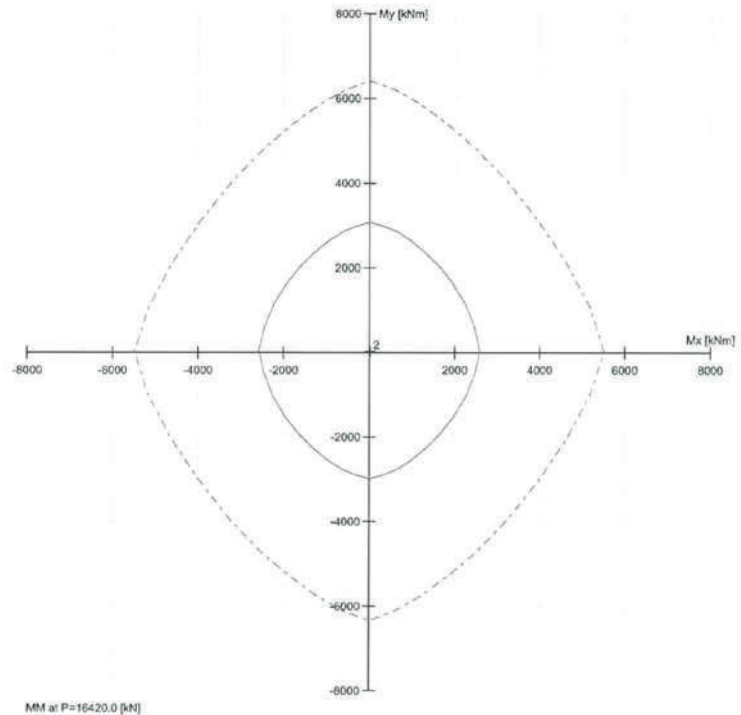
Total steel area, A_s	43050 mm ²
-------------------------	-----------------------

Rho

Rho	5.38 %
-----	--------

Min. clear spacing

Min. clear spacing	25 mm
--------------------	-------



No.	P_u kN	M_{ux} kNm	M_{uy} kNm	ϕP_n kN	ϕM_{nx} kNm	ϕM_{ny} kNm	Capacity Ratio
2	16420.0	21.0	19.0	20329.85	21.00	19.00	0.81

Max. Capacity Ratio: 0.81





รายงานการออกแบบ Design Note รายการคำนวณงานโครงสร้าง

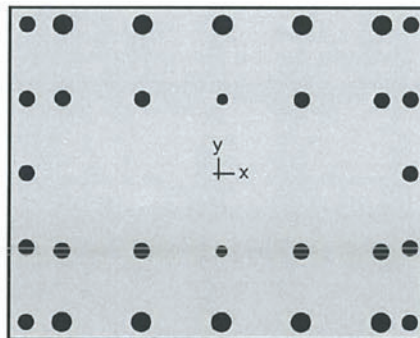
(สัญญาก่อสร้างอาคารทิศตะวันตก Final Detailed Design)

(ส่วนงานโครงสร้าง งานสถาปัตยกรรม และงานระบบหลัก)

โครงการพัฒนาพื้นที่ส่วนขยายศูนย์ราชการเฉลิมพระเกียรติ ๘๐ พรรษา ๕ ธันวาคม ๒๕๕๐ พื้นที่โซน C



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Contents

1. General Information	3
2. Material Properties	3
2.1. Concrete	3
2.2. Steel	3
3. Section	3
3.1. Shape and Properties	3
3.2. Section Figure	4
3.3. Exterior Points	4
4. Reinforcement	4
4.1. Bar Set: ASTM A615	4
4.2. Confinement and Factors	4
4.3. Arrangement	4
4.4. Bars Provided	5
5. Factored Loads and Moments with Corresponding Capacity Ratios	5
6. Diagrams	6
6.1. PM at $\theta=38$ [deg]	6
6.2. MM at $P=16460$ [kN]	7

List of Figures

Figure 1: Column section	4
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Page | 3

9/18/2020

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1. General Information

File Name	C:\193018\GCDT\SPcolumn\10-09-63(C1 ...)\C4-L2.col
Project	---
Column	---
Engineer	---
Code	ACI 318-14
Bar Set	ASTM A615
Units	Metric
Run Option	Investigation
Run Axis	Biaxial
Slenderness	Not Considered
Column Type	Structural
Capacity Method	Critical capacity

2. Material Properties

2.1. Concrete

Type	Standard
f'_c	34 MPa
E_c	27405.5 MPa
f_c	28.9 MPa
ϵ_u	0.003 mm/mm
β_1	0.803444

2.2. Steel

Type	Standard
f_y	400 MPa
E_s	200000 MPa
ϵ_{yt}	0.002 mm/mm

3. Section

3.1. Shape and Properties

Type	Irregular
A_g	800000 mm ²
I_x	4.26667e+010 mm ⁴
I_y	6.66667e+010 mm ⁴
r_x	230.94 mm
r_y	288.675 mm
X_o	0 mm
Y_o	0 mm



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Page | 4

9/18/2020

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3.2. Section Figure

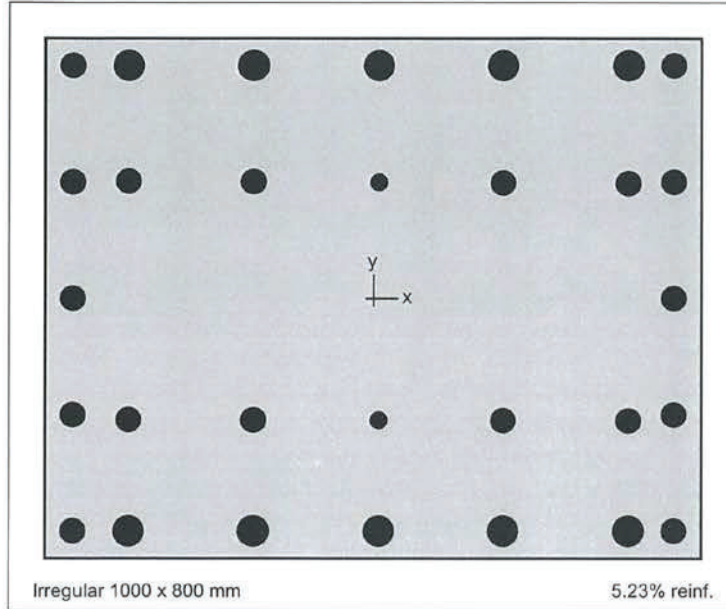


Figure 1: Column section

3.3. Exterior Points

Points	X mm	Y mm	Points	X mm	Y mm	Points	X mm	Y mm
1	-500.0	-400.0	2	500.0	-400.0	3	500.0	400.0
4	-500.0	400.0						

4. Reinforcement

4.1. Bar Set: ASTM A615

Bar	Diameter mm	Area mm ²	Bar	Diameter mm	Area mm ²	Bar	Diameter mm	Area mm ²
#3	9.53	70.97	#4	12.70	129.03	#5	15.88	200.00
#6	19.05	283.87	#7	22.23	387.10	#8	25.40	509.68
#9	28.65	645.16	#10	32.26	819.35	#11	35.81	1006.45
#14	43.00	1451.61	#18	57.33	2580.64			

4.2. Confinement and Factors

Confinement type	Tied
For #10 bars or less	#3 ties
For larger bars	#4 ties
Capacity Reduction Factors	
Axial compression, (a)	0.8
Tension controlled ϕ , (b)	0.9
Compression controlled ϕ , (c)	0.65

4.3. Arrangement

Pattern	Irregular
Bar layout	----
Cover to	----
Clear cover	----



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Page | 5

9/18/2020

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Bars	---
Total steel area, A_s	41820 mm ²
Rho	5.23 %
Minimum clear spacing	25 mm

4.4. Bars Provided

Area mm ²	X mm	Y mm	Area mm ²	X mm	Y mm	Area mm ²	X mm	Y mm
1230.0	-458.0	-358.0	1230.0	-458.0	-179.0	1230.0	-458.0	0.0
1230.0	-458.0	179.0	1230.0	-458.0	358.0	1230.0	458.0	-358.0
1230.0	458.0	-179.0	1230.0	458.0	0.0	1230.0	458.0	179.0
1230.0	458.0	358.0	1845.0	-373.0	358.0	1845.0	-182.5	358.0
1845.0	8.0	358.0	1845.0	198.5	358.0	1845.0	389.0	358.0
1845.0	-373.0	-358.0	1845.0	-182.5	-358.0	1845.0	8.0	-358.0
1845.0	198.5	-358.0	1845.0	389.0	-358.0	1230.0	-373.0	-186.5
1230.0	-182.5	-187.0	615.0	8.0	-187.4	1230.0	198.5	-187.8
1230.0	389.0	-188.2	1230.0	-373.0	180.3	1230.0	-182.5	179.5
615.0	8.0	178.6	1230.0	198.5	177.7	1230.0	389.0	176.9

5. Factored Loads and Moments with Corresponding Capacity Ratios

NOTE: Calculations are based on "Critical Capacity" Method.

No.	Demand			Capacity			Parameters at Capacity			Capacity Ratio
	P_u kN	M_{ux} kNm	M_{uy} kNm	ϕP_n kN	ϕM_{nx} kNm	ϕM_{ny} kNm	NA Depth mm	ϵ_t	ϕ	
1	2160.00	2.00	14.00	8886.83	591.95	4143.68	691	0.00184	0.650	0.19
2	16460.00	41.00	32.00	20092.49	41.00	32.00	1130	-0.00006	0.650	0.82
3	8060.00	12.00	599.00	14224.73	69.99	3493.55	811	0.00063	0.650	0.43
4	11170.00	624.00	78.00	20092.49	624.00	78.00	917	-0.00035	0.650	0.56
5	11690.00	27.00	632.00	20092.49	27.00	632.00	1116	-0.00033	0.650	0.58



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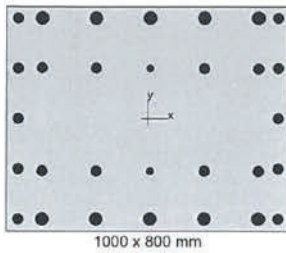
Page | 6

9/18/2020

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6. Diagrams

6.1. PM at $\theta=38$ [deg]



General Information

Project	---
Column	---
Engineer	---
Code	ACI 318-14
Bar Set	ASTM A615
Units	Metric
Run Option	Investigation
Run Axis	Biaxial
Slenderness	Not Considered
Column Type	Structural
Capacity Method	Critical capacity

Materials

f_c	34 MPa
E_c	27405.5 MPa
f_y	400 MPa
E_s	200000 MPa

Section

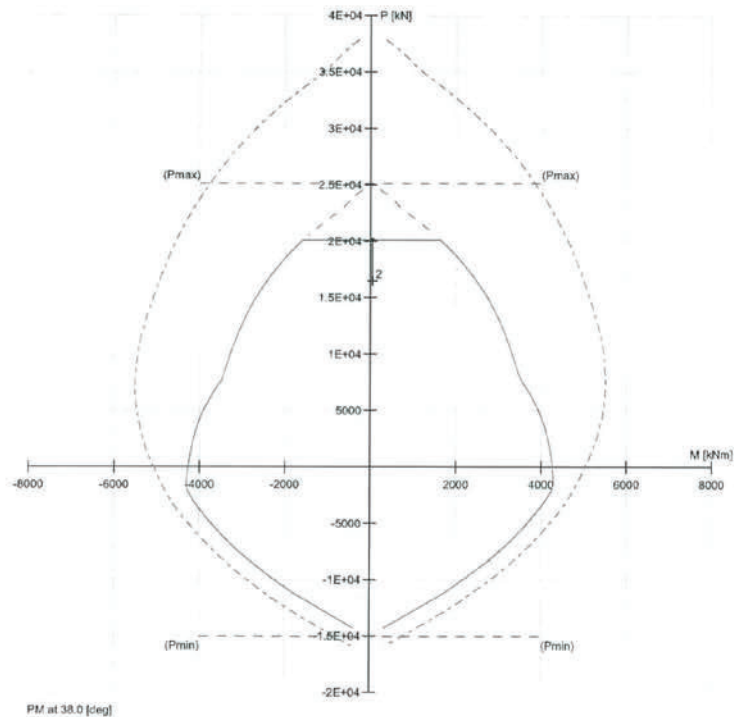
Type	Irregular
A_g	800000 mm ²
I_x	4.26667e+010 mm ⁴
I_y	6.66667e+010 mm ⁴

Reinforcement

Pattern	Irregular
Bar layout	---
Cover to	---
Clear cover	---
Bars	---

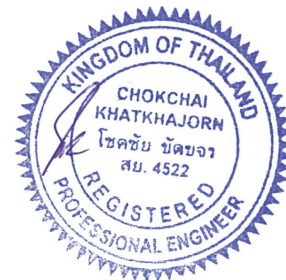
Confinement type

Confinement type	Tied
Total steel area, A_s	41820 mm ²
Rho	5.23 %
Min. clear spacing	25 mm



No.	P_u kN	M_{ux} kNm	M_{uy} kNm	ϕP_u kN	ϕM_{ux} kNm	ϕM_{uy} kNm	Capacity Ratio
2	16460.0	41.0	32.0	20092.49	41.00	32.00	0.82

Max. Capacity Ratio: 0.82



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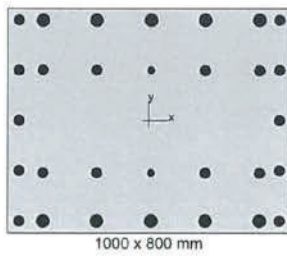
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Page | 7

9/18/2020

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6.2. MM at P=16460 [kN]



General Information

Project	---
Column	---
Engineer	---
Code	ACI 318-14
Bar Set	ASTM A615
Units	Metric
Run Option	Investigation
Run Axis	Biaxial
Slenderness	Not Considered
Column Type	Structural
Capacity Method	Critical capacity

Materials

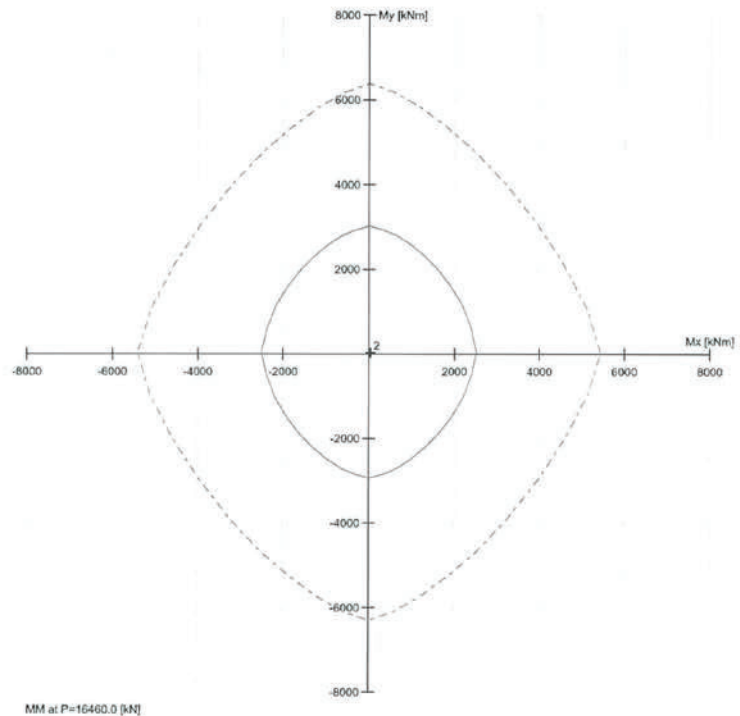
f'_c	34 MPa
E_c	27405.5 MPa
f_y	400 MPa
E_s	200000 MPa

Section

Type	Irregular
A_g	800000 mm ²
I_x	4.26667e+010 mm ⁴
I_y	6.66667e+010 mm ⁴

Reinforcement

Pattern	Irregular
Bar layout	---
Cover to	---
Clear cover	---
Bars	---
Confinement type	Tied
Total steel area, A_s	41820 mm ²
Rho	5.23 %
Min. clear spacing	25 mm



No.	P_u kN	M_{ux} kNm	M_{uy} kNm	ϕP_n kN	ϕM_{nx} kNm	ϕM_{ny} kNm	Capacity Ratio
2	16460.0	41.0	32.0	20092.49	41.00	32.00	0.82

Max. Capacity Ratio: 0.82





รายงานการออกแบบ Design Note รายการคำนวณงานโครงสร้าง

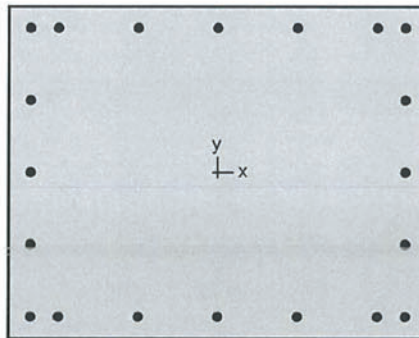
(สัญญาก่อสร้างอาคารทิศตะวันตก Final Detailed Design)

(ส่วนงานโครงสร้าง งานสถาปัตยกรรม และงานระบบหลัก)

โครงการพัฒนาพื้นที่ส่วนขยายศูนย์ราชการเฉลิมพระเกียรติ ๘๐ พรรษา ๕ ธันวาคม ๒๕๕๐ พื้นที่โซน C



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Contents

1. General Information	3
2. Material Properties	3
2.1. Concrete	3
2.2. Steel	3
3. Section	3
3.1. Shape and Properties	3
3.2. Section Figure	4
3.3. Exterior Points	4
4. Reinforcement	4
4.1. Bar Set: ASTM A615	4
4.2. Confinement and Factors	4
4.3. Arrangement	4
4.4. Bars Provided	5
5. Factored Loads and Moments with Corresponding Capacity Ratios	5
6. Diagrams	6
6.1. PM at $\theta=11$ [deg]	6
6.2. MM at P=1030 [kN]	7

List of Figures

Figure 1: Column section	4
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1. General Information

File Name	C:\193018\GCDT\SPcolumn\10-09-63(C1 ...)\C5-L2.col
Project	---
Column	---
Engineer	---
Code	ACI 318-14
Bar Set	ASTM A615
Units	Metric
Run Option	Investigation
Run Axis	Biaxial
Slenderness	Not Considered
Column Type	Structural
Capacity Method	Critical capacity

2. Material Properties

2.1. Concrete

Type	Standard
f'_c	34 MPa
E_c	27405.5 MPa
f_c	28.9 MPa
ϵ_u	0.003 mm/mm
β_1	0.803444

2.2. Steel

Type	Standard
f_y	400 MPa
E_s	200000 MPa
ϵ_{yt}	0.002 mm/mm

3. Section

3.1. Shape and Properties

Type	Irregular
A_g	800000 mm ²
I_x	4.26667e+010 mm ⁴
I_y	6.66667e+010 mm ⁴
r_x	230.94 mm
r_y	288.675 mm
X_o	0 mm
Y_o	0 mm



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Page | 4

9/18/2020

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3.2. Section Figure

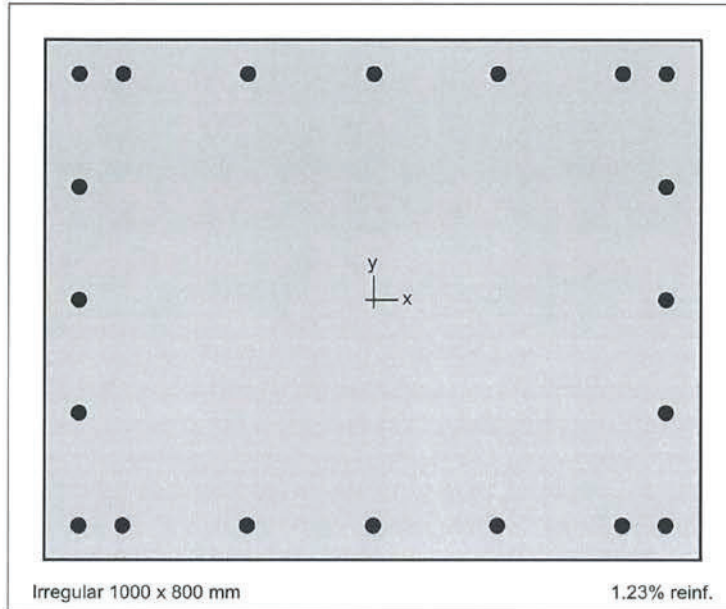


Figure 1: Column section

3.3. Exterior Points

Points	X mm	Y mm	Points	X mm	Y mm	Points	X mm	Y mm
1	-500.0	-400.0	2	500.0	-400.0	3	500.0	400.0
4	-500.0	400.0						

4. Reinforcement

4.1. Bar Set: ASTM A615

Bar	Diameter mm	Area mm ²	Bar	Diameter mm	Area mm ²	Bar	Diameter mm	Area mm ²
#3	9.53	70.97	#4	12.70	129.03	#5	15.88	200.00
#6	19.05	283.87	#7	22.23	387.10	#8	25.40	509.68
#9	28.65	645.16	#10	32.26	819.35	#11	35.81	1006.45
#14	43.00	1451.61	#18	57.33	2580.64			

4.2. Confinement and Factors

Confinement type	Tied
For #10 bars or less	#3 ties
For larger bars	#4 ties
Capacity Reduction Factors	
Axial compression, (a)	0.8
Tension controlled ϕ , (b)	0.9
Compression controlled ϕ , (c)	0.65

4.3. Arrangement

Pattern	Irregular
Bar layout	---
Cover to	---
Clear cover	---



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Page | 5

9/18/2020

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Bars	---
Total steel area, A_s	9820 mm ²
Rho	1.23 %
Minimum clear spacing	41 mm

4.4. Bars Provided

Area mm ²	X mm	Y mm	Area mm ²	X mm	Y mm	Area mm ²	X mm	Y mm
491.0	-447.5	-347.5	491.0	-447.5	-173.7	491.0	-447.5	0.0
491.0	-447.5	173.7	491.0	-447.5	347.5	491.0	447.5	-347.5
491.0	447.5	-173.7	491.0	447.5	0.0	491.0	447.5	173.7
491.0	447.5	347.5	491.0	-381.0	347.5	491.0	-190.5	347.5
491.0	0.0	347.5	491.0	190.5	347.5	491.0	381.0	347.5
491.0	-381.0	-347.5	491.0	-190.5	-347.5	491.0	0.0	-347.5
491.0	190.5	-347.5	491.0	381.0	-347.5			

5. Factored Loads and Moments with Corresponding Capacity Ratios

NOTE: Calculations are based on "Critical Capacity" Method.

No.	Demand			Capacity			Parameters at Capacity			Capacity Ratio
	P_u kN	M_{ux} kNm	M_{uy} kNm	ϕP_n kN	ϕM_{nx} kNm	ϕM_{ny} kNm	NA Depth mm	ϵ_t	ϕ	
1	334.00	0.00	0.00	355.04	1381.42	0.00	93	0.02119	0.900	0.46
2	2630.00	38.00	21.00	0.00	1192.95	659.26	206	0.01072	0.900	0.36
3	1030.00	39.00	110.00	0.00	529.23	1492.70	254	0.01053	0.900	0.41
4	1030.00	124.00	23.00	0.00	1241.84	230.34	124	0.01922	0.900	0.51
5	2070.00	30.00	129.00	0.00	358.43	1541.26	206	0.01286	0.900	0.45



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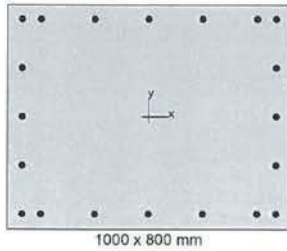
Page | 6

9/18/2020

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6. Diagrams

6.1. PM at $\theta=11$ [deg]



General Information

Project	---
Column	---
Engineer	---
Code	ACI 318-14
Bar Set	ASTM A615
Units	Metric
Run Option	Investigation
Run Axis	Biaxial
Slenderness	Not Considered
Column Type	Structural
Capacity Method	Critical capacity

Materials

f_c	34 MPa
E_s	27405.5 MPa
f_y	400 MPa
E_s	200000 MPa

Section

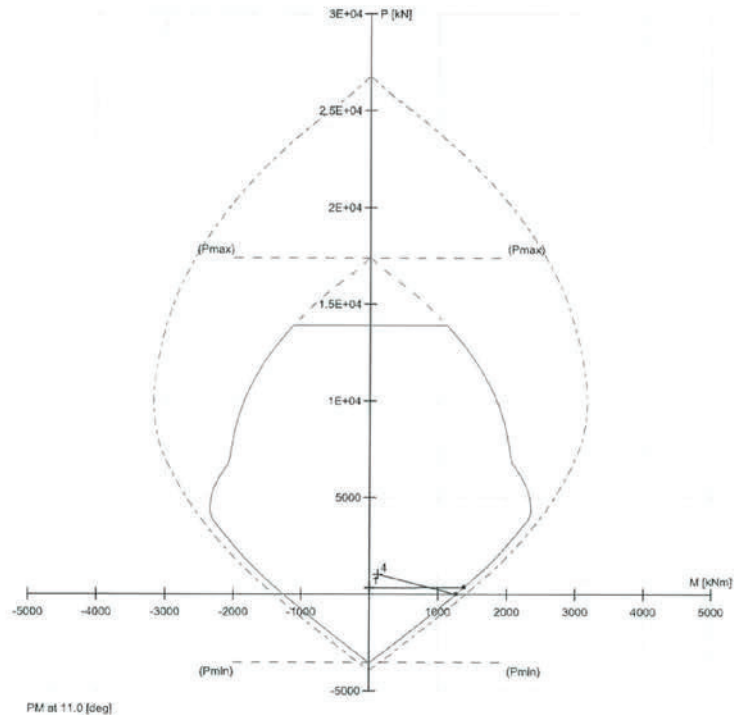
Type	Irregular
A_g	800000 mm ²
I_x	4.26667e+010 mm ⁴
I_y	6.66667e+010 mm ⁴

Reinforcement

Pattern	Irregular
Bar layout	---
Cover to	---
Clear cover	---
Bars	---

Confinement type

Confinement type	Tied
Total steel area, A_s	9820 mm ²
Rho	1.23 %
Min. clear spacing	41 mm



PM at 11.0 [deg]

No.	P_o kN	M_{ux} kNm	M_{uy} kNm	ϕP_n kN	ϕM_{nx} kNm	ϕM_{ny} kNm	Capacity Ratio
4	1030.0	124.0	23.0	0.00	1241.84	230.34	0.51
1	334.0	0.0	0.0	355.04	1381.42	0.00	0.46

Max. Capacity Ratio: 0.51



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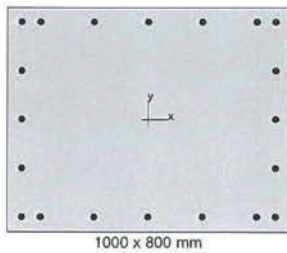
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Page | 7

9/18/2020

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6.2. MM at P=1030 [kN]



General Information

Project	---
Column	---
Engineer	---
Code	ACI 318-14
Bar Set	ASTM A615
Units	Metric
Run Option	Investigation
Run Axis	Biaxial
Slenderness	Not Considered
Column Type	Structural
Capacity Method	Critical capacity

Materials

f'_c	34 MPa
E_c	27405.5 MPa
f_y	400 MPa
E_s	200000 MPa

Section

Type	Irregular
A_g	800000 mm ²
I_x	4.26667e+010 mm ⁴
I_y	6.66667e+010 mm ⁴

Reinforcement

Pattern	Irregular
Bar layout	---
Cover to	---
Clear cover	---
Bars	---

Confinement type

Confinement type	Tied
------------------	------

Total steel area, A_s

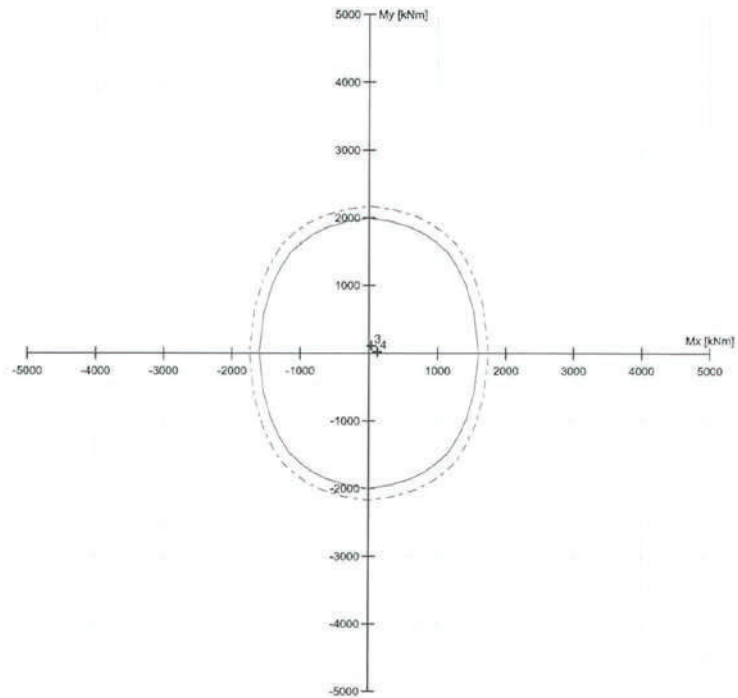
Total steel area, A_s	9820 mm ²
-------------------------	----------------------

Rho

Rho	1.23 %
-----	--------

Min. clear spacing

Min. clear spacing	41 mm
--------------------	-------



No.	P _u kN	M _{ux} kNm	M _{uy} kNm	ϕP_n kN	ϕM_{nx} kNm	ϕM_{ny} kNm	Capacity Ratio
4	1030.0	124.0	23.0	0.00	1241.84	230.34	0.51
3	1030.0	39.0	110.0	0.00	529.23	1492.70	0.41

Max. Capacity Ratio: 0.51





รายงานการออกแบบ Design Note รายการคำนวณงานโครงสร้าง

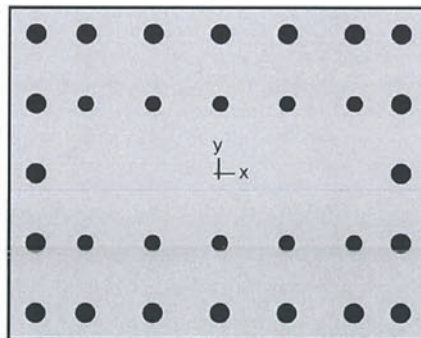
(สัญญาก่อสร้างอาคารทิศตะวันตก Final Detailed Design)

(ส่วนงานโครงสร้าง งานสถาปัตยกรรม และงานระบบหลัก)

โครงการพัฒนาพื้นที่ส่วนขยายศูนย์ราชการเฉลิมพระเกียรติ ๘๐ พรรษา ๕ ธันวาคม ๒๕๕๐ พื้นที่โซน C



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Contents

1. General Information	3
2. Material Properties	3
2.1. Concrete	3
2.2. Steel	3
3. Section	3
3.1. Shape and Properties	3
3.2. Section Figure	4
3.3. Exterior Points	4
4. Reinforcement	4
4.1. Bar Set: ASTM A615	4
4.2. Confinement and Factors	4
4.3. Arrangement	4
4.4. Bars Provided	5
5. Factored Loads and Moments with Corresponding Capacity Ratios	5
6. Diagrams	6
6.1. PM at $\theta=22$ [deg]	6
6.2. MM at $P=21970$ [kN]	7

List of Figures

Figure 1: Column section	4
--------------------------------	---



1. General Information

File Name	C:\193018\GCDT\SPcolumn\10-09-63(C1 ...)\C6-L2.col
Project	---
Column	---
Engineer	---
Code	ACI 318-14
Bar Set	ASTM A615
Units	Metric
Run Option	Investigation
Run Axis	Biaxial
Slenderness	Not Considered
Column Type	Structural
Capacity Method	Critical capacity

2. Material Properties

2.1. Concrete

Type	Standard
f_c	34 MPa
E_c	27405.5 MPa
f'_c	28.9 MPa
ϵ_u	0.003 mm/mm
β_1	0.803444

2.2. Steel

Type	Standard
f_y	400 MPa
E_s	200000 MPa
ϵ_{yt}	0.002 mm/mm

3. Section

3.1. Shape and Properties

Type	Irregular
A_g	800000 mm ²
I_x	4.26667e+010 mm ⁴
I_y	6.66667e+010 mm ⁴
r_x	230.94 mm
r_y	288.675 mm
X_o	0 mm
Y_o	0 mm



3.2. Section Figure

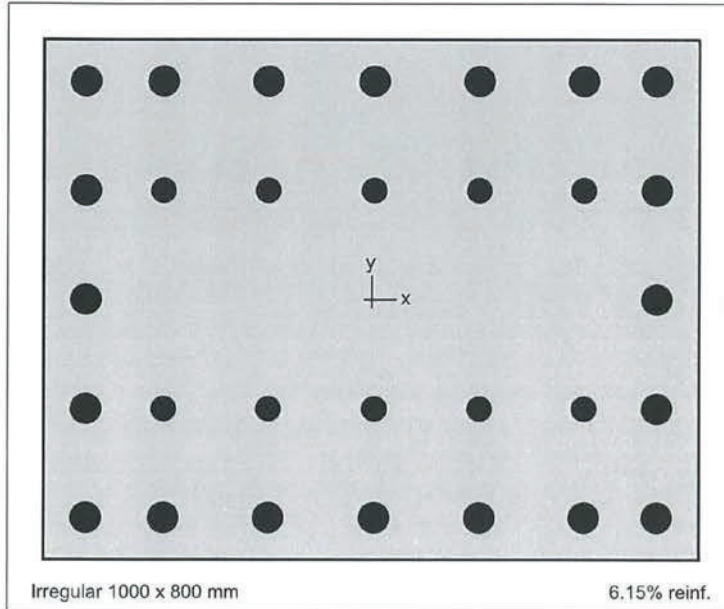


Figure 1: Column section

3.3. Exterior Points

Points	X mm	Y mm	Points	X mm	Y mm	Points	X mm	Y mm
1	-500.0	-400.0	2	500.0	-400.0	3	500.0	400.0
4	-500.0	400.0						

4. Reinforcement

4.1. Bar Set: ASTM A615

Bar	Diameter mm	Area mm ²	Bar	Diameter mm	Area mm ²	Bar	Diameter mm	Area mm ²
#3	9.53	70.97	#4	12.70	129.03	#5	15.88	200.00
#6	19.05	283.87	#7	22.23	387.10	#8	25.40	509.68
#9	28.65	645.16	#10	32.26	819.35	#11	35.81	1006.45
#14	43.00	1451.61	#18	57.33	2580.64			

4.2. Confinement and Factors

Confinement type	Tied
For #10 bars or less	#3 ties
For larger bars	#4 ties
Capacity Reduction Factors	
Axial compression, (a)	0.8
Tension controlled ϕ , (b)	0.9
Compression controlled ϕ , (c)	0.65

4.3. Arrangement

Pattern	Irregular
Bar layout	---
Cover to	---
Clear cover	---



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Page | 5

9/18/2020

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Bars	---
Total steel area, A_s	49200 mm ²
Rho	6.15 %
Minimum clear spacing	63 mm

4.4. Bars Provided

Area mm ²	X mm	Y mm	Area mm ²	X mm	Y mm	Area mm ²	X mm	Y mm
1845.0	-435.8	-335.8	1845.0	-435.8	-167.9	1845.0	-435.8	0.0
1845.0	-435.8	167.9	1845.0	-435.8	335.8	1845.0	435.8	-335.8
1845.0	435.8	-167.9	1845.0	435.8	0.0	1845.0	435.8	167.9
1845.0	435.8	335.8	1845.0	-317.2	335.8	1845.0	-156.8	335.8
1845.0	3.5	335.8	1845.0	163.9	335.8	1845.0	324.3	335.8
1845.0	-317.2	-335.8	1845.0	-156.8	-335.8	1845.0	3.5	-335.8
1845.0	163.9	-335.8	1845.0	324.3	-335.8	1230.0	-317.2	-167.9
1230.0	-156.8	-167.9	1230.0	3.5	-167.9	1230.0	163.9	-167.9
1230.0	324.3	-167.9	1230.0	-317.2	167.9	1230.0	-156.8	167.9
1230.0	3.5	167.9	1230.0	163.9	167.9	1230.0	324.3	167.9

5. Factored Loads and Moments with Corresponding Capacity Ratios

NOTE: Calculations are based on "Critical Capacity" Method.

No.	Demand			Capacity			Parameters at Capacity			Capacity Ratio
	P_u	M_{ux}	M_{uy}	ϕP_n	ϕM_{nx}	ϕM_{ny}	NA Depth	ϵ_t	ϕ	
	kN	kNm	kNm	kN	kNm	kNm	mm			
1	2830.00	277.00	10.00	10087.49	3673.35	132.61	520	0.00139	0.650	0.27
2	21970.00	48.00	19.00	21516.62	48.00	19.00	1014	-0.00028	0.650	1.02 #
3	8884.00	696.00	114.00	15532.95	2813.17	460.78	726	0.00050	0.650	0.46
4	19339.00	412.00	22.00	21516.62	412.00	22.00	896	-0.00047	0.650	0.90
5	19240.00	400.00	398.00	21516.62	400.00	398.00	1180	-0.00015	0.650	0.89
6	8060.00	244.00	224.00	21516.62	244.00	224.00	1166	-0.00015	0.650	0.37

Section capacity exceeded. Revise design!



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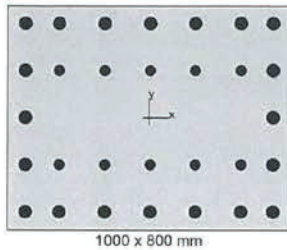
Page | 6

9/18/2020

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6. Diagrams

6.1. PM at $\theta=22$ [deg]



General Information

Project	---
Column	---
Engineer	---
Code	ACI 318-14
Bar Set	ASTM A615
Units	Metric
Run Option	Investigation
Run Axis	Biaxial
Slenderness	Not Considered
Column Type	Structural
Capacity Method	Critical capacity

Materials

f'_c	34 MPa
E_c	27405.5 MPa
f_y	400 MPa
E_s	200000 MPa

Section

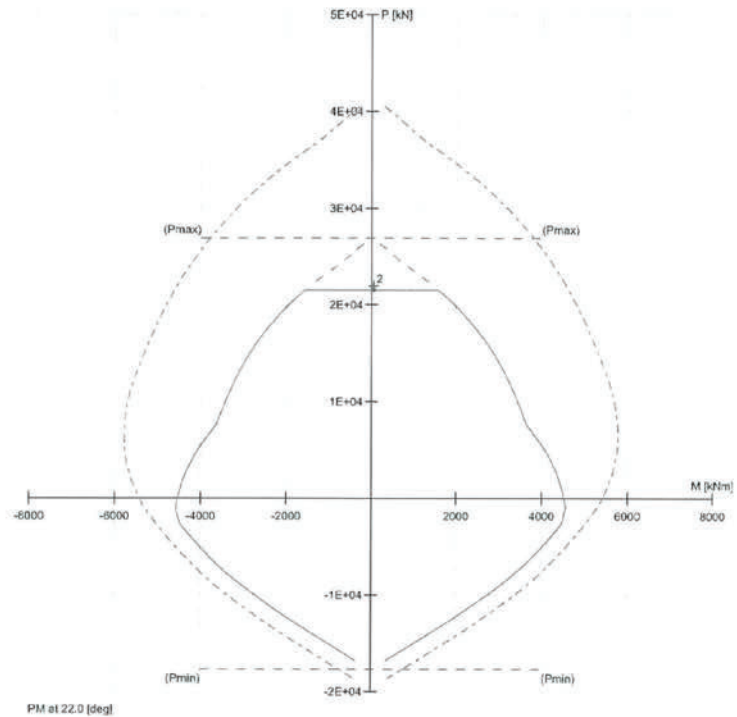
Type	Irregular
A_g	800000 mm ²
I_x	4.26667e+010 mm ⁴
I_y	6.66667e+010 mm ⁴

Reinforcement

Pattern	Irregular
Bar layout	---
Cover to	---
Clear cover	---
Bars	---

Confinement type

Confinement type	Tied
Total steel area, A_s	49200 mm ²
Rho	6.15 %
Min. clear spacing	63 mm



No.	P_u kN	M_{ux} kNm	M_{uy} kNm	ϕP_n kN	ϕM_{nx} kNm	ϕM_{ny} kNm	Capacity Ratio
2	21970.0	48.0	19.0	21516.62	48.00	19.00	1.02

Max. Capacity Ratio: 1.02

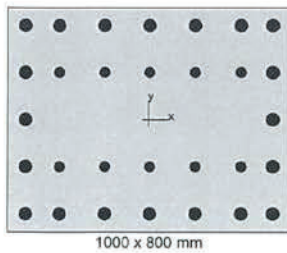


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Page | 7
9/18/2020
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6.2. MM at P=21970 [kN]



General Information

Project	---
Column	---
Engineer	---
Code	ACI 318-14
Bar Set	ASTM A615
Units	Metric
Run Option	Investigation
Run Axis	Biaxial
Slenderness	Not Considered
Column Type	Structural
Capacity Method	Critical capacity

Materials

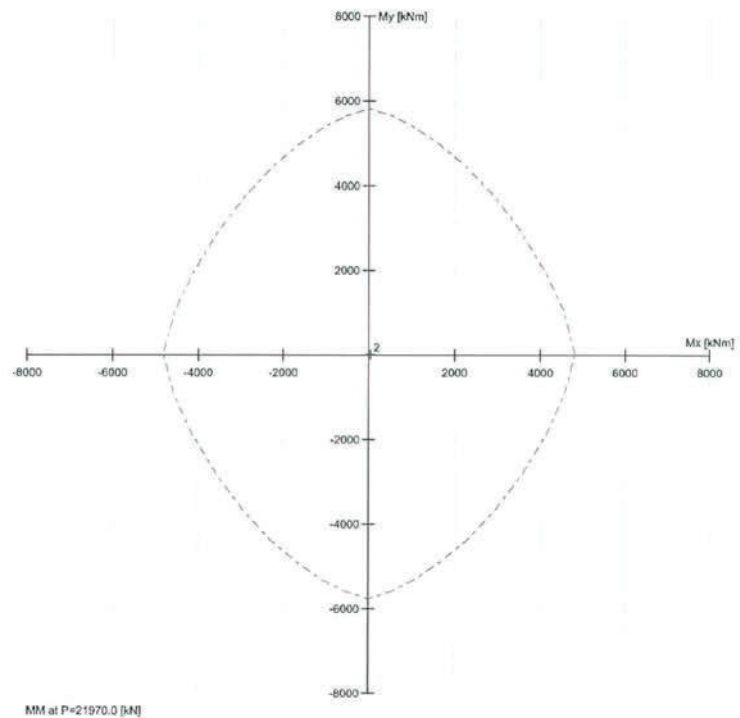
f'_c	34 MPa
E_c	27405.5 MPa
f_y	400 MPa
E_s	200000 MPa

Section

Type	Irregular
A_g	800000 mm ²
I_x	4.26667e+010 mm ⁴
I_y	6.66667e+010 mm ⁴

Reinforcement

Pattern	Irregular
Bar layout	---
Cover to	---
Clear cover	---
Bars	---
Confinement type	Tied
Total steel area, A_s	49200 mm ²
Rho	6.15 %
Min. clear spacing	63 mm



No.	P_u kN	M_{ux} kNm	M_{uy} kNm	ϕP_u kN	ϕM_{ux} kNm	ϕM_{uy} kNm	Capacity Ratio
2	21970.0	48.0	19.0	21516.62	48.00	19.00	1.02

Max. Capacity Ratio: 1.02





รายงานการออกแบบ Design Note รายการคำนวณงานโครงสร้าง

(สัญญาก่อสร้างอาคารทิศตะวันตก Final Detailed Design)

(ส่วนงานโครงสร้าง งานสถาปัตยกรรม และงานระบบหลัก)

โครงการพัฒนาพื้นที่ส่วนขยายศูนย์ราชการเฉลิมพระเกียรติ ๘๐ พรรษา ๕ ธันวาคม ๒๕๕๐ พื้นที่โซน C

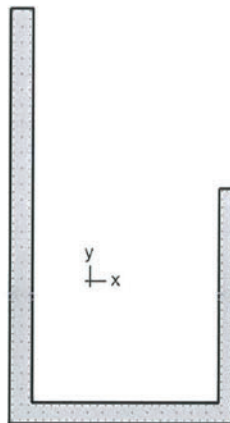


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Contents

1. General Information	3
2. Material Properties	3
2.1. Concrete	3
2.2. Steel	3
3. Section	3
3.1. Shape and Properties	3
3.2. Section Figure	4
3.3. Exterior Points	4
4. Reinforcement	4
4.1. Bar Set: ASTM A615	4
4.2. Confinement and Factors	4
4.3. Arrangement	4
4.4. Bars Provided	5
5. Factored Loads and Moments with Corresponding Capacity Ratios	6
6. Diagrams	7
6.1. PM at $\theta=2$ [deg]	7
6.2. MM at $P=30500$ [kN]	8

List of Figures

Figure 1: Column section	4
--------------------------------	---



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Page | 3
9/18/2020
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1. General Information

File Name	C:\193018\GCDT\SPcolumn\10-09-63(C1 ...)\P1-L2.col
Project	---
Column	---
Engineer	---
Code	ACI 318-14
Bar Set	ASTM A615
Units	Metric
Run Option	Investigation
Run Axis	Biaxial
Slenderness	Not Considered
Column Type	Structural
Capacity Method	Critical capacity

2. Material Properties

2.1. Concrete

Type	Standard
f_c	35 MPa
E_c	27805.6 MPa
f_{cs}	29.75 MPa
ϵ_u	0.003 mm/mm
β_1	0.796192

2.2. Steel

Type	Standard
f_y	400 MPa
E_s	200000 MPa
ϵ_{yt}	0.002 mm/mm

3. Section

3.1. Shape and Properties

Type	Irregular
A_g	6.07125e+006 mm ²
I_x	3.34113e+013 mm ⁴
I_y	1.65083e+013 mm ⁴
r_x	2345.89 mm
r_y	1648.97 mm
X_o	0 mm
Y_o	-0.000168664 mm



3.2. Section Figure

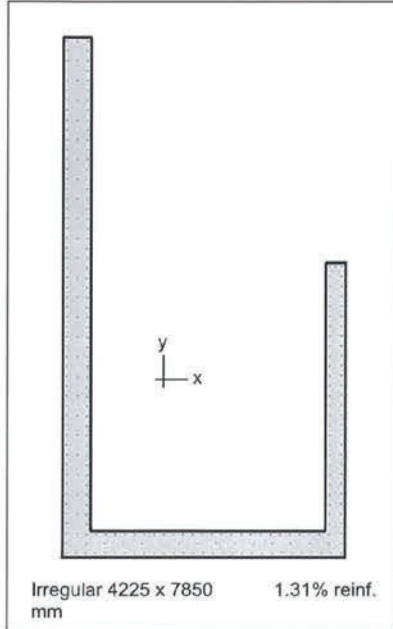


Figure 1: Column section

3.3. Exterior Points

Points	X mm	Y mm	Points	X mm	Y mm	Points	X mm	Y mm
1	2710.6	1757.8	2	2410.6	1757.8	3	2410.6	-2292.2
4	-1089.4	-2292.2	5	-1089.4	5157.8	6	-1514.4	5157.8
7	-1514.4	-2692.2	8	2710.6	-2692.2			

4. Reinforcement

4.1. Bar Set: ASTM A615

Bar	Diameter mm	Area mm ²	Bar	Diameter mm	Area mm ²	Bar	Diameter mm	Area mm ²
#3	9.53	70.97	#4	12.70	129.03	#5	15.88	200.00
#6	19.05	283.87	#7	22.23	387.10	#8	25.40	509.68
#9	28.65	645.16	#10	32.26	819.35	#11	35.81	1006.45
#14	43.00	1451.61	#18	57.33	2580.64			

4.2. Confinement and Factors

Confinement type	Tied
For #10 bars or less	#3 ties
For larger bars	#4 ties
Capacity Reduction Factors	
Axial compression, (a)	0.8
Tension controlled ϕ , (b)	0.9
Compression controlled ϕ , (c)	0.65

4.3. Arrangement

Pattern	Irregular
Bar layout	---



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Page | 5

9/18/2020

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Cover to	---
Clear cover	---
Bars	---
Total steel area, A_s	79756 mm ²
Rho	1.31 %
Minimum clear spacing	70 mm



4.4. Bars Provided

Area mm ²	X mm	Y mm	Area mm ²	X mm	Y mm	Area mm ²	X mm	Y mm
314.0	-1454.4	-2632.2	314.0	-1454.4	-2483.6	314.0	-1454.4	-2334.9
314.0	-1454.4	-2186.3	314.0	-1454.4	-2037.6	314.0	-1454.4	-1889.0
314.0	-1454.4	-1740.3	314.0	-1454.4	-1591.6	314.0	-1454.4	-1443.0
314.0	-1454.4	-1294.3	314.0	-1454.4	-1145.7	314.0	-1454.4	-997.0
314.0	-1454.4	-848.4	314.0	-1454.4	-699.7	314.0	-1454.4	-551.1
314.0	-1454.4	-402.4	314.0	-1454.4	-253.8	314.0	-1454.4	-105.1
314.0	-1454.4	43.5	314.0	-1454.4	192.2	314.0	-1454.4	340.9
314.0	-1454.4	489.5	314.0	-1454.4	638.2	314.0	-1454.4	786.8
314.0	-1454.4	935.5	314.0	-1454.4	1084.1	314.0	-1454.4	1232.8
314.0	-1454.4	1381.4	314.0	-1454.4	1530.1	314.0	-1454.4	1678.7
314.0	-1454.4	1827.4	314.0	-1454.4	1976.0	314.0	-1454.4	2124.7
314.0	-1454.4	2273.4	314.0	-1454.4	2422.0	314.0	-1454.4	2570.7
314.0	-1454.4	2719.3	314.0	-1454.4	2868.0	314.0	-1454.4	3016.6
314.0	-1454.4	3165.3	314.0	-1454.4	3313.9	314.0	-1454.4	3462.6
314.0	-1454.4	3611.2	314.0	-1454.4	3759.9	314.0	-1454.4	3908.5
314.0	-1454.4	4057.2	314.0	-1454.4	4205.9	314.0	-1454.4	4354.5
314.0	-1454.4	4503.2	314.0	-1454.4	4651.8	314.0	-1454.4	4800.5
314.0	-1454.4	4949.1	314.0	-1454.4	5097.8	314.0	-1307.8	-2632.2
314.0	-1161.2	-2632.2	314.0	-1149.4	-2352.2	314.0	-1149.4	-2203.2
314.0	-1149.4	-2054.2	314.0	-1149.4	-1905.2	314.0	-1149.4	-1756.2
314.0	-1149.4	-1607.2	314.0	-1149.4	-1458.2	314.0	-1149.4	-1309.2
314.0	-1149.4	-1160.2	314.0	-1149.4	-1011.2	314.0	-1149.4	-862.2
314.0	-1149.4	-713.2	314.0	-1149.4	-564.2	314.0	-1149.4	-415.2
314.0	-1149.4	-266.2	314.0	-1149.4	-117.2	314.0	-1149.4	31.8
314.0	-1149.4	180.8	314.0	-1149.4	329.8	314.0	-1149.4	478.8
314.0	-1149.4	627.8	314.0	-1149.4	776.8	314.0	-1149.4	925.8
314.0	-1149.4	1074.8	314.0	-1149.4	1223.8	314.0	-1149.4	1372.8
314.0	-1149.4	1521.8	314.0	-1149.4	1670.8	314.0	-1149.4	1819.8
314.0	-1149.4	1968.8	314.0	-1149.4	2117.8	314.0	-1149.4	2266.8
314.0	-1149.4	2415.8	314.0	-1149.4	2564.8	314.0	-1149.4	2713.8
314.0	-1149.4	2862.8	314.0	-1149.4	3011.8	314.0	-1149.4	3160.8
314.0	-1149.4	3309.8	314.0	-1149.4	3458.8	314.0	-1149.4	3607.8
314.0	-1149.4	3756.8	314.0	-1149.4	3905.8	314.0	-1149.4	4054.8
314.0	-1149.4	4203.8	314.0	-1149.4	4352.8	314.0	-1149.4	4501.8
314.0	-1149.4	4650.8	314.0	-1149.4	4799.8	314.0	-1149.4	4948.8
314.0	-1149.4	5097.8	314.0	-1014.5	-2632.2	314.0	-1004.6	-2352.2
314.0	-867.9	-2632.2	314.0	-859.8	-2352.2	314.0	-721.3	-2632.2
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314.0	-428.1	-2632.2	314.0	-425.4	-2352.2	314.0	-281.5	-2632.2
314.0	-280.6	-2352.2	314.0	-135.8	-2352.2	314.0	-134.9	-2632.2
314.0	9.0	-2352.2	314.0	11.7	-2632.2	314.0	153.8	-2352.2
314.0	158.3	-2632.2	314.0	298.6	-2352.2	314.0	304.9	-2632.2
314.0	443.4	-2352.2	314.0	451.5	-2632.2	314.0	588.2	-2352.2
314.0	598.1	-2632.2	314.0	733.0	-2352.2	314.0	744.7	-2632.2
314.0	877.8	-2352.2	314.0	891.4	-2632.2	314.0	1022.6	-2352.2
314.0	1038.0	-2632.2	314.0	1167.4	-2352.2	314.0	1184.6	-2632.2
314.0	1312.2	-2352.2	314.0	1331.2	-2632.2	314.0	1457.0	-2352.2
314.0	1477.8	-2632.2	314.0	1601.8	-2352.2	314.0	1624.4	-2632.2
314.0	1746.6	-2352.2	314.0	1771.0	-2632.2	314.0	1891.4	-2352.2



รายงานการออกแบบ Design Note รายการคำนวณงานโครงสร้าง

(สัญญาก่อสร้างอาคารทิศตะวันตก Final Detailed Design)

(ส่วนงานโครงสร้าง งานสถาปัตยกรรม และงานระบบหลัก)

โครงการพัฒนาพื้นที่ส่วนขยายศูนย์ราชการเฉลิมพระเกียรติ ๘๐ พรรษา ๕ ธันวาคม ๒๕๕๐ พื้นที่โซน C

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Page | 6

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Area mm ²	X mm	Y mm	Area mm ²	X mm	Y mm	Area mm ²	X mm	Y mm
314.0	1917.6	-2632.2	314.0	2036.2	-2352.2	314.0	2064.2	-2632.2
314.0	2181.0	-2352.2	314.0	2210.8	-2632.2	314.0	2325.8	-2352.2
314.0	2357.4	-2632.2	314.0	2470.6	-2352.2	314.0	2470.6	-2202.2
314.0	2470.6	-2052.2	314.0	2470.6	-1902.2	314.0	2470.6	-1752.2
314.0	2470.6	-1602.2	314.0	2470.6	-1452.2	314.0	2470.6	-1302.2
314.0	2470.6	-1152.2	314.0	2470.6	-1002.2	314.0	2470.6	-852.2
314.0	2470.6	-702.2	314.0	2470.6	-552.2	314.0	2470.6	-402.2
314.0	2470.6	-252.2	314.0	2470.6	-102.2	314.0	2470.6	47.8
314.0	2470.6	197.8	314.0	2470.6	347.8	314.0	2470.6	497.8
314.0	2470.6	647.8	314.0	2470.6	797.8	314.0	2470.6	947.8
314.0	2470.6	1097.8	314.0	2470.6	1247.8	314.0	2470.6	1397.8
314.0	2470.6	1547.8	314.0	2470.6	1697.8	314.0	2504.0	-2632.2
314.0	2560.6	1697.8	314.0	2650.6	-2632.2	314.0	2650.6	-2482.9
314.0	2650.6	-2333.6	314.0	2650.6	-2184.3	314.0	2650.6	-2035.0
314.0	2650.6	-1885.7	314.0	2650.6	-1736.4	314.0	2650.6	-1587.1
314.0	2650.6	-1437.7	314.0	2650.6	-1288.4	314.0	2650.6	-1139.1
314.0	2650.6	-989.8	314.0	2650.6	-840.5	314.0	2650.6	-691.2
314.0	2650.6	-541.9	314.0	2650.6	-392.6	314.0	2650.6	-243.3
314.0	2650.6	-93.9	314.0	2650.6	55.4	314.0	2650.6	204.7
314.0	2650.6	354.0	314.0	2650.6	503.3	314.0	2650.6	652.6
314.0	2650.6	801.9	314.0	2650.6	951.2	314.0	2650.6	1100.5
314.0	2650.6	1249.8	314.0	2650.6	1399.2	314.0	2650.6	1548.5
314.0	2650.6	1697.8	314.0	-1301.9	5097.8	314.0	-1301.1	4800.5
314.0	-1300.3	4503.1	314.0	-1299.6	4205.8	314.0	-1298.8	3908.5
314.0	-1298.0	3611.2	314.0	-1297.3	3313.9	314.0	-1296.5	3016.5
314.0	-1295.7	2719.2	314.0	-1295.0	2421.9	314.0	-1294.2	2124.6
314.0	-1293.5	1827.3	314.0	-1292.7	1529.9	314.0	-1291.9	1232.6
314.0	-1291.2	935.3	314.0	-1290.4	638.0	314.0	-1289.6	340.7
314.0	-1288.9	43.3	314.0	-1288.1	-254.0	314.0	-1287.3	-551.3
314.0	-1286.6	-848.6	314.0	-1285.8	-1145.9	314.0	-1285.0	-1443.3
314.0	-1284.3	-1740.6	314.0	-1283.5	-2037.9	314.0	-1282.7	-2335.2
314.0	-1152.3	-2485.8	314.0	-873.9	-2485.6	314.0	-595.5	-2485.5
314.0	-317.1	-2485.3	314.0	-38.8	-2485.1	314.0	239.6	-2485.0
314.0	518.0	-2484.8	314.0	796.4	-2484.7	314.0	1074.7	-2484.5
314.0	1353.1	-2484.4	314.0	1631.5	-2484.2	314.0	1909.9	-2484.1
314.0	2188.3	-2483.9	314.0	2466.6	-2483.8			

5. Factored Loads and Moments with Corresponding Capacity Ratios

NOTE: Calculations are based on "Critical Capacity" Method.

No.	Demand			Capacity			Parameters at Capacity			Capacity Ratio
	P _u kN	M _{ux} kNm	M _{uy} kNm	φP _n kN	φM _{nx} kNm	φM _{ny} kNm	NA Depth mm	ε _t	φ	
1	9030.00	30340.00	1740.00	0.00	72252.30	4143.67	368	0.07756	0.900	0.77
2	42480.00	8270.00	10500.00	0.00	52827.01	67071.79	1017	0.01734	0.900	0.45
3	29800.00	73740.00	440.00	10337.97	96705.86	577.03	599	0.04367	0.900	0.78
4	26440.00	8240.00	20520.00	0.00	28637.41	71315.48	458	0.03759	0.900	0.58
5	35250.00	32520.00	38980.00	1106.91	57002.45	68325.82	1129	0.01637	0.900	0.63
6	30500.00	95750.00	3430.00	17109.35	112881.09	4043.68	694	0.03609	0.900	0.85



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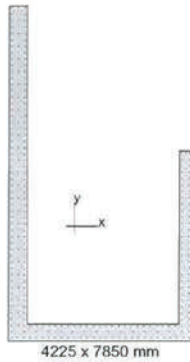
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Page | 7

9/18/2020
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6. Diagrams

6.1. PM at $\theta=2$ [deg]



General Information

Project	---
Column	---
Engineer	---
Code	ACI 318-14
Bar Set	ASTM A615
Units	Metric
Run Option	Investigation
Run Axis	Biaxial
Slenderness	Not Considered
Column Type	Structural
Capacity Method	Critical capacity

Materials

f'_c	35 MPa
E_c	27805.6 MPa
f_y	400 MPa
E_s	200000 MPa

Section

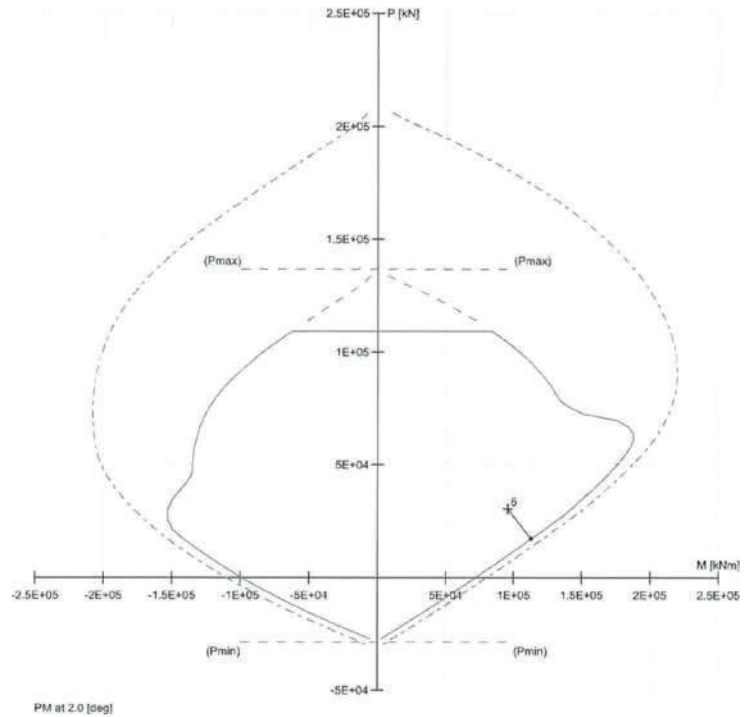
Type	Irregular
A_g	6.07125e+006 mm ²
I_x	3.34113e+013 mm ⁴
I_y	1.65083e+013 mm ⁴

Reinforcement

Pattern	Irregular
Bar layout	---
Cover to	---
Clear cover	---
Bars	---

Confinement type

Confinement type	Tied
Total steel area, A_s	79756 mm ²
Rho	1.31 %
Min. clear spacing	70 mm



PM at 2.0 [deg]

No.	P_u kN	M_{ux} kNm	M_{uy} kNm	ϕP_n kN	ϕM_{nx} kNm	ϕM_{ny} kNm	Capacity Ratio
6	30500.0	95750.0	3430.0	17109.35	112881.09	4043.68	0.85

Max. Capacity Ratio: 0.85



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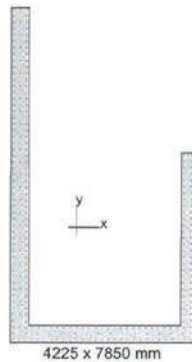
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Page | 8

9/18/2020

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6.2. MM at P=30500 [kN]



General Information

Project	---
Column	---
Engineer	---
Code	ACI 318-14
Bar Set	ASTM A615
Units	Metric
Run Option	Investigation
Run Axis	Biaxial
Slenderness	Not Considered
Column Type	Structural
Capacity Method	Critical capacity

Materials

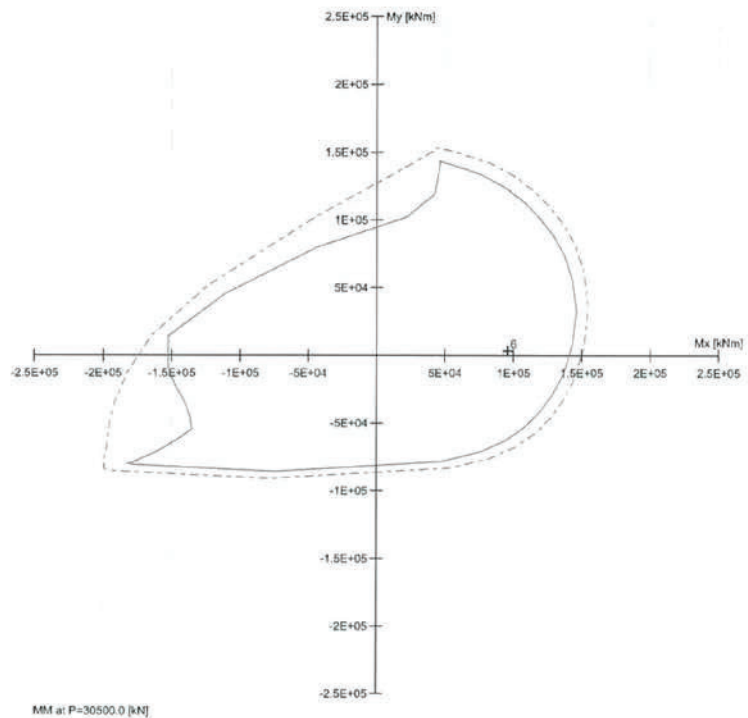
f'_c	35 MPa
E_c	27805.6 MPa
f_y	400 MPa
E_s	200000 MPa

Section

Type	Irregular
A_g	6.07125e+006 mm ²
I_x	3.34113e+013 mm ⁴
I_y	1.65083e+013 mm ⁴

Reinforcement

Pattern	Irregular
Bar layout	---
Cover to	---
Clear cover	---
Bars	---
Confinement type	Tied
Total steel area, A_s	79756 mm ²
Rho	1.31 %
Min. clear spacing	70 mm



No.	P_u kN	M_{ux} kNm	M_{uy} kNm	ϕP_n kN	ϕM_{nx} kNm	ϕM_{ny} kNm	Capacity Ratio
6	30500.0	95750.0	3430.0	17109.35	112881.09	4043.68	0.85

Max. Capacity Ratio: 0.85





รายงานการออกแบบ Design Note รายการคำนวณงานโครงสร้าง

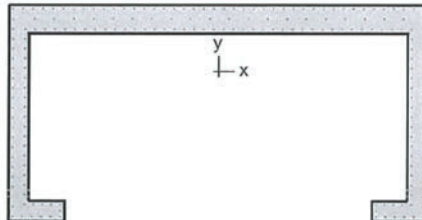
(สัญญาก่อสร้างอาคารทิศตะวันตก Final Detailed Design)

(ส่วนงานโครงสร้าง งานสถาปัตยกรรม และงานระบบหลัก)

โครงการพัฒนาพื้นที่ส่วนขยายศูนย์ราชการเฉลิมพระเกียรติ ๘๐ พรรษา ๕ ธันวาคม ๒๕๕๐ พื้นที่โซน C



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Contents

1. General Information	3
2. Material Properties	3
2.1. Concrete	3
2.2. Steel	3
3. Section	3
3.1. Shape and Properties	3
3.2. Section Figure	4
3.3. Exterior Points	4
4. Reinforcement	4
4.1. Bar Set: ASTM A615	4
4.2. Confinement and Factors	4
4.3. Arrangement	4
4.4. Bars Provided	5
5. Factored Loads and Moments with Corresponding Capacity Ratios	6
6. Diagrams	7
6.1. PM at $\theta=86$ [deg]	7
6.2. MM at $P=22930$ [kN]	8

List of Figures

Figure 1: Column section	4
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1. General Information

File Name	C:\193018\GCDT\SPcolumn\10-09-63(C1 ...)\P2-L2.col
Project	---
Column	---
Engineer	---
Code	ACI 318-14
Bar Set	ASTM A615
Units	Metric
Run Option	Investigation
Run Axis	Biaxial
Slenderness	Not Considered
Column Type	Structural
Capacity Method	Critical capacity

2. Material Properties

2.1. Concrete

Type	Standard
f'_c	35 MPa
E_c	27805.6 MPa
f_c	29.75 MPa
ϵ_u	0.003 mm/mm
β_1	0.796192

2.2. Steel

Type	Standard
f_y	400 MPa
E_s	200000 MPa
ϵ_{yt}	0.002 mm/mm

3. Section

3.1. Shape and Properties

Type	Irregular
A_g	4.63e+006 mm ²
I_x	5.27319e+012 mm ⁴
I_y	2.51091e+013 mm ⁴
r_x	1067.2 mm
r_y	2328.76 mm
X_o	0 mm
Y_o	0 mm



3.2. Section Figure

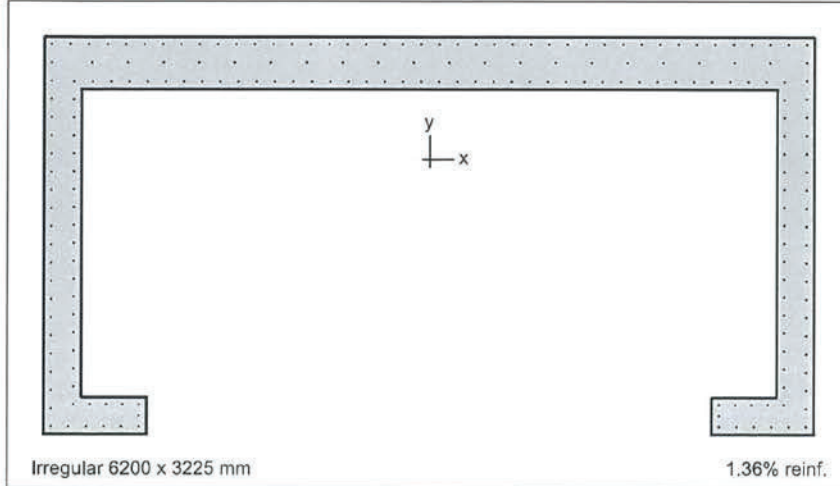


Figure 1: Column section

3.3. Exterior Points

Points	X mm	Y mm	Points	X mm	Y mm	Points	X mm	Y mm
1	-2275.0	-1932.7	2	-2800.0	-1932.7	3	-2800.0	567.3
4	2800.0	567.3	5	2800.0	-1932.7	6	2275.0	-1932.7
7	2275.0	-2232.7	8	3100.0	-2232.7	9	3100.0	992.3
10	-3100.0	992.3	11	-3100.0	-2232.7	12	-2275.0	-2232.7

4. Reinforcement

4.1. Bar Set: ASTM A615

Bar	Diameter mm	Area mm ²	Bar	Diameter mm	Area mm ²	Bar	Diameter mm	Area mm ²
#3	9.53	70.97	#4	12.70	129.03	#5	15.88	200.00
#6	19.05	283.87	#7	22.23	387.10	#8	25.40	509.68
#9	28.65	645.16	#10	32.26	819.35	#11	35.81	1006.45
#14	43.00	1451.61	#18	57.33	2580.64			

4.2. Confinement and Factors

Confinement type	Tied
For #10 bars or less	#3 ties
For larger bars	#4 ties
Capacity Reduction Factors	
Axial compression, (a)	0.8
Tension controlled ϕ , (b)	0.9
Compression controlled ϕ , (c)	0.65

4.3. Arrangement

Pattern	Irregular
Bar layout	---
Cover to	---
Clear cover	---
Bars	---





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Page | 5

9/18/2020

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Total steel area, A_s	62800 mm ²
Rho	1.36 %
Minimum clear spacing	70 mm



4.4. Bars Provided

Area mm ²	X mm	Y mm	Area mm ²	X mm	Y mm	Area mm ²	X mm	Y mm
314.0	-3040.0	932.3	314.0	-2899.6	-2172.7	314.0	-2891.7	932.3
314.0	-2860.0	-1992.7	314.0	-2860.0	-1847.1	314.0	-2860.0	-1701.5
314.0	-2860.0	-1556.0	314.0	-2860.0	-1410.4	314.0	-2860.0	-1264.9
314.0	-2860.0	-1119.3	314.0	-2860.0	-973.8	314.0	-2860.0	-828.2
314.0	-2860.0	-682.7	314.0	-2860.0	-537.1	314.0	-2860.0	-391.5
314.0	-2860.0	-246.0	314.0	-2860.0	-100.4	314.0	-2860.0	45.1
314.0	-2860.0	190.7	314.0	-2860.0	336.2	314.0	-2860.0	481.8
314.0	-2860.0	627.3	314.0	-2759.2	-2172.7	314.0	-2743.4	932.3
314.0	-2729.5	-1992.7	314.0	-2713.3	627.3	314.0	-2618.8	-2172.7
314.0	-2599.0	-1992.7	314.0	-2595.1	932.3	314.0	-2566.7	627.3
314.0	-2478.4	-2172.7	314.0	-2468.5	-1992.7	314.0	-2446.8	932.3
314.0	-2420.0	627.3	314.0	-2338.0	-2172.7	314.0	-2338.0	-2082.7
314.0	-2338.0	-1992.7	314.0	-2298.5	932.3	314.0	-2273.3	627.3
314.0	-2150.2	932.3	314.0	-2126.7	627.3	314.0	-2002.0	932.3
314.0	-1980.0	627.3	314.0	-1853.7	932.3	314.0	-1833.3	627.3
314.0	-1705.4	932.3	314.0	-1686.7	627.3	314.0	-1557.1	932.3
314.0	-1540.0	627.3	314.0	-1408.8	932.3	314.0	-1393.3	627.3
314.0	-1260.5	932.3	314.0	-1246.7	627.3	314.0	-1112.2	932.3
314.0	-1100.0	627.3	314.0	-963.9	932.3	314.0	-953.3	627.3
314.0	-815.6	932.3	314.0	-806.7	627.3	314.0	-667.3	932.3
314.0	-660.0	627.3	314.0	-519.0	932.3	314.0	-513.3	627.3
314.0	-370.7	932.3	314.0	-366.7	627.3	314.0	-222.4	932.3
314.0	-220.0	627.3	314.0	-74.1	932.3	314.0	-73.3	627.3
314.0	73.3	627.3	314.0	74.1	932.3	314.0	220.0	627.3
314.0	222.4	932.3	314.0	366.7	627.3	314.0	370.7	932.3
314.0	513.3	627.3	314.0	519.0	932.3	314.0	660.0	627.3
314.0	667.3	932.3	314.0	806.7	627.3	314.0	815.6	932.3
314.0	953.3	627.3	314.0	963.9	932.3	314.0	1100.0	627.3
314.0	1112.2	932.3	314.0	1246.7	627.3	314.0	1260.5	932.3
314.0	1393.3	627.3	314.0	1408.8	932.3	314.0	1540.0	627.3
314.0	1557.1	932.3	314.0	1686.7	627.3	314.0	1705.4	932.3
314.0	1833.3	627.3	314.0	1853.7	932.3	314.0	1980.0	627.3
314.0	2002.0	932.3	314.0	2126.7	627.3	314.0	2150.2	932.3
314.0	2273.3	627.3	314.0	2298.5	932.3	314.0	2335.0	-2172.7
314.0	2335.0	-2082.7	314.0	2335.0	-1992.7	314.0	2420.0	627.3
314.0	2446.8	932.3	314.0	2466.2	-1992.7	314.0	2476.0	-2172.7
314.0	2566.7	627.3	314.0	2595.1	932.3	314.0	2597.5	-1992.7
314.0	2617.0	-2172.7	314.0	2713.3	627.3	314.0	2728.7	-1992.7
314.0	2743.4	932.3	314.0	2758.0	-2172.7	314.0	2860.0	-1992.7
314.0	2860.0	-1847.1	314.0	2860.0	-1701.5	314.0	2860.0	-1556.0
314.0	2860.0	-1410.4	314.0	2860.0	-1264.9	314.0	2860.0	-1119.3
314.0	2860.0	-973.8	314.0	2860.0	-828.2	314.0	2860.0	-682.7
314.0	2860.0	-537.1	314.0	2860.0	-391.5	314.0	2860.0	-246.0
314.0	2860.0	-100.4	314.0	2860.0	45.1	314.0	2860.0	190.7
314.0	2860.0	336.2	314.0	2860.0	481.8	314.0	2860.0	627.3
314.0	2891.7	932.3	314.0	2899.0	-2172.7	314.0	3040.0	-2172.7
314.0	3040.0	-2024.8	314.0	3040.0	-1876.9	314.0	3040.0	-1729.1
314.0	3040.0	-1581.2	314.0	3040.0	-1433.4	314.0	3040.0	-1285.5
314.0	3040.0	-1137.7	314.0	3040.0	-989.8	314.0	3040.0	-841.9
314.0	3040.0	-694.1	314.0	3040.0	-546.2	314.0	3040.0	-398.4
314.0	3040.0	-250.5	314.0	3040.0	-102.7	314.0	3040.0	45.2
314.0	3040.0	193.1	314.0	3040.0	340.9	314.0	3040.0	488.8
314.0	3040.0	636.6	314.0	3040.0	784.5	314.0	3040.0	932.3



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Page | 6

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Area mm ²	X mm	Y mm	Area mm ²	X mm	Y mm	Area mm ²	X mm	Y mm
314.0	-3040.0	-548.7	314.0	-3040.0	-401.1	314.0	-3040.0	-253.5
314.0	-3040.0	-105.9	314.0	-3040.0	41.8	314.0	-3040.0	189.4
314.0	-3040.0	337.0	314.0	-3040.0	484.7	314.0	-3040.0	632.3
314.0	-3040.0	779.9	314.0	-3040.0	-2172.7	314.0	-3040.0	-2025.0
314.0	-3040.0	-1877.4	314.0	-3040.0	-1729.8	314.0	-3040.0	-1582.1
314.0	-3040.0	-1434.5	314.0	-3040.0	-1286.9	314.0	-3040.0	-1139.3
314.0	-3040.0	-991.6	314.0	-3040.0	-844.0	314.0	-3040.0	-696.4
314.0	-2719.0	784.3	314.0	-2431.6	784.2	314.0	-2144.2	784.1
314.0	-1856.7	784.0	314.0	-1569.3	783.9	314.0	-1281.9	783.9
314.0	-994.5	783.8	314.0	-707.1	783.7	314.0	-419.6	783.6
314.0	-132.2	783.5	314.0	155.2	783.4	314.0	442.6	783.3
314.0	730.1	783.2	314.0	1017.5	783.1	314.0	1304.9	783.0
314.0	1592.3	782.9	314.0	1879.7	782.8	314.0	2167.2	782.7
314.0	2454.6	782.6	314.0	2742.0	782.5			

5. Factored Loads and Moments with Corresponding Capacity Ratios

NOTE: Calculations are based on "Critical Capacity" Method.

No.	Demand			Capacity			Parameters at Capacity			Capacity Ratio
	P_u	M_{ux}	M_{uy}	ϕP_n	ϕM_{nx}	ϕM_{ny}	NA Depth	ϵ_t	ϕ	
	kN	kNm	kNm	kN	kNm	kNm	mm			
1	5670.00	5780.00	9050.00	0.00	36078.04	56488.96	1575	0.00640	0.900	0.42
2	28110.00	2530.00	29960.00	352.32	5762.16	68234.85	385	0.05637	0.900	0.60
3	21820.00	3090.00	32270.00	0.00	6444.59	67303.22	359	0.06016	0.900	0.66
4	19740.00	13680.00	27170.00	21356.38	32473.49	64495.96	3216	0.00205	0.655	0.61
5	20290.00	18650.00	25180.00	22610.27	38524.69	52013.50	3114	0.00193	0.650	0.64
6	22930.00	7660.00	97520.00	15392.19	8593.18	109400.34	892	0.01953	0.900	0.88



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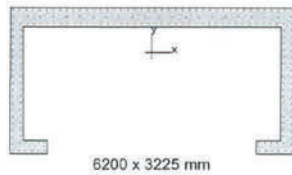
Page | 7

9/18/2020

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6. Diagrams

6.1. PM at $\theta=86$ [deg]



General Information

Project	---
Column	---
Engineer	---
Code	ACI 318-14
Bar Set	ASTM A615
Units	Metric
Run Option	Investigation
Run Axis	Biaxial
Slenderness	Not Considered
Column Type	Structural
Capacity Method	Critical capacity

Materials

f'_c	35 MPa
E_c	27805.6 MPa
f_y	400 MPa
E_s	200000 MPa

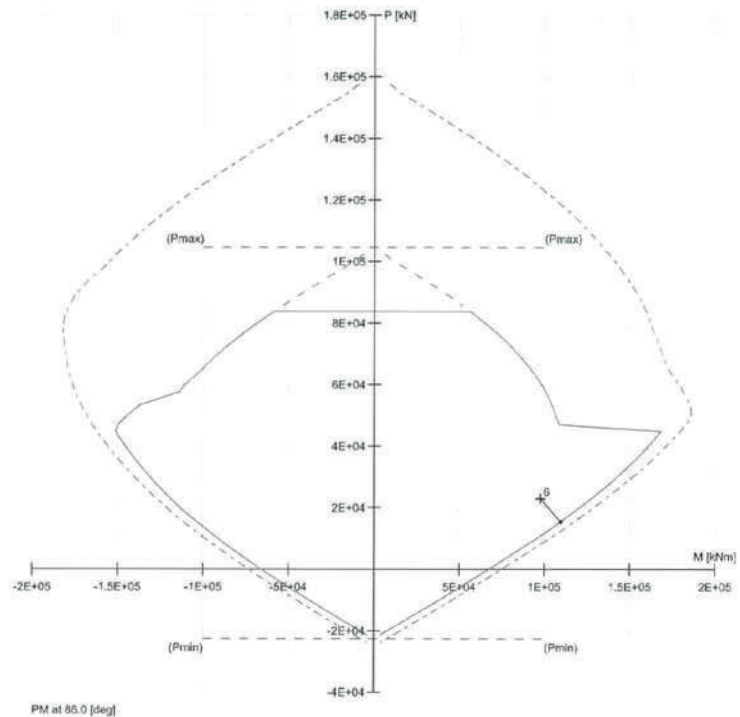
Section

Type	Irregular
A_g	4.63e+006 mm ²
I_x	5.27319e+012 mm ⁴
I_y	2.51091e+013 mm ⁴

Reinforcement

Pattern	Irregular
Bar layout	---
Cover to	---
Clear cover	---
Bars	---
Confinement type	Tied

Total steel area, A_s	62800 mm ²
Rho	1.36 %
Min. clear spacing	70 mm



No.	P_u kN	M_{ux} kNm	M_{uy} kNm	ϕP_u kN	ϕM_{ux} kNm	ϕM_{uy} kNm	Capacity Ratio
6	22930.0	7660.0	97520.0	15392.19	8593.18	109400.34	0.88

Max. Capacity Ratio: 0.88



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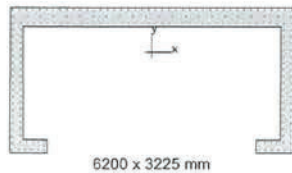
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Page | 8

9/18/2020

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6.2. MM at P=22930 [kN]



General Information

Project	---
Column	---
Engineer	---
Code	ACI 318-14
Bar Set	ASTM A615
Units	Metric
Run Option	Investigation
Run Axis	Biaxial
Slenderness	Not Considered
Column Type	Structural
Capacity Method	Critical capacity

Materials

f'_c	35 MPa
E_c	27805.6 MPa
f_y	400 MPa
E_s	200000 MPa

Section

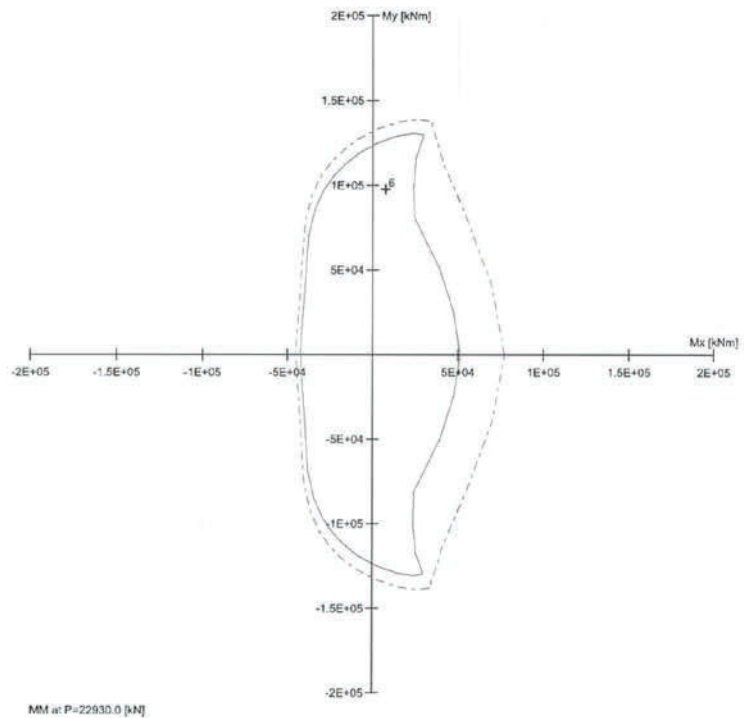
Type	Irregular
A_g	4.63e+006 mm ²
I_x	5.27319e+012 mm ⁴
I_y	2.51091e+013 mm ⁴

Reinforcement

Pattern	Irregular
Bar layout	---
Cover to	---
Clear cover	---
Bars	---

Confinement type

Confinement type	Tied
Total steel area, A_s	62800 mm ²
Rho	1.36 %
Min. clear spacing	70 mm



No.	P_u kN	M_{ux} kNm	M_{uy} kNm	ϕP_u kN	ϕM_{ux} kNm	ϕM_{uy} kNm	Capacity Ratio
6	22930.0	7660.0	97520.0	15392.19	8593.18	109400.34	0.88

Max. Capacity Ratio: 0.88





รายงานการออกแบบ Design Note รายการคำนวณงานโครงสร้าง

(สัญญาก่อสร้างอาคารทิศตะวันตก Final Detailed Design)

(ส่วนงานโครงสร้าง งานสถาปัตยกรรม และงานระบบหลัก)

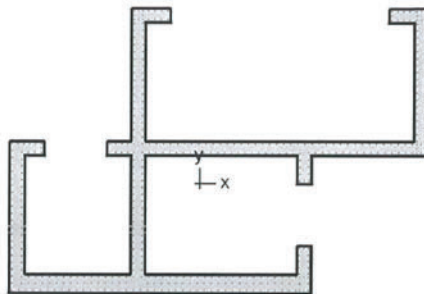
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Contents

1. General Information	3
2. Material Properties	3
2.1. Concrete	3
2.2. Steel	3
3. Section	3
3.1. Shape and Properties	3
3.2. Section Figure	4
3.3. Exterior Points	4
4. Reinforcement	4
4.1. Bar Set: ASTM A615	4
4.2. Confinement and Factors	4
4.3. Arrangement	5
4.4. Bars Provided	5
5. Factored Loads and Moments with Corresponding Capacity Ratios	7
6. Diagrams	9
6.1. PM at $\theta=44$ [deg]	9
6.2. MM at $P=32520$ [kN]	10

List of Figures

Figure 1: Column section	4
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1. General Information

File Name	C:\193018\GCDT\SPcolumn\10-09-63(C1 ...)\P3-L2.col
Project	---
Column	---
Engineer	---
Code	ACI 318-14
Bar Set	ASTM A615
Units	Metric
Run Option	Investigation
Run Axis	Biaxial
Slenderness	Not Considered
Column Type	Structural
Capacity Method	Critical capacity

2. Material Properties

2.1. Concrete

Type	Standard
f_c	35 MPa
E_c	27805.6 MPa
f_t	29.75 MPa
ϵ_u	0.003 mm/mm
β_1	0.796192

2.2. Steel

Type	Standard
f_y	400 MPa
E_s	200000 MPa
ϵ_{yt}	0.002 mm/mm

3. Section

3.1. Shape and Properties

Type	Irregular
A_g	8.6825e+006 mm ²
I_x	2.8376e+013 mm ⁴
I_y	6.17429e+013 mm ⁴
r_x	1807.81 mm
r_y	2666.68 mm
X_o	-0.000117938 mm
Y_o	-0.000235877 mm



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Page | 4

9/18/2020

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3.2. Section Figure

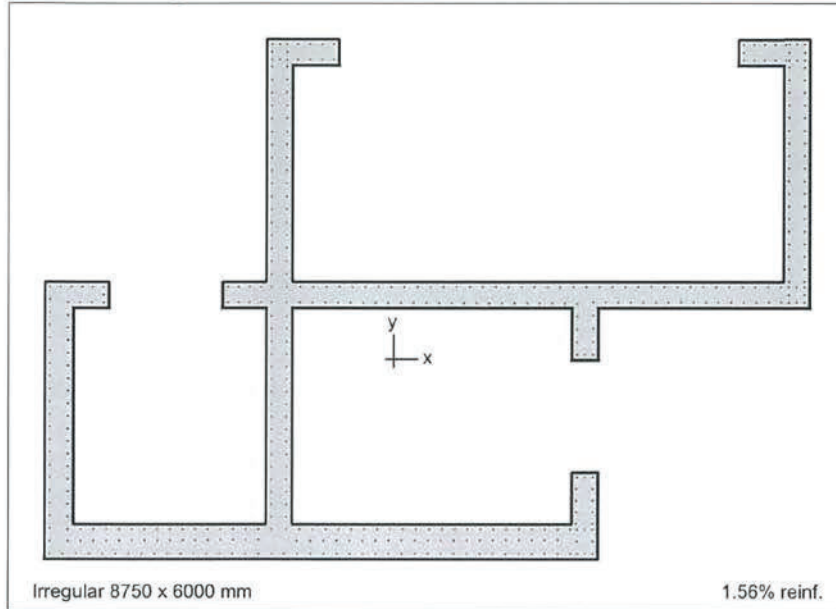


Figure 1: Column section

3.3. Exterior Points

Points	X mm	Y mm	Points	X mm	Y mm	Points	X mm	Y mm
1	2344.9	-1310.9	2	2044.9	-1310.9	3	2044.9	-1910.9
4	-1155.1	-1910.9	5	-1155.1	589.1	6	2044.9	589.1
7	2044.9	-10.9	8	2344.9	-10.9	9	2344.9	589.1
10	4769.9	589.1	11	4769.9	3689.1	12	4469.9	3689.1
13	4469.9	3683.1	14	3944.9	3683.1	15	3944.9	3383.1
16	4469.9	3383.1	17	4469.9	889.1	18	-1155.1	889.1
19	-1155.1	3389.1	20	-630.1	3389.1	21	-630.1	3689.1
22	-1455.1	3689.1	23	-1455.1	889.1	24	-1955.1	889.1
25	-1955.1	589.1	26	-1455.1	589.1	27	-1455.1	-1910.9
28	-3655.1	-1910.9	29	-3655.1	589.1	30	-3255.1	589.1
31	-3255.1	889.1	32	-3980.1	889.1	33	-3980.1	-2310.9
34	2344.9	-2310.9						

4. Reinforcement

4.1. Bar Set: ASTM A615

Bar	Diameter mm	Area mm ²	Bar	Diameter mm	Area mm ²	Bar	Diameter mm	Area mm ²
#3	9.53	70.97	#4	12.70	129.03	#5	15.88	200.00
#6	19.05	283.87	#7	22.23	387.10	#8	25.40	509.68
#9	28.65	645.16	#10	32.26	819.35	#11	35.81	1006.45
#14	43.00	1451.61	#18	57.33	2580.64			

4.2. Confinement and Factors

Confinement type	Tied
For #10 bars or less	#3 ties
For larger bars	#4 ties
Capacity Reduction Factors	
Axial compression, (a)	0.8



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Page | 5

9/18/2020

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Tension controlled ϕ , (b)	0.9
Compression controlled ϕ , (c)	0.65

4.3. Arrangement

Pattern	Irregular
Bar layout	----
Cover to	----
Clear cover	----
Bars	----
Total steel area, A_s	135020 mm ²
Rho	1.56 %
Minimum clear spacing	18 mm



4.4. Bars Provided

Area mm ²	X mm	Y mm	Area mm ²	X mm	Y mm	Area mm ²	X mm	Y mm
314.0	-1395.1	3629.1	314.0	-1305.1	3629.1	314.0	-1215.1	3629.1
314.0	-1215.1	3539.1	314.0	-1215.1	3449.1	314.0	-1305.1	3449.1
314.0	-1395.1	3449.1	314.0	-1395.1	3539.1	314.0	-1305.1	3629.1
314.0	4619.9	3629.1	314.0	4529.9	3629.1	314.0	4529.9	3536.1
314.0	4529.9	3443.1	314.0	4619.9	3443.1	314.0	4709.9	3443.1
314.0	4709.9	3536.1	314.0	4709.9	649.1	314.0	4619.9	649.1
314.0	4529.9	649.1	314.0	4529.9	739.1	314.0	4529.9	829.1
314.0	4619.9	829.1	314.0	4709.9	829.1	314.0	4709.9	739.1
314.0	2104.9	-1970.9	314.0	2194.9	-1970.9	314.0	2284.9	-1970.9
314.0	2284.9	-2110.9	314.0	2284.9	-2250.9	314.0	2194.9	-2250.9
314.0	2104.9	-2250.9	314.0	2104.9	-2110.9	314.0	2104.9	-1370.9
314.0	2194.9	-1370.9	314.0	2284.9	-1504.4	314.0	2284.9	-1370.9
314.0	2284.9	-1904.9	314.0	2284.9	-1771.4	314.0	2284.9	-1637.9
314.0	2094.9	-1504.4	314.0	2094.9	-1904.9	314.0	2094.9	-1771.4
314.0	2094.9	-1637.9	314.0	-3920.1	-2250.9	314.0	-3920.1	-2104.3
314.0	-3920.1	-1957.6	314.0	-3920.1	-1810.9	314.0	-3920.1	-1664.3
314.0	-3920.1	-1517.6	314.0	-3920.1	-1370.9	314.0	-3920.1	-1224.3
314.0	-3920.1	-1077.6	314.0	-3920.1	-930.9	314.0	-3920.1	-784.3
314.0	-3920.1	-637.6	314.0	-3920.1	-490.9	314.0	-3920.1	-344.3
314.0	-3920.1	-197.6	314.0	-3920.1	-50.9	314.0	-3920.1	95.7
314.0	-3920.1	242.4	314.0	-3920.1	389.1	314.0	-3920.1	535.7
314.0	-3920.1	682.4	314.0	-3920.1	829.1	314.0	-3799.1	829.1
314.0	-3771.3	-2250.9	314.0	-3715.1	-1970.9	314.0	-3715.1	-1825.4
314.0	-3715.1	-1679.8	314.0	-3715.1	-1534.3	314.0	-3715.1	-1388.7
314.0	-3715.1	-1243.2	314.0	-3715.1	-1097.6	314.0	-3715.1	-952.0
314.0	-3715.1	-806.5	314.0	-3715.1	-660.9	314.0	-3715.1	-515.4
314.0	-3715.1	-369.8	314.0	-3715.1	-224.3	314.0	-3715.1	-78.7
314.0	-3715.1	66.8	314.0	-3715.1	212.4	314.0	-3715.1	358.0
314.0	-3715.1	503.5	314.0	-3715.1	649.1	314.0	-3678.1	829.1
314.0	-3622.5	-2250.9	314.0	-3581.8	649.1	314.0	-3570.1	-1970.9
314.0	-3557.1	829.1	314.0	-3473.7	-2250.9	314.0	-3448.4	649.1
314.0	-3436.1	829.1	314.0	-3425.1	-1970.9	314.0	-3324.8	-2250.9
314.0	-3315.1	649.1	314.0	-3315.1	739.1	314.0	-3315.1	829.1
314.0	-3280.1	-1970.9	314.0	-3176.0	-2250.9	314.0	-3135.1	-1970.9
314.0	-3027.2	-2250.9	314.0	-2990.1	-1970.9	314.0	-2878.4	-2250.9
314.0	-2845.1	-1970.9	314.0	-2729.5	-2250.9	314.0	-2700.1	-1970.9
314.0	-2580.7	-2250.9	314.0	-2555.1	-1970.9	314.0	-2431.9	-2250.9
314.0	-2410.1	-1970.9	314.0	-2283.1	-2250.9	314.0	-2265.1	-1970.9
314.0	-2134.2	-2250.9	314.0	-2120.1	-1970.9	314.0	-1985.4	-2250.9
314.0	-1975.1	-1970.9	314.0	-1836.6	-2250.9	314.0	-1830.1	-1970.9
314.0	-1687.8	-2250.9	314.0	-1685.1	-1970.9	314.0	-1540.1	-1970.9



รายงานการออกแบบ Design Note รายการคำนวณงานโครงสร้าง

(สัญญาก่อสร้างอาคารทิศตะวันตก Final Detailed Design)

(ส่วนงานโครงสร้าง งานสถาปัตยกรรม และงานระบบหลัก)

โครงการพัฒนาพื้นที่ส่วนขยายศูนย์ราชการเฉลิมพระเกียรติ ๘๐ พรรษา ๕ ธันวาคม ๒๕๕๐ พื้นที่โซน C

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Page | 6

9/18/2020

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Area mm ²	X mm	Y mm	Area mm ²	X mm	Y mm	Area mm ²	X mm	Y mm
314.0	-1539.0	-2250.9	314.0	-1395.1	-1970.9	314.0	-1395.1	-1826.2
314.0	-1395.1	-1681.4	314.0	-1395.1	-1536.6	314.0	-1395.1	-1391.8
314.0	-1395.1	-1247.0	314.0	-1395.1	-1102.3	314.0	-1395.1	-957.5
314.0	-1395.1	-812.7	314.0	-1395.1	-667.9	314.0	-1395.1	-523.2
314.0	-1395.1	-378.4	314.0	-1395.1	-233.6	314.0	-1395.1	-88.8
314.0	-1395.1	56.0	314.0	-1395.1	200.7	314.0	-1395.1	345.5
314.0	-1395.1	490.3	314.0	-1390.1	-2250.9	314.0	-1241.3	-2250.9
314.0	-1215.1	490.3	314.0	-1215.1	345.5	314.0	-1215.1	200.7
314.0	-1215.1	56.0	314.0	-1215.1	-88.8	314.0	-1215.1	-233.6
314.0	-1215.1	-378.4	314.0	-1215.1	-523.2	314.0	-1215.1	-667.9
314.0	-1215.1	-812.7	314.0	-1215.1	-957.5	314.0	-1215.1	-1102.3
314.0	-1215.1	-1247.0	314.0	-1215.1	-1391.8	314.0	-1215.1	-1536.6
314.0	-1215.1	-1970.9	314.0	-1215.1	-1681.4	314.0	-1215.1	-1826.2
314.0	-1092.5	-2250.9	314.0	-1067.5	-1970.9	314.0	-943.7	-2250.9
314.0	-919.9	-1970.9	314.0	-794.8	-2250.9	314.0	-772.3	-1970.9
314.0	-646.0	-2250.9	314.0	-624.7	-1970.9	314.0	-497.2	-2250.9
314.0	-477.1	-1970.9	314.0	-348.4	-2250.9	314.0	-329.5	-1970.9
314.0	-199.6	-2250.9	314.0	-181.9	-1970.9	314.0	-50.7	-2250.9
314.0	-34.3	-1970.9	314.0	98.1	-2250.9	314.0	113.3	-1970.9
314.0	246.9	-2250.9	314.0	260.9	-1970.9	314.0	395.7	-2250.9
314.0	408.5	-1970.9	314.0	544.6	-2250.9	314.0	556.1	-1970.9
314.0	693.4	-2250.9	314.0	703.7	-1970.9	314.0	842.2	-2250.9
314.0	851.3	-1970.9	314.0	991.0	-2250.9	314.0	998.9	-1970.9
314.0	1139.8	-2250.9	314.0	1146.5	-1970.9	314.0	1288.7	-2250.9
314.0	1294.1	-1970.9	314.0	1437.5	-2250.9	314.0	1441.7	-1970.9
314.0	1586.3	-2250.9	314.0	1589.4	-1970.9	314.0	1735.1	-2250.9
314.0	1737.0	-1970.9	314.0	1884.0	-2250.9	314.0	1884.6	-1970.9
314.0	2032.2	-1970.9	314.0	2032.8	-2250.9	314.0	-1895.1	829.1
314.0	-1770.1	829.1	314.0	-1645.1	829.1	314.0	-1520.1	829.1
314.0	-1395.1	829.1	314.0	-1895.1	649.1	314.0	-1770.1	649.1
314.0	-1645.1	649.1	314.0	-1520.1	649.1	314.0	-1395.1	649.1
314.0	-1215.1	649.1	314.0	-1070.8	648.5	314.0	-926.4	647.8
314.0	-782.1	647.2	314.0	-637.7	646.6	314.0	-493.4	646.0
314.0	-349.0	645.4	314.0	-204.7	644.8	314.0	-60.3	644.2
314.0	84.0	643.6	314.0	228.4	643.0	314.0	372.7	642.4
314.0	517.1	641.8	314.0	661.4	641.2	314.0	805.8	640.5
314.0	950.1	639.9	314.0	1094.4	639.3	314.0	1238.8	638.7
314.0	1383.1	638.1	314.0	1527.5	637.5	314.0	1671.8	636.9
314.0	1816.2	636.3	314.0	1960.5	635.7	314.0	2104.9	49.1
314.0	2104.9	195.6	314.0	2104.9	342.1	314.0	2104.9	488.6
314.0	2104.9	635.1	314.0	2194.9	49.1	314.0	2284.9	49.1
314.0	2284.9	199.1	314.0	2284.9	349.1	314.0	2284.9	499.1
314.0	2284.9	649.1	314.0	2428.7	649.1	314.0	2572.6	649.1
314.0	2716.5	649.1	314.0	2860.3	649.1	314.0	3004.2	649.1
314.0	3148.0	649.1	314.0	3291.9	649.1	314.0	3435.8	649.1
314.0	3579.6	649.1	314.0	3723.5	649.1	314.0	3867.3	649.1
314.0	4011.2	649.1	314.0	4155.0	649.1	314.0	4298.9	649.1
314.0	4442.8	649.1	314.0	-1215.1	978.5	314.0	-1215.1	1128.0
314.0	-1215.1	1277.4	314.0	-1215.1	1426.9	314.0	-1215.1	1576.3
314.0	-1215.1	1725.7	314.0	-1215.1	1875.2	314.0	-1215.1	2024.6
314.0	-1215.1	2174.1	314.0	-1215.1	2323.5	314.0	-1215.1	2473.0
314.0	-1215.1	2622.4	314.0	-1215.1	2771.9	314.0	-1215.1	2921.3
314.0	-1215.1	3070.8	314.0	-1215.1	3220.2	314.0	-1215.1	3369.7
314.0	-1215.1	829.1	314.0	-1066.3	829.1	314.0	-917.4	829.1
314.0	-768.6	829.1	314.0	-619.8	829.1	314.0	-470.9	829.1
314.0	-322.1	829.1	314.0	-173.2	829.1	314.0	-24.4	829.1
314.0	124.4	829.1	314.0	273.3	829.1	314.0	422.1	829.1
314.0	571.0	829.1	314.0	719.8	829.1	314.0	868.6	829.1
314.0	1017.5	829.1	314.0	1166.3	829.1	314.0	1315.1	829.1





รายงานการออกแบบ Design Note รายการคำนวณงานโครงสร้าง

(สัญญาก่อสร้างอาคารทิศตะวันตก Final Detailed Design)

(ส่วนงานโครงสร้าง งานสถาปัตยกรรม และงานระบบหลัก)

โครงการพัฒนาพื้นที่ส่วนขยายศูนย์ราชการเฉลิมพระเกียรติ ๘๐ พรรษา ๕ ธันวาคม ๒๕๕๐ พื้นที่โซน C

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Page | 7

9/18/2020

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Area mm ²	X mm	Y mm	Area mm ²	X mm	Y mm	Area mm ²	X mm	Y mm
314.0	1464.0	829.1	314.0	1612.8	829.1	314.0	1761.7	829.1
314.0	1910.5	829.1	314.0	2059.3	829.1	314.0	2208.2	829.1
314.0	2357.0	829.1	314.0	2505.9	829.1	314.0	2654.7	829.1
314.0	2803.5	829.1	314.0	2952.4	829.1	314.0	3101.2	829.1
314.0	3250.0	829.1	314.0	3398.9	829.1	314.0	3547.7	829.1
314.0	3696.6	829.1	314.0	3845.4	829.1	314.0	3994.2	829.1
314.0	4143.1	829.1	314.0	4291.9	829.1	314.0	4440.8	829.1
314.0	-1395.1	974.7	314.0	-1395.1	1124.2	314.0	-1395.1	1273.7
314.0	-1395.1	1423.2	314.0	-1395.1	1572.7	314.0	-1395.1	1722.2
314.0	-1395.1	1871.7	314.0	-1395.1	2021.1	314.0	-1395.1	2170.6
314.0	-1395.1	2320.1	314.0	-1395.1	2469.6	314.0	-1395.1	2619.1
314.0	-1395.1	2768.6	314.0	-1395.1	2918.1	314.0	-1395.1	3067.6
314.0	-1395.1	3217.1	314.0	-1395.1	3366.6	314.0	-1096.1	3629.1
314.0	-960.8	3629.1	314.0	-825.4	3629.1	314.0	-690.1	3629.1
314.0	-1096.1	3449.1	314.0	-960.8	3449.1	314.0	-825.4	3449.1
314.0	-690.1	3449.1	314.0	4004.9	3443.1	314.0	4004.9	3533.1
314.0	4004.9	3623.1	314.0	4126.6	3443.1	314.0	4126.6	3623.1
314.0	4248.4	3443.1	314.0	4248.4	3623.1	314.0	4370.1	3443.1
314.0	4370.1	3623.1	314.0	4491.9	3443.1	314.0	4491.9	3623.1
314.0	4529.9	2199.3	314.0	4529.9	2344.8	314.0	4529.9	2490.4
314.0	4529.9	2636.0	314.0	4529.9	2781.6	314.0	4529.9	2927.2
314.0	4529.9	3072.7	314.0	4529.9	3218.3	314.0	4529.9	3363.9
314.0	4529.9	889.1	314.0	4529.9	1034.6	314.0	4529.9	1180.2
314.0	4529.9	1325.8	314.0	4529.9	1471.4	314.0	4529.9	1617.0
314.0	4529.9	1762.5	314.0	4529.9	1908.1	314.0	4529.9	2053.7
314.0	4709.9	2780.0	314.0	4709.9	2925.5	314.0	4709.9	3070.9
314.0	4709.9	3216.4	314.0	4709.9	3361.9	314.0	4709.9	1616.4
314.0	4709.9	1761.8	314.0	4709.9	1907.3	314.0	4709.9	2052.7
314.0	4709.9	2198.2	314.0	4709.9	2343.7	314.0	4709.9	2489.1
314.0	4709.9	2634.6	314.0	4709.9	889.1	314.0	4709.9	1034.5
314.0	4709.9	1180.0	314.0	4709.9	1325.4	314.0	4709.9	1470.9
314.0	-1096.1	-2105.6	314.0	-947.0	-2105.1	314.0	-797.8	-2104.6
314.0	-648.7	-2104.1	314.0	-499.5	-2103.5	314.0	-350.3	-2103.0
314.0	-201.2	-2102.5	314.0	-52.0	-2102.0	314.0	97.1	-2101.4
314.0	246.3	-2100.9	314.0	395.4	-2100.4	314.0	544.6	-2099.8
314.0	693.7	-2099.3	314.0	842.9	-2098.8	314.0	992.0	-2098.3
314.0	1141.2	-2097.7	314.0	1290.3	-2097.2	314.0	1439.5	-2096.7
314.0	1588.6	-2096.2	314.0	1737.8	-2095.6	314.0	1887.0	-2095.1
314.0	-3712.6	-2106.4	314.0	-3567.6	-2105.4	314.0	-3422.7	-2104.4
314.0	-3277.7	-2103.4	314.0	-3132.8	-2102.4	314.0	-2987.8	-2101.4
314.0	-2842.9	-2100.4	314.0	-2697.9	-2099.4	314.0	-2553.0	-2098.4
314.0	-2408.0	-2097.3	314.0	-2263.1	-2096.3	314.0	-2118.1	-2095.3
314.0	-1973.2	-2094.3	314.0	-1828.2	-2093.3	314.0	-1683.3	-2092.3
314.0	-1538.3	-2091.3						

5. Factored Loads and Moments with Corresponding Capacity Ratios

NOTE: Calculations are based on "Critical Capacity" Method.

No.	Demand			Capacity			Parameters at Capacity			Capacity Ratio
	P _u kN	M _{ux} kNm	M _{uy} kNm	φP _n kN	φM _{nx} kNm	φM _{ny} kNm	NA Depth mm	ε _t	φ	
1	8100.00	14430.00	65540.00	0.00	30474.13	138411.25	1198	0.01435	0.900	0.69
2	39480.00	14450.00	56680.00	0.00	34248.41	134339.09	1239	0.01389	0.900	0.58
3	20190.00	18350.00	85420.00	0.00	29872.96	139059.86	1192	0.01442	0.900	0.74
4	31510.00	73530.00	81820.00	9941.86	85603.32	95254.51	1802	0.00866	0.900	0.83
5	27190.00	26660.00	147420.00	10277.38	30177.01	166867.83	1420	0.01159	0.900	0.87
6	32520.00	91080.00	88620.00	19341.96	99519.65	96831.69	2023	0.00739	0.900	0.89
7	28190.00	28530.00	17183.00	0.00	93711.84	56440.61	1514	0.01093	0.900	0.51





รายงานการออกแบบ Design Note รายการคำนวณงานโครงสร้าง
(สัญญาก่อสร้างอาคารทิศตะวันตก Final Detailed Design)
(ส่วนงานโครงสร้าง งานสถาปัตยกรรม และงานระบบหลัก)

โครงการพัฒนาพื้นที่ส่วนขยายศูนย์ราชการเฉลิมพระเกียรติ ๘๐ พรรษา ๕ ธันวาคม ๒๕๕๐ พื้นที่โซน C

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Page | 8
9/18/2020
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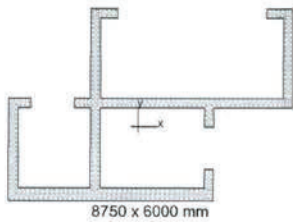
Page | 9

9/18/2020

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6. Diagrams

6.1. PM at $\theta=44$ [deg]



General Information

Project	---
Column	---
Engineer	---
Code	ACI 318-14
Bar Set	ASTM A615
Units	Metric
Run Option	Investigation
Run Axis	Biaxial
Slenderness	Not Considered
Column Type	Structural
Capacity Method	Critical capacity

Materials

f_c	35 MPa
E_c	27805.6 MPa
f_y	400 MPa
E_s	200000 MPa

Section

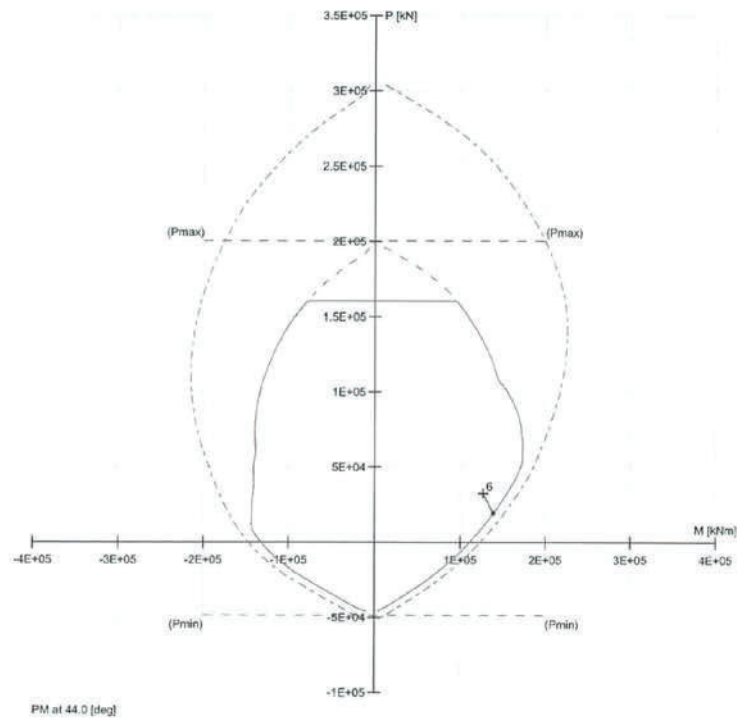
Type	Irregular
A_g	8.6825e+006 mm ²
I_x	2.8376e+013 mm ⁴
I_y	6.17429e+013 mm ⁴

Reinforcement

Pattern	Irregular
Bar layout	---
Cover to	---
Clear cover	---
Bars	---

Confinement type

Confinement type	Tied
Total steel area, A_s	135020 mm ²
Rho	1.56 %
Min. clear spacing	18 mm



No.	P_u kN	M_{ux} kNm	M_{uy} kNm	ϕP_n kN	ϕM_{nx} kNm	ϕM_{ny} kNm	Capacity Ratio
6	32520.0	91080.0	88620.0	19341.96	99519.65	96831.69	0.89

Max. Capacity Ratio: 0.89



STRUCTUREPOINT - spColumn v6.50

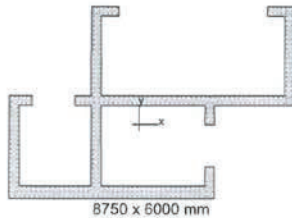
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Page | 10

9/18/2020

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6.2. MM at P=32520 [kN]



General Information

Project	---
Column	---
Engineer	---
Code	ACI 318-14
Bar Set	ASTM A615
Units	Metric
Run Option	Investigation
Run Axis	Biaxial
Slenderness	Not Considered
Column Type	Structural
Capacity Method	Critical capacity

Materials

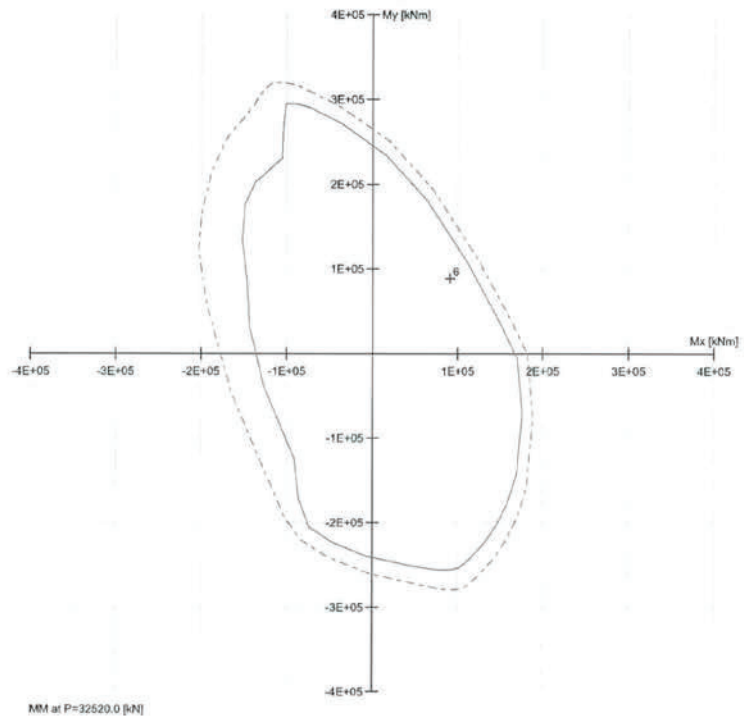
f_c	35 MPa
E_c	27805.6 MPa
f_y	400 MPa
E_s	200000 MPa

Section

Type	Irregular
A_g	8.6825e+006 mm ²
I_x	2.8376e+013 mm ⁴
I_y	6.17429e+013 mm ⁴

Reinforcement

Pattern	Irregular
Bar layout	---
Cover to	---
Clear cover	---
Bars	---
Confinement type	Tied
Total steel area, A_s	135020 mm ²
Rho	1.56 %
Min. clear spacing	18 mm



No.	P_u kN	M_{ux} kNm	M_{uy} kNm	ϕP_n kN	ϕM_{nx} kNm	ϕM_{ny} kNm	Capacity Ratio
6	32520.0	91080.0	88620.0	19341.96	99519.65	96831.69	0.89

Max. Capacity Ratio: 0.89





รายงานการออกแบบ Design Note รายการคำนวณงานโครงสร้าง

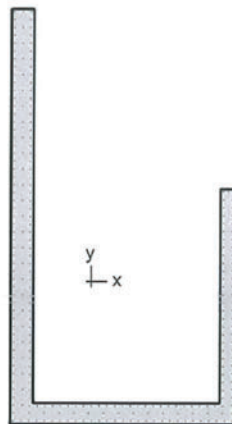
(สัญญาก่อสร้างอาคารทิศตะวันตก Final Detailed Design)

(ส่วนงานโครงสร้าง งานสถาปัตยกรรม และงานระบบหลัก)

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Contents

1. General Information	3
2. Material Properties	3
2.1. Concrete	3
2.2. Steel	3
3. Section	3
3.1. Shape and Properties	3
3.2. Section Figure	4
3.3. Exterior Points	4
4. Reinforcement	4
4.1. Bar Set: ASTM A615	4
4.2. Confinement and Factors	4
4.3. Arrangement	4
4.4. Bars Provided	5
5. Factored Loads and Moments with Corresponding Capacity Ratios	6
6. Diagrams	7
6.1. PM at $\theta=0$ [deg]	7
6.2. MM at $P=37620$ [kN]	8

List of Figures

Figure 1: Column section	4
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Page | 3
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1. General Information

File Name	C:\193018\GCDT\SPcolumn\10-09-63(C1 ...)\P4-L2.col
Project	---
Column	---
Engineer	---
Code	ACI 318-14
Bar Set	ASTM A615
Units	Metric
Run Option	Investigation
Run Axis	Biaxial
Slenderness	Not Considered
Column Type	Structural
Capacity Method	Critical capacity

2. Material Properties

2.1. Concrete

Type	Standard
f_c	35 MPa
E_c	27805.6 MPa
f_c	29.75 MPa
ϵ_u	0.003 mm/mm
β_1	0.796192

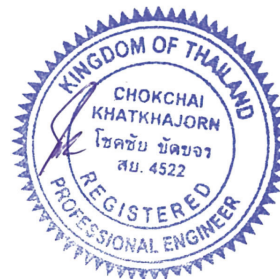
2.2. Steel

Type	Standard
f_y	400 MPa
E_s	200000 MPa
ϵ_{y1}	0.002 mm/mm

3. Section

3.1. Shape and Properties

Type	Irregular
A_g	6.07125e+006 mm ²
I_x	3.34113e+013 mm ⁴
I_y	1.65083e+013 mm ⁴
r_x	2345.89 mm
r_y	1648.97 mm
X_o	0 mm
Y_o	-0.000168664 mm



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Page | 4

9/18/2020
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3.2. Section Figure

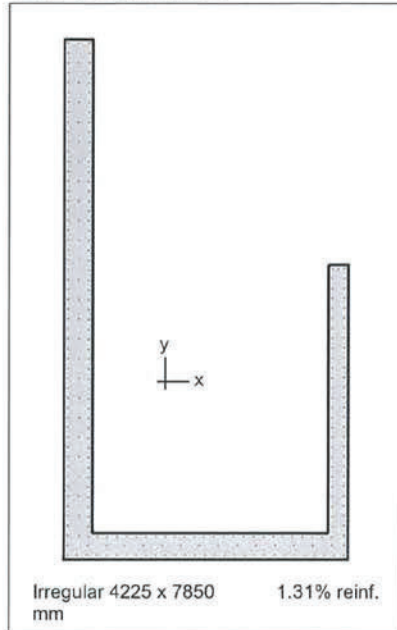


Figure 1: Column section

3.3. Exterior Points

Points	X mm	Y mm	Points	X mm	Y mm	Points	X mm	Y mm
1	2710.6	1757.8	2	2410.6	1757.8	3	2410.6	-2292.2
4	-1089.4	-2292.2	5	-1089.4	5157.8	6	-1514.4	5157.8
7	-1514.4	-2692.2	8	2710.6	-2692.2			

4. Reinforcement

4.1. Bar Set: ASTM A615

Bar	Diameter mm	Area mm ²	Bar	Diameter mm	Area mm ²	Bar	Diameter mm	Area mm ²
#3	9.53	70.97	#4	12.70	129.03	#5	15.88	200.00
#6	19.05	283.87	#7	22.23	387.10	#8	25.40	509.68
#9	28.65	645.16	#10	32.26	819.35	#11	35.81	1006.45
#14	43.00	1451.61	#18	57.33	2580.64			

4.2. Confinement and Factors

Confinement type	Tied
For #10 bars or less	#3 ties
For larger bars	#4 ties
Capacity Reduction Factors	
Axial compression, (a)	0.8
Tension controlled ϕ , (b)	0.9
Compression controlled ϕ , (c)	0.65

4.3. Arrangement

Pattern	Irregular
Bar layout	---





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Page | 5

9/18/2020

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Cover to	---
Clear cover	---
Bars	---
Total steel area, A_s	79756 mm ²
Rho	1.31 %
Minimum clear spacing	70 mm



4.4. Bars Provided

Area mm ²	X mm	Y mm	Area mm ²	X mm	Y mm	Area mm ²	X mm	Y mm
314.0	-1454.4	-2632.2	314.0	-1454.4	-2483.6	314.0	-1454.4	-2334.9
314.0	-1454.4	-2186.3	314.0	-1454.4	-2037.6	314.0	-1454.4	-1889.0
314.0	-1454.4	-1740.3	314.0	-1454.4	-1591.6	314.0	-1454.4	-1443.0
314.0	-1454.4	-1294.3	314.0	-1454.4	-1145.7	314.0	-1454.4	-997.0
314.0	-1454.4	-848.4	314.0	-1454.4	-699.7	314.0	-1454.4	-551.1
314.0	-1454.4	-402.4	314.0	-1454.4	-253.8	314.0	-1454.4	-105.1
314.0	-1454.4	43.5	314.0	-1454.4	192.2	314.0	-1454.4	340.9
314.0	-1454.4	489.5	314.0	-1454.4	638.2	314.0	-1454.4	786.8
314.0	-1454.4	935.5	314.0	-1454.4	1084.1	314.0	-1454.4	1232.8
314.0	-1454.4	1381.4	314.0	-1454.4	1530.1	314.0	-1454.4	1678.7
314.0	-1454.4	1827.4	314.0	-1454.4	1976.0	314.0	-1454.4	2124.7
314.0	-1454.4	2273.4	314.0	-1454.4	2422.0	314.0	-1454.4	2570.7
314.0	-1454.4	2719.3	314.0	-1454.4	2868.0	314.0	-1454.4	3016.6
314.0	-1454.4	3165.3	314.0	-1454.4	3313.9	314.0	-1454.4	3462.6
314.0	-1454.4	3611.2	314.0	-1454.4	3759.9	314.0	-1454.4	3908.5
314.0	-1454.4	4057.2	314.0	-1454.4	4205.9	314.0	-1454.4	4354.5
314.0	-1454.4	4503.2	314.0	-1454.4	4651.8	314.0	-1454.4	4800.5
314.0	-1454.4	4949.1	314.0	-1454.4	5097.8	314.0	-1307.8	-2632.2
314.0	-1161.2	-2632.2	314.0	-1149.4	-2352.2	314.0	-1149.4	-2203.2
314.0	-1149.4	-2054.2	314.0	-1149.4	-1905.2	314.0	-1149.4	-1756.2
314.0	-1149.4	-1607.2	314.0	-1149.4	-1458.2	314.0	-1149.4	-1309.2
314.0	-1149.4	-1160.2	314.0	-1149.4	-1011.2	314.0	-1149.4	-862.2
314.0	-1149.4	-713.2	314.0	-1149.4	-564.2	314.0	-1149.4	-415.2
314.0	-1149.4	-266.2	314.0	-1149.4	-117.2	314.0	-1149.4	31.8
314.0	-1149.4	180.8	314.0	-1149.4	329.8	314.0	-1149.4	478.8
314.0	-1149.4	627.8	314.0	-1149.4	776.8	314.0	-1149.4	925.8
314.0	-1149.4	1074.8	314.0	-1149.4	1223.8	314.0	-1149.4	1372.8
314.0	-1149.4	1521.8	314.0	-1149.4	1670.8	314.0	-1149.4	1819.8
314.0	-1149.4	1968.8	314.0	-1149.4	2117.8	314.0	-1149.4	2266.8
314.0	-1149.4	2415.8	314.0	-1149.4	2564.8	314.0	-1149.4	2713.8
314.0	-1149.4	2862.8	314.0	-1149.4	3011.8	314.0	-1149.4	3160.8
314.0	-1149.4	3309.8	314.0	-1149.4	3458.8	314.0	-1149.4	3607.8
314.0	-1149.4	3756.8	314.0	-1149.4	3905.8	314.0	-1149.4	4054.8
314.0	-1149.4	4203.8	314.0	-1149.4	4352.8	314.0	-1149.4	4501.8
314.0	-1149.4	4650.8	314.0	-1149.4	4799.8	314.0	-1149.4	4948.8
314.0	-1149.4	5097.8	314.0	-1014.5	-2632.2	314.0	-1004.6	-2352.2
314.0	-867.9	-2632.2	314.0	-859.8	-2352.2	314.0	-721.3	-2632.2
314.0	-715.0	-2352.2	314.0	-574.7	-2632.2	314.0	-570.2	-2352.2
314.0	-428.1	-2632.2	314.0	-425.4	-2352.2	314.0	-281.5	-2632.2
314.0	-280.6	-2352.2	314.0	-135.8	-2352.2	314.0	-134.9	-2632.2
314.0	9.0	-2352.2	314.0	11.7	-2632.2	314.0	153.8	-2352.2
314.0	158.3	-2632.2	314.0	298.6	-2352.2	314.0	304.9	-2632.2
314.0	443.4	-2352.2	314.0	451.5	-2632.2	314.0	588.2	-2352.2
314.0	598.1	-2632.2	314.0	733.0	-2352.2	314.0	744.7	-2632.2
314.0	877.8	-2352.2	314.0	891.4	-2632.2	314.0	1022.6	-2352.2
314.0	1038.0	-2632.2	314.0	1167.4	-2352.2	314.0	1184.6	-2632.2
314.0	1312.2	-2352.2	314.0	1331.2	-2632.2	314.0	1457.0	-2352.2
314.0	1477.8	-2632.2	314.0	1601.8	-2352.2	314.0	1624.4	-2632.2
314.0	1746.6	-2352.2	314.0	1771.0	-2632.2	314.0	1891.4	-2352.2



รายงานการออกแบบ Design Note รายการคำนวณงานโครงสร้าง

(สัญญาก่อสร้างอาคารทิศตะวันตก Final Detailed Design)

(ส่วนงานโครงสร้าง งานสถาปัตยกรรม และงานระบบหลัก)

โครงการพัฒนาพื้นที่ส่วนขยายศูนย์ราชการเฉลิมพระเกียรติ ๘๐ พรรษา ๕ ธันวาคม ๒๕๕๐ พื้นที่โซน C

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Page | 6

9/18/2020

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Area mm ²	X mm	Y mm	Area mm ²	X mm	Y mm	Area mm ²	X mm	Y mm
314.0	1917.6	-2632.2	314.0	2036.2	-2352.2	314.0	2064.2	-2632.2
314.0	2181.0	-2352.2	314.0	2210.8	-2632.2	314.0	2325.8	-2352.2
314.0	2357.4	-2632.2	314.0	2470.6	-2352.2	314.0	2470.6	-2202.2
314.0	2470.6	-2052.2	314.0	2470.6	-1902.2	314.0	2470.6	-1752.2
314.0	2470.6	-1602.2	314.0	2470.6	-1452.2	314.0	2470.6	-1302.2
314.0	2470.6	-1152.2	314.0	2470.6	-1002.2	314.0	2470.6	-852.2
314.0	2470.6	-702.2	314.0	2470.6	-552.2	314.0	2470.6	-402.2
314.0	2470.6	-252.2	314.0	2470.6	-102.2	314.0	2470.6	47.8
314.0	2470.6	197.8	314.0	2470.6	347.8	314.0	2470.6	497.8
314.0	2470.6	647.8	314.0	2470.6	797.8	314.0	2470.6	947.8
314.0	2470.6	1097.8	314.0	2470.6	1247.8	314.0	2470.6	1397.8
314.0	2470.6	1547.8	314.0	2470.6	1697.8	314.0	2504.0	-2632.2
314.0	2560.6	1697.8	314.0	2650.6	-2632.2	314.0	2650.6	-2482.9
314.0	2650.6	-2333.6	314.0	2650.6	-2184.3	314.0	2650.6	-2035.0
314.0	2650.6	-1885.7	314.0	2650.6	-1736.4	314.0	2650.6	-1587.1
314.0	2650.6	-1437.7	314.0	2650.6	-1288.4	314.0	2650.6	-1139.1
314.0	2650.6	-989.8	314.0	2650.6	-840.5	314.0	2650.6	-691.2
314.0	2650.6	-541.9	314.0	2650.6	-392.6	314.0	2650.6	-243.3
314.0	2650.6	-93.9	314.0	2650.6	55.4	314.0	2650.6	204.7
314.0	2650.6	354.0	314.0	2650.6	503.3	314.0	2650.6	652.6
314.0	2650.6	801.9	314.0	2650.6	951.2	314.0	2650.6	1100.5
314.0	2650.6	1249.8	314.0	2650.6	1399.2	314.0	2650.6	1548.5
314.0	2650.6	1697.8	314.0	-1301.9	5097.8	314.0	-1301.1	4800.5
314.0	-1300.3	4503.1	314.0	-1299.6	4205.8	314.0	-1298.8	3908.5
314.0	-1298.0	3611.2	314.0	-1297.3	3313.9	314.0	-1296.5	3016.5
314.0	-1295.7	2719.2	314.0	-1295.0	2421.9	314.0	-1294.2	2124.6
314.0	-1293.5	1827.3	314.0	-1292.7	1529.9	314.0	-1291.9	1232.6
314.0	-1291.2	935.3	314.0	-1290.4	638.0	314.0	-1289.6	340.7
314.0	-1288.9	43.3	314.0	-1288.1	-254.0	314.0	-1287.3	-551.3
314.0	-1286.6	-848.6	314.0	-1285.8	-1145.9	314.0	-1285.0	-1443.3
314.0	-1284.3	-1740.6	314.0	-1283.5	-2037.9	314.0	-1282.7	-2335.2
314.0	-1152.3	-2485.8	314.0	-873.9	-2485.6	314.0	-595.5	-2485.5
314.0	-317.1	-2485.3	314.0	-38.8	-2485.1	314.0	239.6	-2485.0
314.0	518.0	-2484.8	314.0	796.4	-2484.7	314.0	1074.7	-2484.5
314.0	1353.1	-2484.4	314.0	1631.5	-2484.2	314.0	1909.9	-2484.1
314.0	2188.3	-2483.9	314.0	2466.6	-2483.8			

5. Factored Loads and Moments with Corresponding Capacity Ratios

NOTE: Calculations are based on "Critical Capacity" Method.

No.	Demand			Capacity			Parameters at Capacity			Capacity Ratio
	P _u	M _{ux}	M _{uy}	φP _n	φM _{nx}	φM _{ny}	NA Depth	ε _t	φ	
	kN	kNm	kNm	kN	kNm	kNm	mm			
1	8950.00	22220.00	7760.00	0.00	72261.95	25236.40	372	0.07828	0.900	0.74
2	42930.00	17590.00	13670.00	0.00	67910.73	52776.55	996	0.02369	0.900	0.51
3	29860.00	48030.00	18960.00	4712.17	83456.88	32944.88	482	0.05947	0.900	0.71
4	23560.00	17000.00	18640.00	0.00	58490.25	64132.84	1174	0.01686	0.900	0.62
5	32950.00	38240.00	41760.00	3097.69	64167.63	70074.27	1281	0.01539	0.900	0.67
6	37620.00	99840.00	77.00	20602.70	120536.41	92.96	850	0.02596	0.900	0.81



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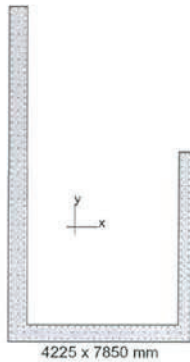
Page | 7

9/18/2020

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6. Diagrams

6.1. PM at $\theta=0$ [deg]



General Information

Project	---
Column	---
Engineer	---
Code	ACI 318-14
Bar Set	ASTM A615
Units	Metric
Run Option	Investigation
Run Axis	Biaxial
Slenderness	Not Considered
Column Type	Structural
Capacity Method	Critical capacity

Materials

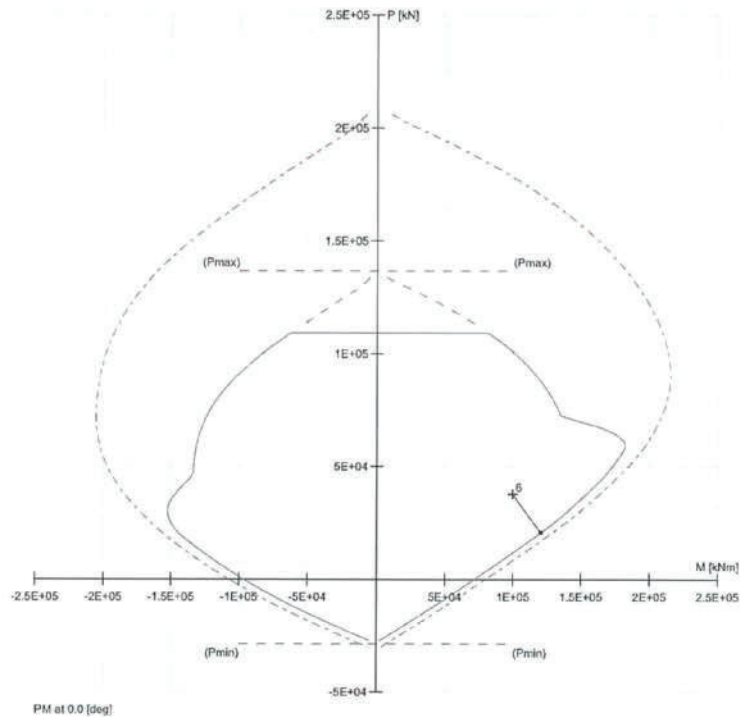
f_c	35 MPa
E_s	27805.6 MPa
f_y	400 MPa
E_s	200000 MPa

Section

Type	Irregular
A_g	6.07125e+006 mm ²
I_x	3.34113e+013 mm ⁴
I_y	1.65083e+013 mm ⁴

Reinforcement

Pattern	Irregular
Bar layout	---
Cover to	---
Clear cover	---
Bars	---
Confinement type	Tied
Total steel area, A_s	79756 mm ²
Rho	1.31 %
Min. clear spacing	70 mm



No.	P_u kN	M_{ux} kNm	M_{uy} kNm	ϕP_n kN	ϕM_{nx} kNm	ϕM_{ny} kNm	Capacity Ratio
6	37620.0	99840.0	77.0	20602.70	120536.41	92.96	0.81

Max. Capacity Ratio: 0.81



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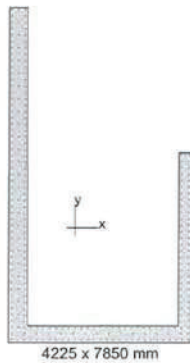
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Page | 8

9/18/2020

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6.2. MM at P=37620 [kN]



General Information

Project	---
Column	---
Engineer	---
Code	ACI 318-14
Bar Set	ASTM A615
Units	Metric
Run Option	Investigation
Run Axis	Biaxial
Slenderness	Not Considered
Column Type	Structural
Capacity Method	Critical capacity

Materials

f_c	35 MPa
E_c	27805.6 MPa

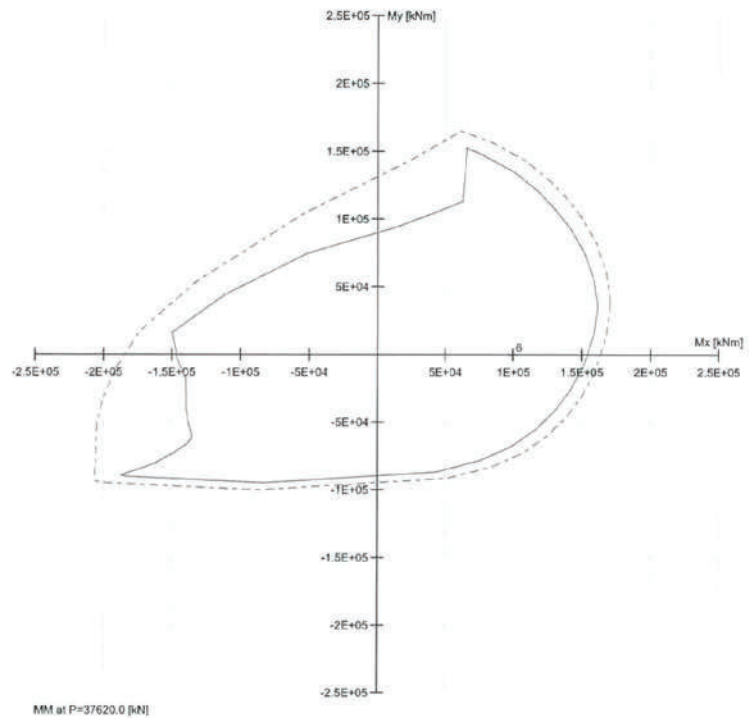
f_y	400 MPa
E_s	200000 MPa

Section

Type	Irregular
A_g	6.07125e+006 mm ²
I_x	3.34113e+013 mm ⁴
I_y	1.65083e+013 mm ⁴

Reinforcement

Pattern	Irregular
Bar layout	---
Cover to	---
Clear cover	---
Bars	---
Confinement type	Tied
Total steel area, A_s	79756 mm ²
Rho	1.31 %
Min. clear spacing	70 mm



No.	P_u kN	M_{ux} kNm	M_{uy} kNm	ϕP_n kN	ϕM_{ux} kNm	ϕM_{uy} kNm	Capacity Ratio
6	37620.0	99840.0	77.0	20602.70	120536.41	92.96	0.81

Max. Capacity Ratio: 0.81





รายงานการออกแบบ Design Note รายการคำนวณงานโครงสร้าง

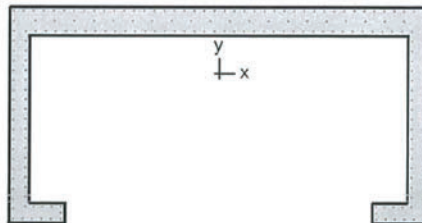
(สัญญาก่อสร้างอาคารทิศตะวันตก Final Detailed Design)

(ส่วนงานโครงสร้าง งานสถาปัตยกรรม และงานระบบหลัก)

โครงการพัฒนาพื้นที่ส่วนขยายศูนย์ราชการเฉลิมพระเกียรติ ๘๐ พรรษา ๕ ธันวาคม ๒๕๕๐ พื้นที่โซน C



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Computer program for the Strength Design of Reinforced Concrete Sections
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Contents

1. General Information	3
2. Material Properties	3
2.1. Concrete	3
2.2. Steel	3
3. Section	3
3.1. Shape and Properties	3
3.2. Section Figure	4
3.3. Exterior Points	4
4. Reinforcement	4
4.1. Bar Set: ASTM A615	4
4.2. Confinement and Factors	4
4.3. Arrangement	4
4.4. Bars Provided	5
5. Factored Loads and Moments with Corresponding Capacity Ratios	6
6. Diagrams	7
6.1. PM at $\theta=86$ [deg]	7
6.2. MM at $P=22200$ [kN]	8

List of Figures

Figure 1: Column section	4
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1. General Information

File Name	C:\193018\GCDT\SPcolumn\10-09-63(C1 ...)\P5-L2.col
Project	---
Column	---
Engineer	---
Code	ACI 318-14
Bar Set	ASTM A615
Units	Metric
Run Option	Investigation
Run Axis	Biaxial
Slenderness	Not Considered
Column Type	Structural
Capacity Method	Critical capacity

2. Material Properties

2.1. Concrete

Type	Standard
f_c	35 MPa
E_c	27805.6 MPa
f_{ct}	29.75 MPa
ϵ_u	0.003 mm/mm
β_1	0.796192

2.2. Steel

Type	Standard
f_y	400 MPa
E_s	200000 MPa
ϵ_{yt}	0.002 mm/mm

3. Section

3.1. Shape and Properties

Type	Irregular
A_g	4.63e+006 mm ²
I_x	5.27319e+012 mm ⁴
I_y	2.51091e+013 mm ⁴
r_x	1067.2 mm
r_y	2328.76 mm
X_o	0 mm
Y_o	0 mm



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Page | 4

9/18/2020
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3.2. Section Figure

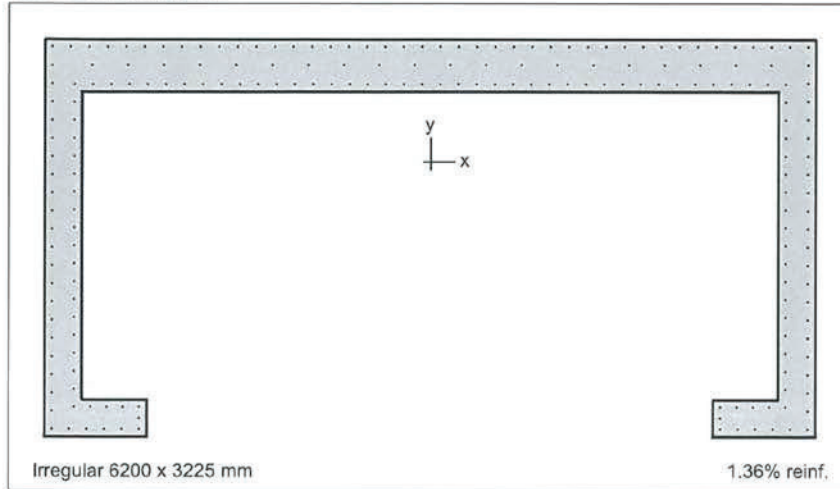


Figure 1: Column section

3.3. Exterior Points

Points	X mm	Y mm	Points	X mm	Y mm	Points	X mm	Y mm
1	-2275.0	-1932.7	2	-2800.0	-1932.7	3	-2800.0	567.3
4	2800.0	567.3	5	2800.0	-1932.7	6	2275.0	-1932.7
7	2275.0	-2232.7	8	3100.0	-2232.7	9	3100.0	992.3
10	-3100.0	992.3	11	-3100.0	-2232.7	12	-2275.0	-2232.7

4. Reinforcement

4.1. Bar Set: ASTM A615

Bar	Diameter mm	Area mm ²	Bar	Diameter mm	Area mm ²	Bar	Diameter mm	Area mm ²
#3	9.53	70.97	#4	12.70	129.03	#5	15.88	200.00
#6	19.05	283.87	#7	22.23	387.10	#8	25.40	509.68
#9	28.65	645.16	#10	32.26	819.35	#11	35.81	1006.45
#14	43.00	1451.61	#18	57.33	2580.64			

4.2. Confinement and Factors

Confinement type	Tied
For #10 bars or less	#3 ties
For larger bars	#4 ties
Capacity Reduction Factors	
Axial compression, (a)	0.8
Tension controlled ϕ , (b)	0.9
Compression controlled ϕ , (c)	0.65

4.3. Arrangement

Pattern	Irregular
Bar layout	---
Cover to	---
Clear cover	---
Bars	---





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Page | 5

9/18/2020

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Total steel area, A_s	62800 mm ²
Rho	1.36 %
Minimum clear spacing	70 mm



4.4. Bars Provided

Area mm ²	X mm	Y mm	Area mm ²	X mm	Y mm	Area mm ²	X mm	Y mm
314.0	-3040.0	932.3	314.0	-2899.6	-2172.7	314.0	-2891.7	932.3
314.0	-2860.0	-1992.7	314.0	-2860.0	-1847.1	314.0	-2860.0	-1701.5
314.0	-2860.0	-1556.0	314.0	-2860.0	-1410.4	314.0	-2860.0	-1264.9
314.0	-2860.0	-1119.3	314.0	-2860.0	-973.8	314.0	-2860.0	-828.2
314.0	-2860.0	-682.7	314.0	-2860.0	-537.1	314.0	-2860.0	-391.5
314.0	-2860.0	-246.0	314.0	-2860.0	-100.4	314.0	-2860.0	45.1
314.0	-2860.0	190.7	314.0	-2860.0	336.2	314.0	-2860.0	481.8
314.0	-2860.0	627.3	314.0	-2759.2	-2172.7	314.0	-2743.4	932.3
314.0	-2729.5	-1992.7	314.0	-2713.3	627.3	314.0	-2618.8	-2172.7
314.0	-2599.0	-1992.7	314.0	-2595.1	932.3	314.0	-2566.7	627.3
314.0	-2478.4	-2172.7	314.0	-2468.5	-1992.7	314.0	-2446.8	932.3
314.0	-2420.0	627.3	314.0	-2338.0	-2172.7	314.0	-2338.0	-2082.7
314.0	-2338.0	-1992.7	314.0	-2298.5	932.3	314.0	-2273.3	627.3
314.0	-2150.2	932.3	314.0	-2126.7	627.3	314.0	-2002.0	932.3
314.0	-1980.0	627.3	314.0	-1853.7	932.3	314.0	-1833.3	627.3
314.0	-1705.4	932.3	314.0	-1686.7	627.3	314.0	-1557.1	932.3
314.0	-1540.0	627.3	314.0	-1408.8	932.3	314.0	-1393.3	627.3
314.0	-1260.5	932.3	314.0	-1246.7	627.3	314.0	-1112.2	932.3
314.0	-1100.0	627.3	314.0	-963.9	932.3	314.0	-953.3	627.3
314.0	-815.6	932.3	314.0	-806.7	627.3	314.0	-667.3	932.3
314.0	-660.0	627.3	314.0	-519.0	932.3	314.0	-513.3	627.3
314.0	-370.7	932.3	314.0	-366.7	627.3	314.0	-222.4	932.3
314.0	-220.0	627.3	314.0	-74.1	932.3	314.0	-73.3	627.3
314.0	73.3	627.3	314.0	74.1	932.3	314.0	220.0	627.3
314.0	222.4	932.3	314.0	366.7	627.3	314.0	370.7	932.3
314.0	513.3	627.3	314.0	519.0	932.3	314.0	660.0	627.3
314.0	667.3	932.3	314.0	806.7	627.3	314.0	815.6	932.3
314.0	953.3	627.3	314.0	963.9	932.3	314.0	1100.0	627.3
314.0	1112.2	932.3	314.0	1246.7	627.3	314.0	1260.5	932.3
314.0	1393.3	627.3	314.0	1408.8	932.3	314.0	1540.0	627.3
314.0	1557.1	932.3	314.0	1686.7	627.3	314.0	1705.4	932.3
314.0	1833.3	627.3	314.0	1853.7	932.3	314.0	1980.0	627.3
314.0	2002.0	932.3	314.0	2126.7	627.3	314.0	2150.2	932.3
314.0	2273.3	627.3	314.0	2298.5	932.3	314.0	2335.0	-2172.7
314.0	2335.0	-2082.7	314.0	2335.0	-1992.7	314.0	2420.0	627.3
314.0	2446.8	932.3	314.0	2466.2	-1992.7	314.0	2476.0	-2172.7
314.0	2566.7	627.3	314.0	2595.1	932.3	314.0	2597.5	-1992.7
314.0	2617.0	-2172.7	314.0	2713.3	627.3	314.0	2728.7	-1992.7
314.0	2743.4	932.3	314.0	2758.0	-2172.7	314.0	2860.0	-1992.7
314.0	2860.0	-1847.1	314.0	2860.0	-1701.5	314.0	2860.0	-1556.0
314.0	2860.0	-1410.4	314.0	2860.0	-1264.9	314.0	2860.0	-1119.3
314.0	2860.0	-973.8	314.0	2860.0	-828.2	314.0	2860.0	-682.7
314.0	2860.0	-537.1	314.0	2860.0	-391.5	314.0	2860.0	-246.0
314.0	2860.0	-100.4	314.0	2860.0	45.1	314.0	2860.0	190.7
314.0	2860.0	336.2	314.0	2860.0	481.8	314.0	2860.0	627.3
314.0	2891.7	932.3	314.0	2899.0	-2172.7	314.0	3040.0	-2172.7
314.0	3040.0	-2024.8	314.0	3040.0	-1876.9	314.0	3040.0	-1729.1
314.0	3040.0	-1581.2	314.0	3040.0	-1433.4	314.0	3040.0	-1285.5
314.0	3040.0	-1137.7	314.0	3040.0	-989.8	314.0	3040.0	-841.9
314.0	3040.0	-694.1	314.0	3040.0	-546.2	314.0	3040.0	-398.4
314.0	3040.0	-250.5	314.0	3040.0	-102.7	314.0	3040.0	45.2
314.0	3040.0	193.1	314.0	3040.0	340.9	314.0	3040.0	488.8
314.0	3040.0	636.6	314.0	3040.0	784.5	314.0	3040.0	932.3

Area mm ²	X mm	Y mm	Area mm ²	X mm	Y mm	Area mm ²	X mm	Y mm
314.0	-3040.0	-548.7	314.0	-3040.0	-401.1	314.0	-3040.0	-253.5
314.0	-3040.0	-105.9	314.0	-3040.0	41.8	314.0	-3040.0	189.4
314.0	-3040.0	337.0	314.0	-3040.0	484.7	314.0	-3040.0	632.3
314.0	-3040.0	779.9	314.0	-3040.0	-2172.7	314.0	-3040.0	-2025.0
314.0	-3040.0	-1877.4	314.0	-3040.0	-1729.8	314.0	-3040.0	-1582.1
314.0	-3040.0	-1434.5	314.0	-3040.0	-1286.9	314.0	-3040.0	-1139.3
314.0	-3040.0	-991.6	314.0	-3040.0	-844.0	314.0	-3040.0	-696.4
314.0	-2719.0	784.3	314.0	-2431.6	784.2	314.0	-2144.2	784.1
314.0	-1856.7	784.0	314.0	-1569.3	783.9	314.0	-1281.9	783.9
314.0	-994.5	783.8	314.0	-707.1	783.7	314.0	-419.6	783.6
314.0	-132.2	783.5	314.0	155.2	783.4	314.0	442.6	783.3
314.0	730.1	783.2	314.0	1017.5	783.1	314.0	1304.9	783.0
314.0	1592.3	782.9	314.0	1879.7	782.8	314.0	2167.2	782.7
314.0	2454.6	782.6	314.0	2742.0	782.5			

5. Factored Loads and Moments with Corresponding Capacity Ratios

NOTE: Calculations are based on "Critical Capacity" Method.

No.	Demand			Capacity			Parameters at Capacity			Capacity Ratio
	P _u	M _{ux}	M _{uy}	φP _n	φM _{nx}	φM _{ny}	NA Depth	ε _t	φ	
	kN	kNm	kNm	kN	kNm	kNm	mm			
1	5660.00	4260.00	7710.00	0.00	34613.90	62646.29	1609	0.00743	0.900	0.39
2	27940.00	2700.00	21030.00	0.00	8667.66	67511.40	307	0.06737	0.900	0.55
3	16230.00	4470.00	45140.00	0.00	6666.78	67324.03	354	0.06088	0.900	0.76
4	19660.00	8810.00	23510.00	0.00	24968.12	66628.86	544	0.03511	0.900	0.54
5	21650.00	7050.00	82060.00	10885.20	8396.39	97731.63	675	0.02829	0.900	0.84
6	24820.00	18280.00	25300.00	23492.01	38103.29	52735.95	3178	0.00185	0.650	0.64
7	22200.00	7470.00	98340.00	15327.44	8291.05	109148.80	898	0.01944	0.900	0.89



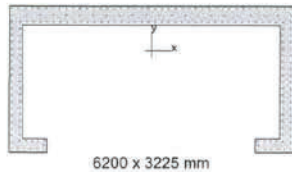
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Page | 7
9/18/2020
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6. Diagrams

6.1. PM at $\theta=86$ [deg]



General Information

Project	---
Column	---
Engineer	---
Code	ACI 318-14
Bar Set	ASTM A615
Units	Metric
Run Option	Investigation
Run Axis	Biaxial
Slenderness	Not Considered
Column Type	Structural
Capacity Method	Critical capacity

Materials

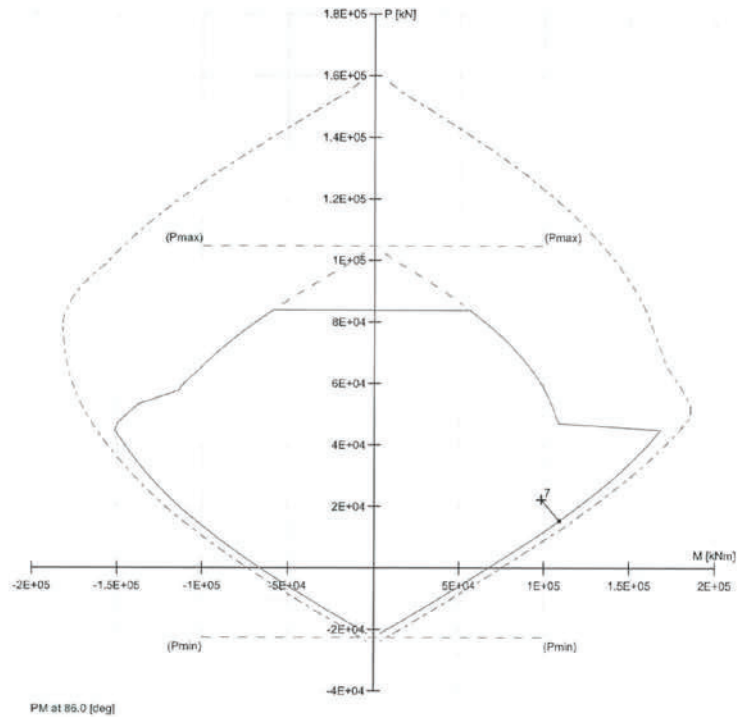
f_c	35 MPa
E_c	27805.6 MPa
f_y	400 MPa
E_s	200000 MPa

Section

Type	Irregular
A_g	4.63e+006 mm ²
I_x	5.27319e+012 mm ⁴
I_y	2.51091e+013 mm ⁴

Reinforcement

Pattern	Irregular
Bar layout	---
Cover to	---
Clear cover	---
Bars	---
Confinement type	Tied
Total steel area, A_s	62800 mm ²
Rho	1.36 %
Min. clear spacing	70 mm



No.	P_u kN	M_{ux} kNm	M_{uy} kNm	ϕP_u kN	ϕM_{ux} kNm	ϕM_{uy} kNm	Capacity Ratio
7	22200.0	7470.0	98340.0	15327.44	8291.05	109148.80	0.89

Max. Capacity Ratio: 0.89



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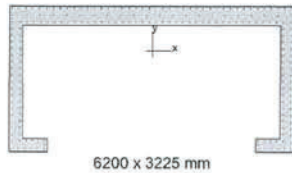
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Page | 8

9/18/2020

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6.2. MM at P=22200 [kN]



General Information

Project	---
Column	---
Engineer	---
Code	ACI 318-14
Bar Set	ASTM A615
Units	Metric
Run Option	Investigation
Run Axis	Biaxial
Slenderness	Not Considered
Column Type	Structural
Capacity Method	Critical capacity

Materials

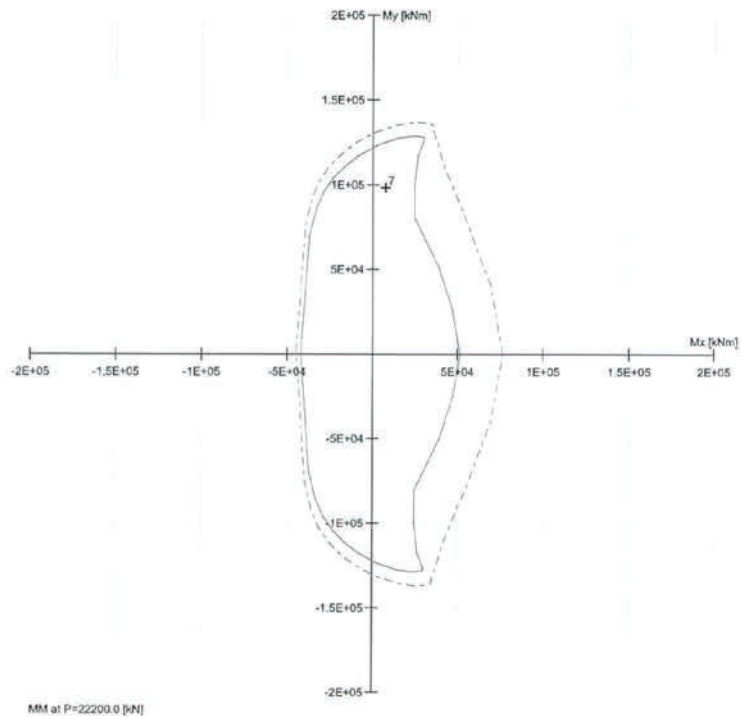
f_c	35 MPa
E_c	27805.6 MPa
f_y	400 MPa
E_s	200000 MPa

Section

Type	Irregular
A_g	4.63e+006 mm ²
I_x	5.27319e+012 mm ⁴
I_y	2.51091e+013 mm ⁴

Reinforcement

Pattern	Irregular
Bar layout	---
Cover to	---
Clear cover	---
Bars	---
Confinement type	Tied
Total steel area, A_s	62800 mm ²
Rho	1.36 %
Min. clear spacing	70 mm



No.	P_u kN	M_{ux} kNm	M_{uy} kNm	ϕP_u kN	ϕM_{ux} kNm	ϕM_{uy} kNm	Capacity Ratio
7	22200.0	7470.0	98340.0	15327.44	8291.05	109148.80	0.89

Max. Capacity Ratio: 0.89





รายงานการออกแบบ Design Note รายการคำนวณงานโครงสร้าง

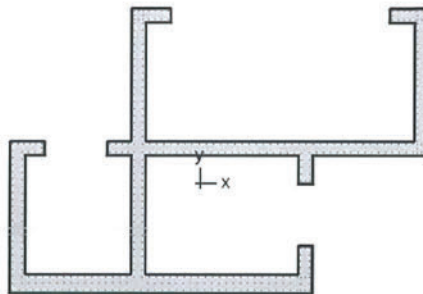
(สัญญาก่อสร้างอาคารทิศตะวันตก Final Detailed Design)

(ส่วนงานโครงสร้าง งานสถาปัตยกรรม และงานระบบหลัก)

โครงการพัฒนาพื้นที่ส่วนขยายศูนย์ราชการเฉลิมพระเกียรติ ๘๐ พรรษา ๕ ธันวาคม ๒๕๕๐ พื้นที่โซน C



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Computer program for the Strength Design of Reinforced Concrete Sections
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Contents

1. General Information	3
2. Material Properties.....	3
2.1. Concrete	3
2.2. Steel	3
3. Section	3
3.1. Shape and Properties.....	3
3.2. Section Figure	4
3.3. Exterior Points	4
4. Reinforcement	4
4.1. Bar Set: ASTM A615	4
4.2. Confinement and Factors	4
4.3. Arrangement.....	5
4.4. Bars Provided.....	5
5. Factored Loads and Moments with Corresponding Capacity Ratios.....	7
6. Diagrams	9
6.1. PM at $\theta=84$ [deg]	9
6.2. MM at $P=38760$ [kN].....	10

List of Figures

Figure 1: Column section	4
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1. General Information

File Name	C:\193018\GCDT\SPcolumn\10-09-63(C1 ...)\P6-L2.col
Project	---
Column	---
Engineer	---
Code	ACI 318-14
Bar Set	ASTM A615
Units	Metric
Run Option	Investigation
Run Axis	Biaxial
Slenderness	Not Considered
Column Type	Structural
Capacity Method	Critical capacity

2. Material Properties

2.1. Concrete

Type	Standard
f_c	35 MPa
E_c	27805.6 MPa
f_{ct}	29.75 MPa
ϵ_u	0.003 mm/mm
β_1	0.796192

2.2. Steel

Type	Standard
f_y	400 MPa
E_s	200000 MPa
ϵ_{yt}	0.002 mm/mm

3. Section

3.1. Shape and Properties

Type	Irregular
A_g	8.6825e+006 mm ²
I_x	2.8376e+013 mm ⁴
I_y	6.17429e+013 mm ⁴
r_x	1807.81 mm
r_y	2666.68 mm
X_o	-0.000117938 mm
Y_o	-0.000235877 mm



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Page | 4

9/18/2020

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3.2. Section Figure

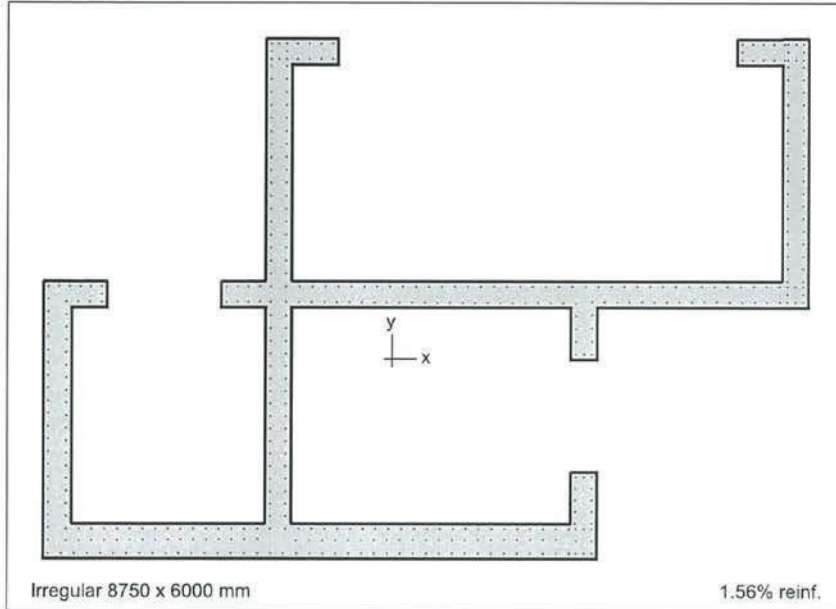


Figure 1: Column section

3.3. Exterior Points

Points	X mm	Y mm	Points	X mm	Y mm	Points	X mm	Y mm
1	2344.9	-1310.9	2	2044.9	-1310.9	3	2044.9	-1910.9
4	-1155.1	-1910.9	5	-1155.1	589.1	6	2044.9	589.1
7	2044.9	-10.9	8	2344.9	-10.9	9	2344.9	589.1
10	4769.9	589.1	11	4769.9	3689.1	12	4469.9	3689.1
13	4469.9	3683.1	14	3944.9	3683.1	15	3944.9	3383.1
16	4469.9	3383.1	17	4469.9	889.1	18	-1155.1	889.1
19	-1155.1	3389.1	20	-630.1	3389.1	21	-630.1	3689.1
22	-1455.1	3689.1	23	-1455.1	889.1	24	-1955.1	889.1
25	-1955.1	589.1	26	-1455.1	589.1	27	-1455.1	-1910.9
28	-3655.1	-1910.9	29	-3655.1	589.1	30	-3255.1	589.1
31	-3255.1	889.1	32	-3980.1	889.1	33	-3980.1	-2310.9
34	2344.9	-2310.9						

4. Reinforcement

4.1. Bar Set: ASTM A615

Bar	Diameter mm	Area mm ²	Bar	Diameter mm	Area mm ²	Bar	Diameter mm	Area mm ²
#3	9.53	70.97	#4	12.70	129.03	#5	15.88	200.00
#6	19.05	283.87	#7	22.23	387.10	#8	25.40	509.68
#9	28.65	645.16	#10	32.26	819.35	#11	35.81	1006.45
#14	43.00	1451.61	#18	57.33	2580.64			

4.2. Confinement and Factors

Confinement type	Tied
For #10 bars or less	#3 ties
For larger bars	#4 ties
Capacity Reduction Factors	
Axial compression, (a)	0.8



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Page | 5

9/18/2020

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Tension controlled ϕ , (b)	0.9
Compression controlled ϕ , (c)	0.65

4.3. Arrangement

Pattern	Irregular
Bar layout	---
Cover to	---
Clear cover	---
Bars	---
Total steel area, A_s	135020 mm ²
Rho	1.56 %
Minimum clear spacing	18 mm



4.4. Bars Provided

Area mm ²	X mm	Y mm	Area mm ²	X mm	Y mm	Area mm ²	X mm	Y mm
314.0	-1395.1	3629.1	314.0	-1305.1	3629.1	314.0	-1215.1	3629.1
314.0	-1215.1	3539.1	314.0	-1215.1	3449.1	314.0	-1305.1	3449.1
314.0	-1395.1	3449.1	314.0	-1395.1	3539.1	314.0	-1305.1	3629.1
314.0	4619.9	3629.1	314.0	4529.9	3629.1	314.0	4529.9	3536.1
314.0	4529.9	3443.1	314.0	4619.9	3443.1	314.0	4709.9	3443.1
314.0	4709.9	3536.1	314.0	4709.9	649.1	314.0	4619.9	649.1
314.0	4529.9	649.1	314.0	4529.9	739.1	314.0	4529.9	829.1
314.0	4619.9	829.1	314.0	4709.9	829.1	314.0	4709.9	739.1
314.0	2104.9	-1970.9	314.0	2194.9	-1970.9	314.0	2284.9	-1970.9
314.0	2284.9	-2110.9	314.0	2284.9	-2250.9	314.0	2194.9	-2250.9
314.0	2104.9	-2250.9	314.0	2104.9	-2110.9	314.0	2104.9	-1370.9
314.0	2194.9	-1370.9	314.0	2284.9	-1504.4	314.0	2284.9	-1370.9
314.0	2284.9	-1904.9	314.0	2284.9	-1771.4	314.0	2284.9	-1637.9
314.0	2094.9	-1504.4	314.0	2094.9	-1904.9	314.0	2094.9	-1771.4
314.0	2094.9	-1637.9	314.0	-3920.1	-2250.9	314.0	-3920.1	-2104.3
314.0	-3920.1	-1957.6	314.0	-3920.1	-1810.9	314.0	-3920.1	-1664.3
314.0	-3920.1	-1517.6	314.0	-3920.1	-1370.9	314.0	-3920.1	-1224.3
314.0	-3920.1	-1077.6	314.0	-3920.1	-930.9	314.0	-3920.1	-784.3
314.0	-3920.1	-637.6	314.0	-3920.1	-490.9	314.0	-3920.1	-344.3
314.0	-3920.1	-197.6	314.0	-3920.1	-50.9	314.0	-3920.1	95.7
314.0	-3920.1	242.4	314.0	-3920.1	389.1	314.0	-3920.1	535.7
314.0	-3920.1	682.4	314.0	-3920.1	829.1	314.0	-3799.1	829.1
314.0	-3771.3	-2250.9	314.0	-3715.1	-1970.9	314.0	-3715.1	-1825.4
314.0	-3715.1	-1679.8	314.0	-3715.1	-1534.3	314.0	-3715.1	-1388.7
314.0	-3715.1	-1243.2	314.0	-3715.1	-1097.6	314.0	-3715.1	-952.0
314.0	-3715.1	-806.5	314.0	-3715.1	-660.9	314.0	-3715.1	-515.4
314.0	-3715.1	-369.8	314.0	-3715.1	-224.3	314.0	-3715.1	-78.7
314.0	-3715.1	66.8	314.0	-3715.1	212.4	314.0	-3715.1	358.0
314.0	-3715.1	503.5	314.0	-3715.1	649.1	314.0	-3678.1	829.1
314.0	-3622.5	-2250.9	314.0	-3581.8	649.1	314.0	-3570.1	-1970.9
314.0	-3557.1	829.1	314.0	-3473.7	-2250.9	314.0	-3448.4	649.1
314.0	-3436.1	829.1	314.0	-3425.1	-1970.9	314.0	-3324.8	-2250.9
314.0	-3315.1	649.1	314.0	-3315.1	739.1	314.0	-3315.1	829.1
314.0	-3280.1	-1970.9	314.0	-3176.0	-2250.9	314.0	-3135.1	-1970.9
314.0	-3027.2	-2250.9	314.0	-2990.1	-1970.9	314.0	-2878.4	-2250.9
314.0	-2845.1	-1970.9	314.0	-2729.5	-2250.9	314.0	-2700.1	-1970.9
314.0	-2580.7	-2250.9	314.0	-2555.1	-1970.9	314.0	-2431.9	-2250.9
314.0	-2410.1	-1970.9	314.0	-2283.1	-2250.9	314.0	-2265.1	-1970.9
314.0	-2134.2	-2250.9	314.0	-2120.1	-1970.9	314.0	-1985.4	-2250.9
314.0	-1975.1	-1970.9	314.0	-1836.6	-2250.9	314.0	-1830.1	-1970.9
314.0	-1687.8	-2250.9	314.0	-1685.1	-1970.9	314.0	-1540.1	-1970.9



รายงานการออกแบบ Design Note รายการคำนวณงานโครงสร้าง

(สัญญาก่อสร้างอาคารทิศตะวันตก Final Detailed Design)

(ส่วนงานโครงสร้าง งานสถาปัตยกรรม และงานระบบหลัก)

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Page | 6

9/18/2020

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Area mm ²	X mm	Y mm	Area mm ²	X mm	Y mm	Area mm ²	X mm	Y mm
314.0	-1539.0	-2250.9	314.0	-1395.1	-1970.9	314.0	-1395.1	-1826.2
314.0	-1395.1	-1681.4	314.0	-1395.1	-1536.6	314.0	-1395.1	-1391.8
314.0	-1395.1	-1247.0	314.0	-1395.1	-1102.3	314.0	-1395.1	-957.5
314.0	-1395.1	-812.7	314.0	-1395.1	-667.9	314.0	-1395.1	-523.2
314.0	-1395.1	-378.4	314.0	-1395.1	-233.6	314.0	-1395.1	-88.8
314.0	-1395.1	56.0	314.0	-1395.1	200.7	314.0	-1395.1	345.5
314.0	-1395.1	490.3	314.0	-1390.1	-2250.9	314.0	-1241.3	-2250.9
314.0	-1215.1	490.3	314.0	-1215.1	345.5	314.0	-1215.1	200.7
314.0	-1215.1	56.0	314.0	-1215.1	-88.8	314.0	-1215.1	-233.6
314.0	-1215.1	-378.4	314.0	-1215.1	-523.2	314.0	-1215.1	-667.9
314.0	-1215.1	-812.7	314.0	-1215.1	-957.5	314.0	-1215.1	-1102.3
314.0	-1215.1	-1247.0	314.0	-1215.1	-1391.8	314.0	-1215.1	-1536.6
314.0	-1215.1	-1970.9	314.0	-1215.1	-1681.4	314.0	-1215.1	-1826.2
314.0	-1092.5	-2250.9	314.0	-1067.5	-1970.9	314.0	-943.7	-2250.9
314.0	-919.9	-1970.9	314.0	-794.8	-2250.9	314.0	-772.3	-1970.9
314.0	-646.0	-2250.9	314.0	-624.7	-1970.9	314.0	-497.2	-2250.9
314.0	-477.1	-1970.9	314.0	-348.4	-2250.9	314.0	-329.5	-1970.9
314.0	-199.6	-2250.9	314.0	-181.9	-1970.9	314.0	-50.7	-2250.9
314.0	-34.3	-1970.9	314.0	98.1	-2250.9	314.0	113.3	-1970.9
314.0	246.9	-2250.9	314.0	260.9	-1970.9	314.0	395.7	-2250.9
314.0	408.5	-1970.9	314.0	544.6	-2250.9	314.0	556.1	-1970.9
314.0	693.4	-2250.9	314.0	703.7	-1970.9	314.0	842.2	-2250.9
314.0	851.3	-1970.9	314.0	991.0	-2250.9	314.0	998.9	-1970.9
314.0	1139.8	-2250.9	314.0	1146.5	-1970.9	314.0	1288.7	-2250.9
314.0	1294.1	-1970.9	314.0	1437.5	-2250.9	314.0	1441.7	-1970.9
314.0	1586.3	-2250.9	314.0	1589.4	-1970.9	314.0	1735.1	-2250.9
314.0	1737.0	-1970.9	314.0	1884.0	-2250.9	314.0	1884.6	-1970.9
314.0	2032.2	-1970.9	314.0	2032.8	-2250.9	314.0	-1895.1	829.1
314.0	-1770.1	829.1	314.0	-1645.1	829.1	314.0	-1520.1	829.1
314.0	-1395.1	829.1	314.0	-1895.1	649.1	314.0	-1770.1	649.1
314.0	-1645.1	649.1	314.0	-1520.1	649.1	314.0	-1395.1	649.1
314.0	-1215.1	649.1	314.0	-1070.8	648.5	314.0	-926.4	647.8
314.0	-782.1	647.2	314.0	-637.7	646.6	314.0	-493.4	646.0
314.0	-349.0	645.4	314.0	-204.7	644.8	314.0	-60.3	644.2
314.0	84.0	643.6	314.0	228.4	643.0	314.0	372.7	642.4
314.0	517.1	641.8	314.0	661.4	641.2	314.0	805.8	640.5
314.0	950.1	639.9	314.0	1094.4	639.3	314.0	1238.8	638.7
314.0	1383.1	638.1	314.0	1527.5	637.5	314.0	1671.8	636.9
314.0	1816.2	636.3	314.0	1960.5	635.7	314.0	2104.9	49.1
314.0	2104.9	195.6	314.0	2104.9	342.1	314.0	2104.9	488.6
314.0	2104.9	635.1	314.0	2194.9	49.1	314.0	2284.9	49.1
314.0	2284.9	199.1	314.0	2284.9	349.1	314.0	2284.9	499.1
314.0	2284.9	649.1	314.0	2428.7	649.1	314.0	2572.6	649.1
314.0	2716.5	649.1	314.0	2860.3	649.1	314.0	3004.2	649.1
314.0	3148.0	649.1	314.0	3291.9	649.1	314.0	3435.8	649.1
314.0	3579.6	649.1	314.0	3723.5	649.1	314.0	3867.3	649.1
314.0	4011.2	649.1	314.0	4155.0	649.1	314.0	4298.9	649.1
314.0	4442.8	649.1	314.0	-1215.1	978.5	314.0	-1215.1	1128.0
314.0	-1215.1	1277.4	314.0	-1215.1	1426.9	314.0	-1215.1	1576.3
314.0	-1215.1	1725.7	314.0	-1215.1	1875.2	314.0	-1215.1	2024.6
314.0	-1215.1	2174.1	314.0	-1215.1	2323.5	314.0	-1215.1	2473.0
314.0	-1215.1	2622.4	314.0	-1215.1	2771.9	314.0	-1215.1	2921.3
314.0	-1215.1	3070.8	314.0	-1215.1	3220.2	314.0	-1215.1	3369.7
314.0	-1215.1	829.1	314.0	-1066.3	829.1	314.0	-917.4	829.1
314.0	-768.6	829.1	314.0	-619.8	829.1	314.0	-470.9	829.1
314.0	-322.1	829.1	314.0	-173.2	829.1	314.0	-24.4	829.1
314.0	124.4	829.1	314.0	273.3	829.1	314.0	422.1	829.1
314.0	571.0	829.1	314.0	719.8	829.1	314.0	868.6	829.1
314.0	1017.5	829.1	314.0	1166.3	829.1	314.0	1315.1	829.1



รายงานการออกแบบ Design Note รายการคำนวณงานโครงสร้าง

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Page | 7

9/18/2020

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Area mm ²	X mm	Y mm	Area mm ²	X mm	Y mm	Area mm ²	X mm	Y mm
314.0	1464.0	829.1	314.0	1612.8	829.1	314.0	1761.7	829.1
314.0	1910.5	829.1	314.0	2059.3	829.1	314.0	2208.2	829.1
314.0	2357.0	829.1	314.0	2505.9	829.1	314.0	2654.7	829.1
314.0	2803.5	829.1	314.0	2952.4	829.1	314.0	3101.2	829.1
314.0	3250.0	829.1	314.0	3398.9	829.1	314.0	3547.7	829.1
314.0	3696.6	829.1	314.0	3845.4	829.1	314.0	3994.2	829.1
314.0	4143.1	829.1	314.0	4291.9	829.1	314.0	4440.8	829.1
314.0	-1395.1	974.7	314.0	-1395.1	1124.2	314.0	-1395.1	1273.7
314.0	-1395.1	1423.2	314.0	-1395.1	1572.7	314.0	-1395.1	1722.2
314.0	-1395.1	1871.7	314.0	-1395.1	2021.1	314.0	-1395.1	2170.6
314.0	-1395.1	2320.1	314.0	-1395.1	2469.6	314.0	-1395.1	2619.1
314.0	-1395.1	2768.6	314.0	-1395.1	2918.1	314.0	-1395.1	3067.6
314.0	-1395.1	3217.1	314.0	-1395.1	3366.6	314.0	-1096.1	3629.1
314.0	-960.8	3629.1	314.0	-825.4	3629.1	314.0	-690.1	3629.1
314.0	-1096.1	3449.1	314.0	-960.8	3449.1	314.0	-825.4	3449.1
314.0	-690.1	3449.1	314.0	4004.9	3443.1	314.0	4004.9	3533.1
314.0	4004.9	3623.1	314.0	4126.6	3443.1	314.0	4126.6	3623.1
314.0	4248.4	3443.1	314.0	4248.4	3623.1	314.0	4370.1	3443.1
314.0	4370.1	3623.1	314.0	4491.9	3443.1	314.0	4491.9	3623.1
314.0	4529.9	2199.3	314.0	4529.9	2344.8	314.0	4529.9	2490.4
314.0	4529.9	2636.0	314.0	4529.9	2781.6	314.0	4529.9	2927.2
314.0	4529.9	3072.7	314.0	4529.9	3218.3	314.0	4529.9	3363.9
314.0	4529.9	889.1	314.0	4529.9	1034.6	314.0	4529.9	1180.2
314.0	4529.9	1325.8	314.0	4529.9	1471.4	314.0	4529.9	1617.0
314.0	4529.9	1762.5	314.0	4529.9	1908.1	314.0	4529.9	2053.7
314.0	4709.9	2780.0	314.0	4709.9	2925.5	314.0	4709.9	3070.9
314.0	4709.9	3216.4	314.0	4709.9	3361.9	314.0	4709.9	1616.4
314.0	4709.9	1761.8	314.0	4709.9	1907.3	314.0	4709.9	2052.7
314.0	4709.9	2198.2	314.0	4709.9	2343.7	314.0	4709.9	2489.1
314.0	4709.9	2634.6	314.0	4709.9	889.1	314.0	4709.9	1034.5
314.0	4709.9	1180.0	314.0	4709.9	1325.4	314.0	4709.9	1470.9
314.0	-1096.1	-2105.6	314.0	-947.0	-2105.1	314.0	-797.8	-2104.6
314.0	-648.7	-2104.1	314.0	-499.5	-2103.5	314.0	-350.3	-2103.0
314.0	-201.2	-2102.5	314.0	-52.0	-2102.0	314.0	97.1	-2101.4
314.0	246.3	-2100.9	314.0	395.4	-2100.4	314.0	544.6	-2099.8
314.0	693.7	-2099.3	314.0	842.9	-2098.8	314.0	992.0	-2098.3
314.0	1141.2	-2097.7	314.0	1290.3	-2097.2	314.0	1439.5	-2096.7
314.0	1588.6	-2096.2	314.0	1737.8	-2095.6	314.0	1887.0	-2095.1
314.0	-3712.6	-2106.4	314.0	-3567.6	-2105.4	314.0	-3422.7	-2104.4
314.0	-3277.7	-2103.4	314.0	-3132.8	-2102.4	314.0	-2987.8	-2101.4
314.0	-2842.9	-2100.4	314.0	-2697.9	-2099.4	314.0	-2553.0	-2098.4
314.0	-2408.0	-2097.3	314.0	-2263.1	-2096.3	314.0	-2118.1	-2095.3
314.0	-1973.2	-2094.3	314.0	-1828.2	-2093.3	314.0	-1683.3	-2092.3
314.0	-1538.3	-2091.3						

5. Factored Loads and Moments with Corresponding Capacity Ratios

NOTE: Calculations are based on "Critical Capacity" Method.

No.	Demand			Capacity			Parameters at Capacity			Capacity Ratio
	P _u kN	M _{ux} kNm	M _{uy} kNm	φP _n kN	φM _{nx} kNm	φM _{ny} kNm	NA Depth mm	ε _t	φ	
1	9140.00	11680.00	38260.00	0.00	39335.46	128850.56	1293	0.01327	0.900	0.59
2	43180.00	2110.00	46790.00	0.00	7065.40	156677.83	1223	0.01453	0.900	0.54
3	28560.00	11559.00	81990.00	0.00	20818.40	147668.56	1141	0.01508	0.900	0.69
4	34480.00	61580.00	3120.00	0.00	106524.84	5397.17	650	0.03630	0.900	0.67
5	30180.00	18560.00	64720.00	0.00	37514.41	130815.34	1274	0.01349	0.900	0.65
6	35490.00	79010.00	3880.00	0.00	106535.33	5231.71	649	0.03642	0.900	0.73
7	38760.00	16890.00	164790.00	15864.75	19662.69	191842.20	1469	0.01096	0.900	0.83



รายงานการออกแบบ Design Note รายการคำนวณงานโครงสร้าง

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Page | 8

9/18/2020

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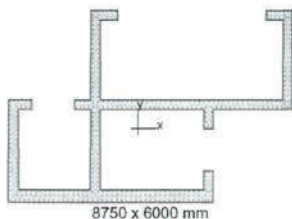
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Page | 9
9/18/2020
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6. Diagrams

6.1. PM at $\theta=84$ [deg]



General Information

Project	---
Column	---
Engineer	---
Code	ACI 318-14
Bar Set	ASTM A615
Units	Metric
Run Option	Investigation
Run Axis	Biaxial
Slenderness	Not Considered
Column Type	Structural
Capacity Method	Critical capacity

Materials

f_c	35 MPa
E_c	27805.6 MPa
f_y	400 MPa
E_s	200000 MPa

Section

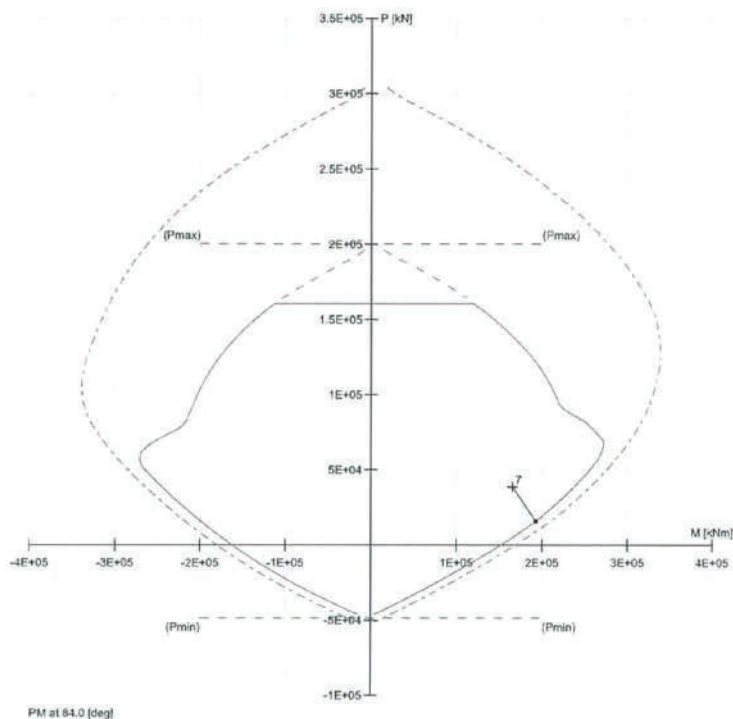
Type	Irregular
A_g	8.6825e+006 mm ²
I_x	2.8376e+013 mm ⁴
I_y	6.17429e+013 mm ⁴

Reinforcement

Pattern	Irregular
Bar layout	---
Cover to	---
Clear cover	---
Bars	---

Confinement type Tied

Total steel area, A_s	135020 mm ²
Rho	1.56 %
Min. clear spacing	18 mm



No.	P_u kN	M_{ux} kNm	M_{uy} kNm	ϕP_u kN	ϕM_{ux} kNm	ϕM_{uy} kNm	Capacity Ratio
7	38760.0	16890.0	164790.0	15864.75	19662.69	191842.20	0.83

Max. Capacity Ratio: 0.83

